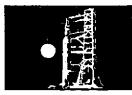
## S P A C E DIVISION





















# ERTS 1 FLIGHT EVALUATION REPORT 23 APRIL 1974 TO 23 JULY 1974

Prepared By
GE ERTS OPERATIONS CONTROL CENTER

For

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
Goddard Space Flight Center
Greenbelt, Maryland 20771



## Contract NAS5-21808

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APPROVED:

Thomas W. Winchester



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## INTRODUCTION

This is the ninth report in a continuing series of documents issued quarterly to present flight performance analysis of the ERTS-1 Spacecraft. Previously issued documents are:

72SD4255	ERTS-1 Launch and Flight Activation Evaluation Report 23 to 26 July 1972	18 October 1972
72SD4262	ERTS-1 Flight Evaluation Report 23 July 1972 to 23 October 1972	28 November 1972
72SD4224	ERTS-1 Flight Evaluation Report 23 October 1972 to 23 January 1973	27 February 1973
73SD4249	ERTS-1 Flight Evaluation Report 23 January 1973 to 23 April 1973	29 May 1973
73SD4260	ERTS-1 Flight Evaluation Report 23 April 1973 to 23 July 1973	10 August 1973
73SD4274	ERTS-1 Flight Evaluation Report 23 July 1973 to 23 October 1973	28 November 1973
74SD4205	ERTS-1 Flight Evaluation Report 23 October 1973 to 23 January 1974	26 February 1974
74SD4217	ERTS-1 Flight Evaluation Report 23 January 1974 to 23 April 1974	18 May 1974

This report contains analyses of performance for the eighth quarter of operation i.e., Orbit 8908 to 10182.

## SECTION 1 SUMMARY - ERTS-1 OPERATIONS

### SUMMARY - ERTS-1 OPERATIONS

The ERTS-1 spacecraft was launched from the Western Test Range on 23 July 1972 at 18:06:06.508Z. The launch and orbital injection phase of the space flight were nominal and deployment of the spacecraft followed predictions. Orbital operations of the spacecraft and payload subsystems were satisfactory through Orbit 147 after which an internal short circuit disabled one of the Wideband Video Tape Recorders (WBVTR-2). Operations resumed until Orbit 196 when the Return Beam Vidicon failed to respond when commanded off. The RBV was commanded off via alternate commands and since that time ERTS-1 has performed its mission with the Multispectral Scanner and the remaining Wideband Video Tape Recorder providing image data. The remaining Wideband Video Tape Recorder experienced four suspensions of operation, but corrective measures have permitted resumption of limited operations the first three times. The last suspension of operations was in Orbit 9881 on 2 July 1974, and corrective measures are still being studied. In Orbit 4396 an integrated circuit chip in the TMP failed, disabling four TLM functions. COMSTOR "B" has an intermittent problem with cell 12, and the pitch flywheel duty cycle is somewhat higher than normal for this flight and also exhibited a two minute halt in Orbit 8040. The "B" section of the USB with full power output of 1.5 watts was substituted for the "A" section in Orbit 10068 because of excessive decline of transmitter power. Spacecraft performance has not been degraded by these anomalies thus far, except for the inability to record remote MSS imagery.

## ORBITAL PARAMETERS

The initial orbit of ERTS-1 required some correction at Orbits 44 and 59 to achieve the desired 18-day repeat cycle. During Orbits 938, 2416, 6390 and 7826 it was necessary to fire the -X thruster of the orbit adjust system to maintain the ground trace in the desired 18-day repeat pattern of ± 10 nm. The ground trace was within the allowable band throughout this reporting period.

#### POWER SUBSYSTEM

The power subsystem performed well throughout this report period. Solar array current has been slightly lower than predicted. Data from this period shows the array degradation to be -21.1% after 24 months in orbit. The power subsystem will meet ERTS-1 power requirements thru 1976 with the present payload configuration. Battery temperature spread remained low and performance of each battery remained good.

#### ATTITUDE CONTROL SUBSYSTEM

From the initial acquisition, the ACS performance has been excellent. All functions are active and well within specifications. Perturbations due to sun glint in the IR horizon scanners are not disruptive enough to necessitiate single scanner mode. Gating frequency decreased during this period conforming to performance at this time last year. The forward IR scanner pressure has decreased slightly (4.6 PSIA at launch, 3.50 PSIA at Orbit 10182). Pitch, roll and yaw flywheel drive duty cycles increase for short periods but return to normal. The increases in pitch are more sustained and a two minute halt in the pitch flywheel was noted in Orbit 8040. The pitch flywheel average speed was increased to obtain a better lubrication condition.

## COMMAND/CLOCK SUBSYSTEM

All stored commands and real time commands have executed except for the expected one-in-approximately 10,000 associated with the logic race condition. No serious problems have resulted from these few commands failing to execute. Use of cell 12 COMSTOR "B" has been discontinued for active commands because of intermittent time delta errors of 256 seconds. Occasionally stored commands are blocked by real-time sequences which overlap in time. Specific cause has not been determined. The VHF command receiver was switched from side B to side A at the time of USB subsystem switchover to side B.

## TELEMETRY SUBSYSTEM

The telemetry subsystem has consistently performed in an excellent manner. Memory Section 0, 0 has been in use since launch. All dropouts have been associated with known link or ground problems. Except for failure of an integrated circuit chip in the TMP (Orbit 4396), disabling four telemetry functions, all functions have performed in a nominal manner.

## ORBIT ADJUST SUBSYSTEM

The orbit adjust subsystem has been fired eight times, using the -X thruster each time. Three firings were for initial correction, and five for orbit maintenance. All functions were normal with the expected ephemeris changes being achieved. Pressure/temperature parameters continue to be normal.

#### MAGNETIC MOMENT COMPENSATING ASSEMBLY

The Magnetic Moment Compensating Assembly has been operated five times prior to this report period and performance has been considered excellent. It has held the Pole-Cm values commanded in earlier orbits. Status Telemetry values continue to be normal.

## UNIFIED "S" BAND/PRE-MODULATION PROCESSOR

The Unified S-Band Subsystem has operated satisfactorily since launch. On Orbit 10068 the B-Section was substituted for the A-Section because the A-transmitter power output had declined from 1.6 watts at launch to 0.14 watts with noticeable loss of DCS coverage. The B-transmitter has power output of 1.5 watts.

#### ELECTRICAL INTERFACE SUBSYSTEM

The Auxiliary Processing Unit (APU), Interface Switching Module (ISM) and Power Switching Module (PSM) performed normally in this report period. The RBV switching relay (within the PSM) failed in Orbit 196.

#### THERMAL CONTROL SUBSYSTEM

The thermal subsystem performed normally throughout this period. Temperatures decreased slightly due to decreasing sun intensity but had no noticeable effect on operation.

### NARROWBAND TAPE RECORDER SUBSYSTEM

The Narrowband Tape Recorder Subsystem has continued to operate satisfactorily without incident. The total ON time is 9217 hours for each recorder (A and B).

## WIDEBAND TELEMETRY SUBSYSTEM

The Wideband Telemetry Subsystem has continued to operate satisfactorily. The power output has continued at 20 watts since launch. WPA-2 is currently in use. WPA-1 was used with RBV to Orbit 196 and subsequently between Orbits 1890 and 2099 with MSS during Apollo 17 operations.

### ATTITUDE MEASUREMENT SENSOR

The AMS continues to function normally in all aspects.

## WIDEBAND VIDEO TAPE RECORDERS

Wideband Video Tape Recorder-2 failed after 10 days in orbit. Wideband Video Tape Recorder-1 has 3 prior gaps in its satisfactory performance since launch, and again has been temporarily removed from service since Orbit 9881 pending study of corrective action.

### RETURN BEAM VIDICON

The Return Beam Vidicon has been idle since Orbit 196 when its prime input power switching relay failed. RBV performed satisfactorily up to that point and is available for use, if needed, by an alternate switching mode.

## MULTISPECTRAL SCANNER SUBSYSTEM

The Multispectral Scanner Subsystem continues to operate in a completely satisfactory manner. It has imaged more than 27% of the earth's surface (including water) between the latitudes of 81.42°, including 78% of the continents, with a cloud cover of 30% or less. All units of the Subsystem are normal and stable.

## DATA COLLECTION SYSTEM

The Data Collection Subsystem continues to operate satisfactorily. Only Receiver A has been used to date.

## PAYLOAD OPERATION SUMMARY

Launch through Orbit 10182

Subsystem	Orbital On-Time HH:MM:SS	Operational Summary	
RBV	13:59:09	Total scenes photographed Average scenes per day Total area photographed (millions of square nautical miles) ON-OFF cycles % Real Time scenes % Recorded scenes	1,690 139 14.7 91 57 43
MSS	1431:59:24	Total scenes photographed Average scenes per day Total area photographed (millions of square nautical miles) ON-OFF cycles % Real Time scenes % Recorded scenes	113,781 184 1166.5 11284 65 35
DCS	17516:14:43	Messages received at OCC Non perfect messages Maximum Ground platforms active/day Users Average messages per orbit	945, 451 74, 442 110 43 186
WBVTR-1	882:25:04	% Record Mode % Playback Mode % Rewind Mode % Standby Mode Minor Frame Sync. Error Count during Playback Time Video Head-to tape contact Cycles of Head-to tape contact	38 41 20 1 150 724:18:00 12017
WBVTR-2	9:26:33	% Usage same as WBVTR-1 Failed in Orbit 148/9	
WPA-1	31:55:09	% Real Time Mode % Playback Mode (Used in Orbits 5 thru 196 and 1890 thru 2099) ON-OFF cycles	55 45 311
WPA-2	1377:31:48	% Real Time Mode % Playback Mode (Used in Orbits 5 thru 1899 and since 2100) ON-OFF cycles	65 35 8774

ORBITAL PARAMETERS

## SECTION 2 ORBITAL PARAMETERS

ERTS-1 launch and injection was satisfactory and required only a minor orbit adjust to achieve normal parameters. These adjustments were made in Orbits 38, 44 and 59. After several 18-day repeat cycles, orbit maintenance burns were made in Orbit 938, Orbit 2416, Orbit 6390 and Orbit 7826.

The orbital parameters are given in Table 2-1. Figure 2-1 shows the sub-satellite plot and Figure 2-2 shows the longitude error as a function of time and orbit maintenance burns. The longitude error has been maintained within the  $\pm$  10 nm average in the east-west direction at the equator as planned. Figure 2-3 shows the change of sun time at the descending node equator crossing. Appendix B gives ground trace repeat cycle predictions.

Table 2-1. Brouwer Mean Orbital Parameters

	Element		25 Oct 1972	25 Jan 1973	25 Apr 1973	25 July-1973	25 Oct 1973	25 Jan 1974	24 Apr 1974	23 July 1974
(1)	Apogee	KM	917.3	922.3	911, 056	914, 341	922, 013	915, 873	920, 090	922, 363
(2)	Perigee	KM	898.1	893.1	888.763	900. 810	893. 229	899, 111	912,672	892,629
(3)	Inclination	deg	99, 103	99,090	99.073	99,068	99, 056	99, 041	99.023	99.017
(4)	Semimajor Axis	KM	7,285,850	7,285.865	7,285,767	7,285,741	7,285,786	7,285,657	7, 285, 691	7, 285, 661
(5)	Eccentricity		0.00132	0.00200	0,00073	0, 00093	0. 00198	0,00115	0,000802	0.002041
(6)	Anomalistic Period	min	103, 152	103, 153	103, 151	103,150	103, 151	103, 148	103.149	103, 148
(7)	Nodal Period	min	103, 268	103,268	103, 267	103, 266	103, 266	103, 264	103, 265	103, 264
(B)	Argument of Perigee	deg	93, 721	133, 693	168, 857	95, 602	65. 071	160, 866	117.631	109, 225
(9)	Right Ascension	deg	1.060	91,805	181, 411	268, 944	0.2912	88, 606	176, 743	269,779
(10)	Mean Anomaly	deg	86.484	52,797	11,098	84, 301	301, 002	19.049	62,319	70, 540

REFECTIVE OF THE ORIGINAL PAGE IS POOR

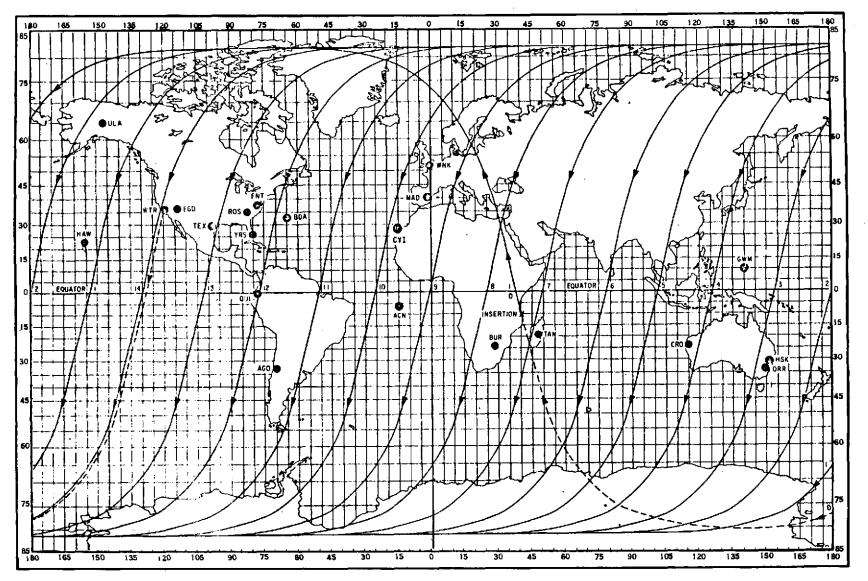


Figure 2-1. Typical Subsatellite Plot of the ERTS-1 Spacecraft

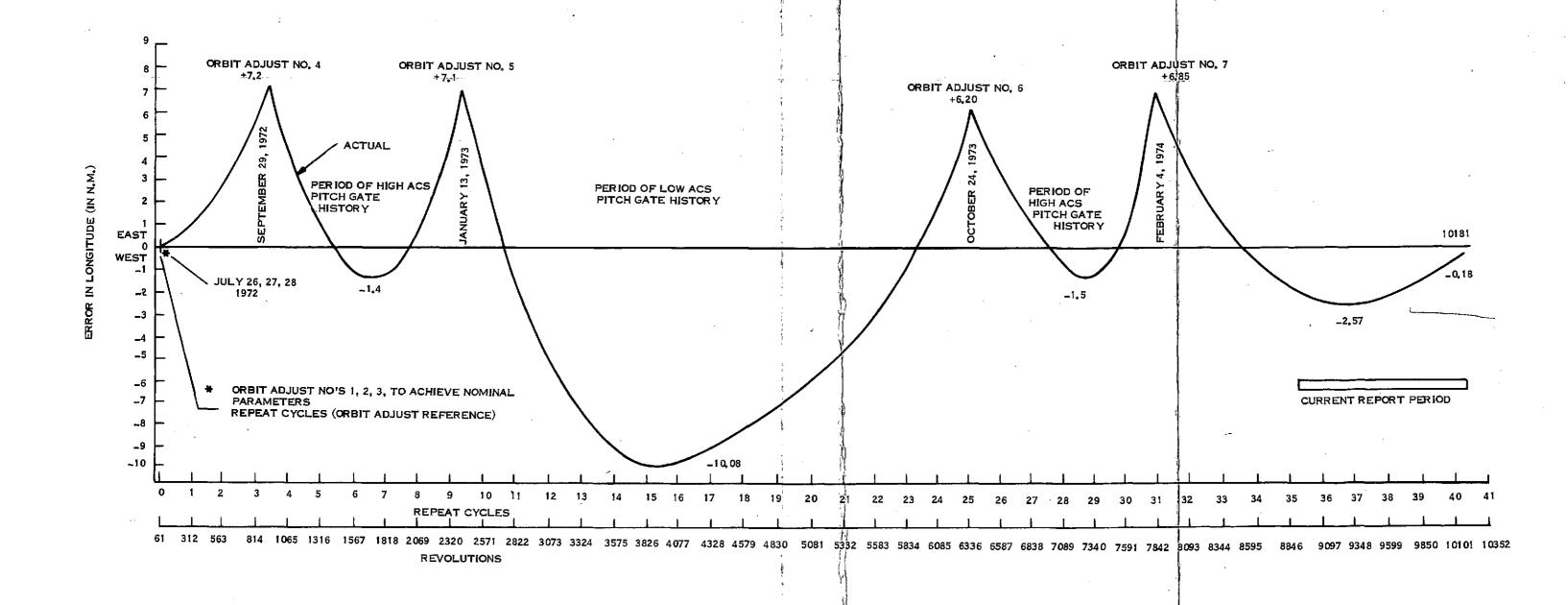


Figure 2-2. Effects of Orbits Adjust on Ground Track

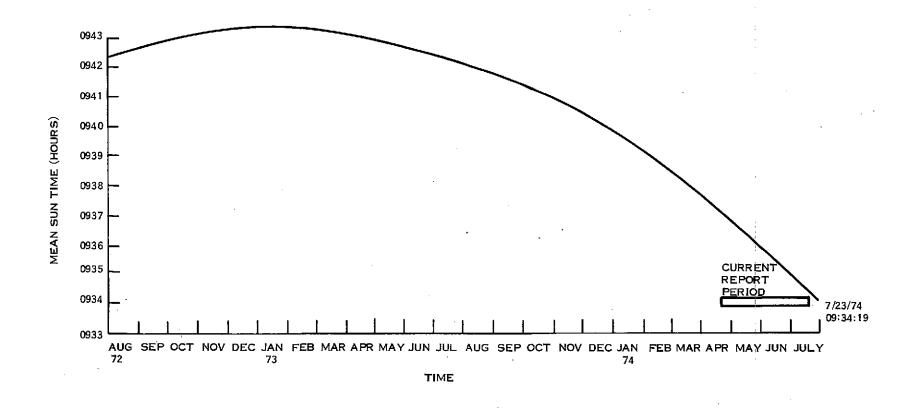


Figure 2-3. Mean Sun Time Equator Crossing-Descending Node

SECTION 3
POWER SUBSYSTEM (PWR)

## POWER SUBSYSTEM (PWR)

The solar array continued to provide excess energy for the payload and spacecraft load throughout this report period. Compensation loads and auxiliary loads dissipated the excess power above the battery and load requirements using ERTS-1 power management procedures. Midday measured solar array current tracked slightly below the values predicted earlier due to higher than predicted beta angle variations. Solar array degradation was -21.1% at the end of 24 months in orbit. The power subsystem is predicted to have adequate power through 1976 for the present ERTS-1 payload configuration and may extend to 1977 and 1978 depending on the electro-chemical degradation of the battery packs for that period.

A plot of measured and predicted midday solar current is shown in Figure 3-1. Figure 3-2 shows actual and predicted solar array current degradation. Figure 3-3 shows actual sun angles to the spacecraft and solar panels. Figure 3-4 shows seasonal solar intensity variation. It is noted on Figure 3-1 that the high noon solar array current is slightly lower than predicted. This is due to slightly different solar panel sun angles and operating point high noon solar array degradation than initially predicted. On 20 June 1974, in Orbit 9711, ERTS-1 passed through a total solar eclipse in the southern hemisphere over the Indian Ocean. The ground trace through the eclipse is shown in Figure 3-5.

Battery packs ranged from 9.8 to 11.2 percent depth of Discharge (DOD) with an average of 10.0 over a 24-hour period of normal operation. Temperature spread between batteries decreased to 5.1 degrees C during this report period due to decreasing sun intensity. Charge and load sharing were satisfactory.

The power system electronics performed well in this report period with all voltages stable. Table 3-1 shows major power subsystem parameters and Table 3-2 shows power subsystem telemetry for selected orbits. Some parameters in Table 3-2 may be slightly different than Table 3-1 because Table 3-1 uses a time span for power management

(night followed by a day) different from the time span which is used in Table 3-2 which is the playback period from the NBTR. The Shunt Limiter has not operated since Orbit 3 because the unregulated voltage has been held below cut-in voltage by power management.

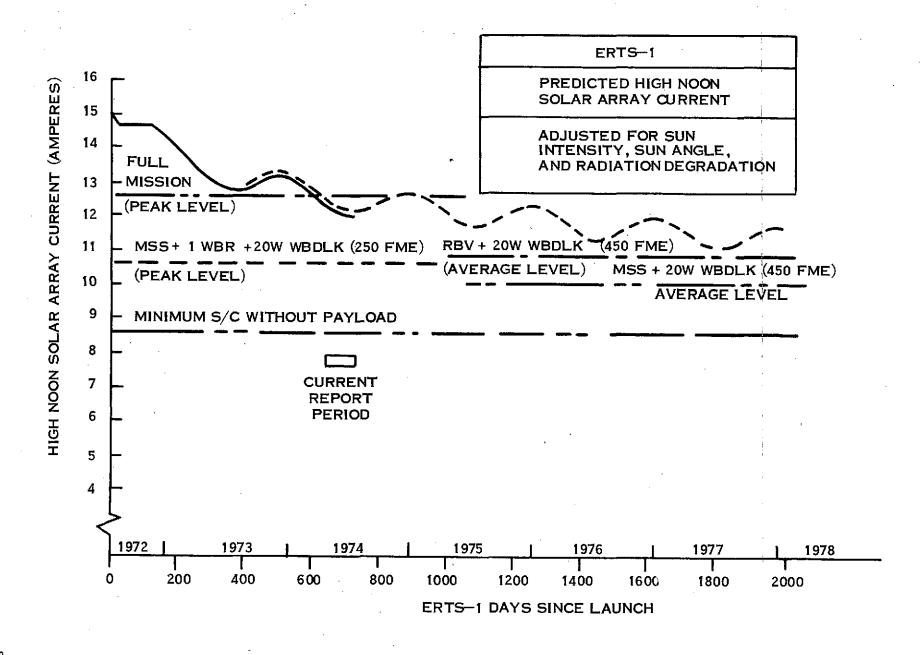


Figure 3-1. Predicted Midday Solar Current

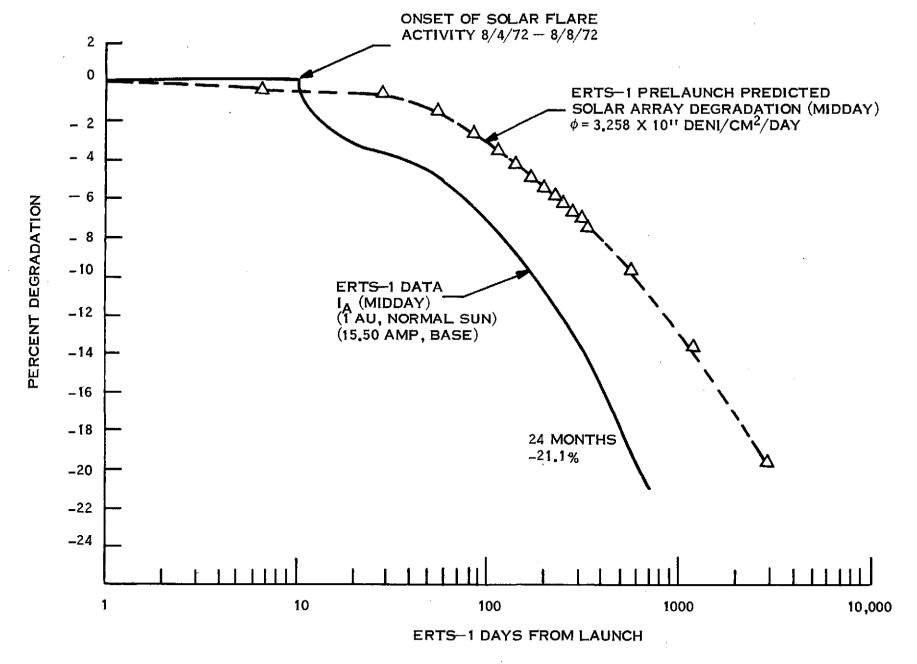


Figure 3-2. IA (Midday) Degradation vs. Days

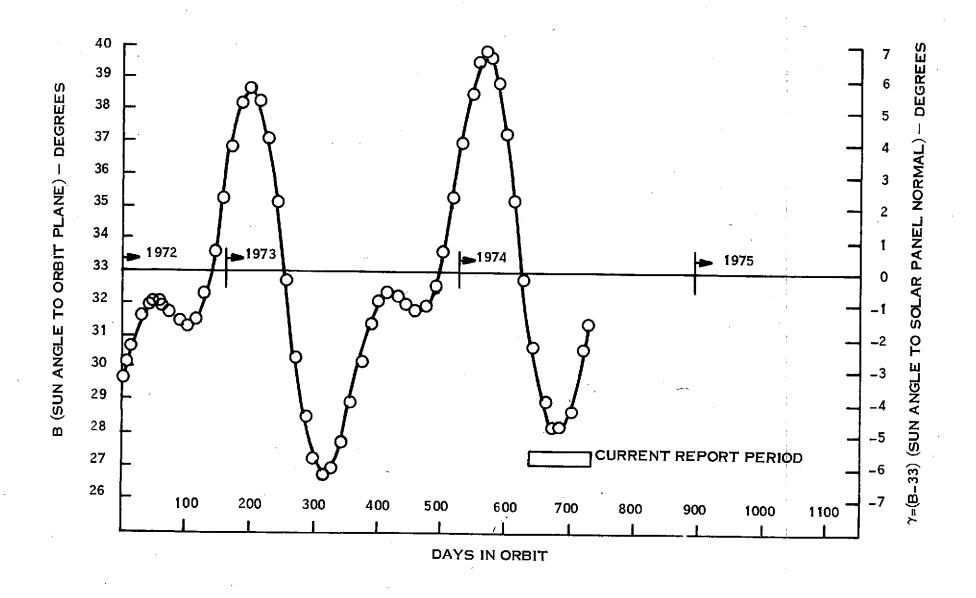


Figure 3-3. Actual  $\beta$  and  $\gamma$  (Paddle) Sun Angles

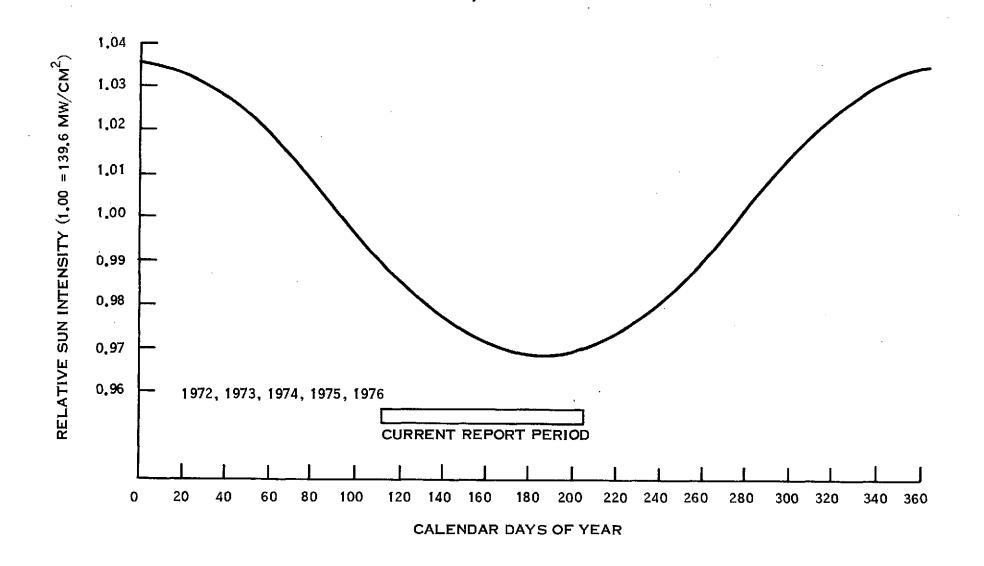


Figure 3-4. Seasonal Solar Intensity Variations

## TOTAL SOLAR ECLIPSE OF 1974 JUNE 20

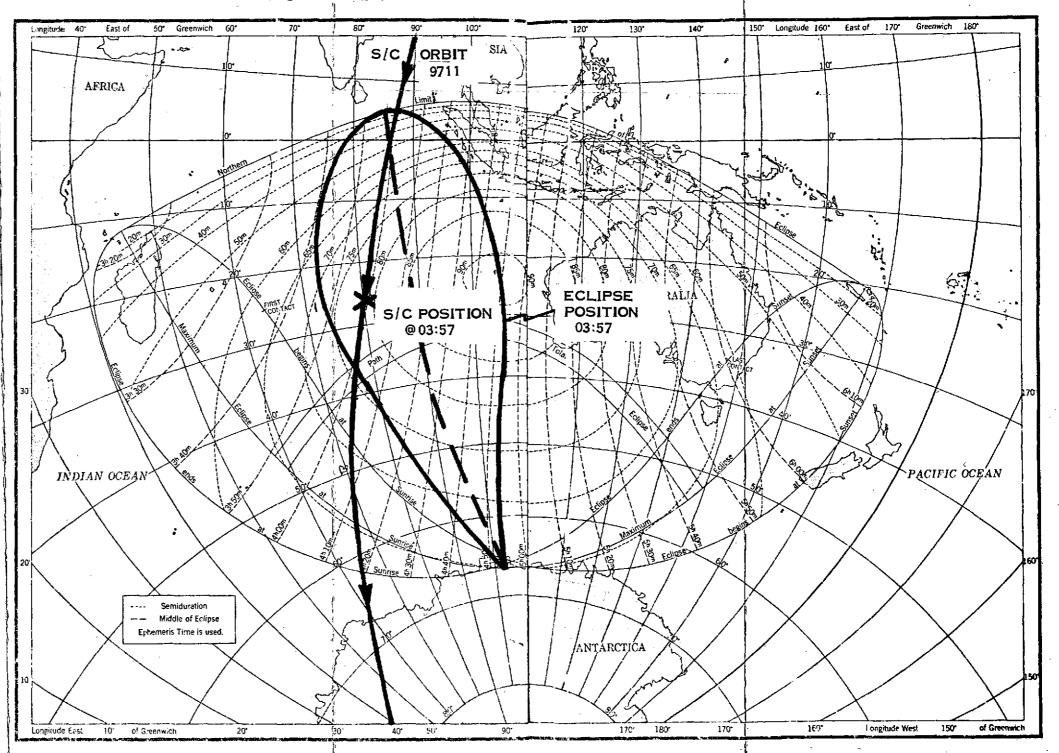


Figure 3-5. ERTS-1 Ground Trace Through Eclipse

Table 3-1. Major Power Subsystems Parameters

ORBIT NO.	26	2600	5098	7650	8912	9327	9751	10178
BATT 1 MAX	32.48	32.91	32.91	32,73	33, 08	32, 99	33, 08	33, 25
2 CHGE	32.48	32,91	32.91	32,73	33, 08	32.99	33.08	33, 16
3 VOLTS	32.48	32.91	32.99	32,73	33, 08	32, 99	33, 16	33, 25
4	32.48	32.48	32.99	32,73	. 33, 16	33.08	33,16	33, 25
5	32.48	32.99	32.99	32,82	33.16	33, 08	33, 16	33, 33
. 6 .	.32.31	3291	32.91	- 32,73-	33,_08	_ 32, 99.	33,.16	33,.25
7	32.22	32,91	32.91	32,73	33, 08	32.99	33. 16	33. 25
] 8	32.14	32.91	32,91	32,73	33, 08	32, 99	33,16	33, 26
AVERAGE	32.38	32.92	32.92	32.75	33, 10	33, 01	33, 14	33, 25
BATT 1 END-	28.81	28.12	28.30	28.04	29. 23	28, 98	28, 98	28, 98
2 OF-	28.81	28.12	28.30	28,04	29, 32	28, 98	28, 98	28,98
3 NIGHT	28.81	28.04	28,30	28.04	29, 23	28,98	28, 98	28, 98
4 VOLTS	28.89	28.12	28.38	28.04	29, 32	28, 98	28,98	28, 98
5	28.89	28.21	28.38	28, 12	29, 32 29, 23	28, 98 28, 89	29, 06 28, 98	29, 06 28, 98
6	28.81	28.04	28.30	27.95	29, 23	28,98	28,00	28,98
7	28.81 28.81	28.12 28.12	28.30 28.30	28,04 28,04	29, 23	28.98	28.98	28.98
8 AVERAGE	28.84	28.12	28.32	28,04	29, 27	28.97	28, 99	28, 99
AVERAGE .	20.04	20.11	20.02	20,01				
BATT 1 (*) CHGE	13.11	13.00	13.58	13, 14	13,78	13.82	13.84	13, 96
2 SHARE	12.93	13.00	* 13.58	*13, 14	*13,78	*13,82	*13,84	*13, 96
3 (%)	11.38	11.53	11.38	11,66	1 <b>1.</b> 99	12.02	12.22	11.95
4	12.39	12.13	11.95	12,02	12, 18	12,27	12, 40	12,28
5	12.32	12,41	11,85	12,38	11.86	11.77	11, 82	11, 93
6	12.80	12.82	12.35	12,84	11, 91	12.05	11.76	11.79
7	12.62	12.66	12.42	12.55	12, 39 12, 11	12.24 12,01	12.08 12,02	12, 13
8	12.45	12.45	12.10	12.25	12,11	12,01	12,02	11,98
BATT 1 LOAD	12.71	12.61	12,44	12,68	12, 58	12.64	12, 61	12,58
2 SHARE	12.90	13,43	13.62	13,44	13, 97	13.75	14.01	13.70
3 (%)	11.43	12,11	11.91	12.04	12, 26	12, 02	12, 32	12, 23
4 (77)	12.77	12.88	13.01	12.83	18, 35	13, 04	. 13, 10	13. 12
5	12.54	12.29	12.42	12,41	12.35	12.37	12.34	12, 60
6	12.53	12.29	12.21	12, 11	11, 43	11, 64	11, 40	11.30
7	12.80	12.27	12.41	12,41	12, 42	12, 48	12, 33	12.50
8	12.32	12.12	11.98	12.09	t1, 66	12.05	11.88	11.97
Diam's west	01 11	05.15	04.65		25, 92	24. 13	24, 40	24, 76
BATT 1 TEMP 2 IN	21.11 18.74	25.13 22.33	24.65 21,42	25,31	23.06	20. 71	21.45	20,89
2 IN 3 (°C)	18.77	20.72	20.29	21,37 20,33	21,34	20, 12	20, 64	20, 16
4	21.57	23.23	23.17	23, 28	23.86	23, 27	23, 37	23.32
5	21.82	26.77	23.85	27.62	25, 28	23, 47	23.68	24, 09
] 6	21.21	26.95	24.37	27.84	25, 87	24, 08	24, 32	24.78
7	21.41	27.18	25.01	27.62	26.43	24. 44	24. 66	24, 96
8	21.82	26,68	25.14	27.01	26, 40	24, 79	24, 91	25, 24
AVERAGE	20.81	24.87	23.49	25,05	24.77	23.13	23. 43	23.53
S/C REG BUS PWR (W)	176.8	182.3	153,4	160.0	167.9	144.8	151.2	165.6
				0.4.0	<b> </b>			<b>i</b>
COMP LOAD PWR (W)	49.0	34.8	34.8	34,8	41.9	34, 8	34, 8	41.9
(P/O S/C REG BUS PWR)				:				ĺ
P/L REG BUS PWR (W)	16.2	36.1	13.7	16.5	8.9	8.9	8.9	8.9
					ļ .			1
C/D RATIO	1.06	1.08	1.13	1, 17	1.17	1, 26	1, 27	1, 21
TOTAL CHARGE (A-M)	309.2	353.85	290.21	*291.5	,*257.8	*263,1	*270.7	*258, 3
TOTAL DISCHARGE (A-M)	290.9	327.08	256.28	249.0	220.1	209.5	213.8	214, 2
1		1	908	024	865	844	835	832
· ·	1044	1028		934		•		
S.A. PEAK I (AMP)	15.8	15.10	13.68	13,68	13.06	12.80	12, 53	12. 44
SUN: ANGLE (DEG)	-3.33	+5.15	-3.54	+5.81	-1.4	-4. 47	-4.31	-1.82
MAX R PAD TEMP (°C)	+62.0	+71.00	+68.00	+72.0	⊦ <b>64.4</b> 0	64, 40	62.00	63.20
MIN R PAD TEMP (°C)	-62.0	-56.00	-59.00	-56.0	-42, 18	-43, 39	-43. 39	-42.79
MAX L PAD TEMP (°C)	+57.9	+66.00	+60.50	+67.0	+57. 20	55, 12	54, 25	56.00
MIN L PAD TEMP (°C)	-67.0	-60.00	-64.00	-60.0	-46, 25	-47.75	-47.74	-47, 00
	<u> </u>		V27 VV,		.0, =0	-11.10		

<sup>\*</sup> After the telemetry failure in Orbit 4396 Battery 2 charge share was taken equal to Battery 1 charge as an approximation in order to derive a charge share value for each battery.

Table 3-2. Power Subsystem Analog Telemetry (Average Value for Data Received in NBTR Playback)

						Or	hits			
Function	Description	Unit	26	2600	50 <del>9</del> 8	7650	8912.	9335	9751	10182
6001	BATT 1 DISC	AMP	0.94	1.23	0.81	1,01	0, 75	0.89	0.72	0. 81
6002	. 2		0.95	1.29	*. 0.70	0.95	* .	0,00	0,00	0,00 0,80
6003	3 4		0.84	1.17 1.23	0.78 0.86	1, 02	0.75 0.79	0, 84 0, 90	0.70 0.76	0.86
6004 6005	5		0.92	1.19	0.82	0.98	0,74	0.87	0.77	0, 82
600 <b>5</b>	6		0.91	1.20	0.78	0.96	0.71	0, 81	0, 72	0, 72
6007	7		0.94	1.19	0.82	1.01	0, 74	0.85	0, 73	0.80
6008	8		0.91	1.19	0.77	0,97	0.71	0, 83	0, 71	0,78
6011	BATT 1 CHG	AMP	0.58 0.57	0.71	0.58 *	0.49	0, 53 *	0. 57 0. 79	0, 57 0, 79	0. <del>6</del> 9 0. 78
6012 6013	3		0.50	0.63	0.48	0.44	0, 47	0. 50	0, 13	0, 60
6014	. 4		0.54	0.66	0.51	0.45	0.47	0, 51	0, 52	0, 60
6015	5		0.54	0.68	0.50	0.46	0, 46	0.50	0.49	0.58
6016	6		0.57	0.70	0.52	0.48	0.46	0.50	0, 49	0, 56
6017	7		0.55	0.70	0.53	0.47	0.48	0.51	0.50	0.60
6018	8	VDC	0.55	0.69 30.74	0.52 31.24	0,46	0, 47 31, 31	0.50 -31,15	0,50 -31,50	0.58 -31,64
6021	BATT 1 VOLT 2	VDC	30.87 30.87	30.74	31.25	31.08 31.08	31, 32	-31.15 -31.15	-31.50 -31.50	-31.66
6022 6023	3		30.87	30.74	31.25	31.08	31.32	-31, 15	-31,50	-31,66
6024	4		30.90	30.77	31.28	31, 11	31, 35	-31.18	-31.54	-31.70
6025	5		30.95	30.82	31.33	31. 17	31, 41	-31, 24	-31, 59	-31.75
6026	6		30.86	30.72	31.24	31,07	31. 31	-31, 14	-31, 49	-31, 65
6027	7		30.89	30.76	31,27	31.10	31, 41	-31.18	-31.53	-31.68
6028	8	200	30.89	30.75	31,27	31, 10	31, 34	-31, 18	-31, 53	-31,68 26,09
6031	BATT 1 TEMP	DGC	21.17 18.80	25, 19 22, 44	24.48 21,29	25.38 21.51	-25.76 22,96	24. 17 21. 10	24, 39 21, 37	20, 09
6032 6033	2 3		18.76	20.80	20.17	20,36	21, 39	20, 33	20, 61	21.26
6034	4		21.57	23,20	23.04	23.30	23.96	23, 35	23, 45	23, 83
6035	5		21.84	26.86	23.77	27.68	25, 20	23, 55	23.70	24.78
6036	6		21.24	26.99	24.27	27.95	25, 69	24,08	24, 31	25,78
6037	7		21.43	27.20	24.88	27.74	26, 21	24. 35	24.63	26, 09
6038		200	21.86	26.75	25.02	27.10	26, 25	24.68	24, 91	26. 21
6040	RT PAD TEMP	DGC	25.82	27.98 33.01	27.22 33.85	33.79	21, 00 34, 00	23, 65 33, 74	26, 76 34, 13	27. 16 34. 36
60 <b>41</b> 60 <b>42</b>	R PAD V N R PAD V N	VDC VDC	33.40 33.29	32.43	33.50	33.00 32.05	32, 69	33, 23	33, 80	33, 60
6044	LT PAD TEMP	DGC	14,14	18.56	16,61	24, 89	12, 10	14. 91	18.30	19, 11
6045	L PAD V F	DVC	33.69	33.71	34,16	33.84	34, 32	34, 02	34, 44	34.67
6046	L PAD V G	DVC	33.68	33.73	34.19	33.89	34. 37	34.07	34.46	34, 72
6050	S/CUR BUS V	VDC	31.24	31.03	31.68	31.50	31, 67	-31.54	-31.90	-32,06
6051	S/C RG BUS V	VDC	24.54	24.54	24,55	24.55	24, 55	-24, 55	-24.55	-24, 55
6052	AUX REG A V AUX REG B V	VDC VDC	23.41 23.50	23,46 23,50	23.48 23.50	23.47 23.50	23, 47 23, 50	-23, 49 -23, 50	-23, 49 -23, 50	-23.47 -23,50
6053 6054	SOLAR I	AMP	14.87	13.97	12.69	12.61	23, 30 12, 04	11, 77	11.70	11, 60
6055	S/C RG BUS I	AMP	7.11	7.45	6.27	6.54	6, 86	6, 41	6, 18	6. 80
6056	S/C RG BUS I	AMP	7,11	7.46	6.27	6,53	6. 85	6, 40	6, 17	6, 79
6058	PC MOD T 1	DGC	21.82	23.53	22.23	22.65	23, 29	22, 39	22, 48	23, 22
6059	PC MOD T 2	DGC	21.68	23.08	22.53	22.72	23, 26	22.48	22, 61	23.00
6070	P/L RG BUS V	VDC VDC	24.66	24.67	24.68 31.53	24.68	24, 67	-24, 67 -31, 38	-24, 68 -31, 75	-24.68 -31.92
6071 6072	P/L UR BUS V P/L RG BUS I	AMP	31.08 0.57	30.88 1.47	0.56	31.55 0.67	31. 52 0, 36	0.66	0, 36	0,36
6073	P AUX A V	VDC	23.51	23.53	23.51	23,51	23, 50	-23, 51	-23, 50	-23.50
6074	P AUX B V	VDC	23.51	23.53	23.51	23.51	23, 50	-23.51	-23, 50	-23, 50
6075	PR MOD T1	DGC	21.50	24.40	23.13	23, 36	23, 91	22, 97	23. 02	23.62
6076	PR MOD T2	DGC	20.34	22.31	21.45	21,62	22. 12	21, 24	21, 39	21.84
6079	FUSE BLOW V	VDC	24.56	**	24.57	24.58	24, 61	-24.60	-24, 60	-24, 60
6080	SHUNT I I	AMP	0.00	0.00	0.00	0,00	0, 0	0.00	0,00 0,00	0,00 0.00
6081 6082	2		0.00	0.00	0.00 0.00	0.00 0.00	0.0	0,00 0,00	0,00	0.00
6083	4		0.00	0.00	0.00	0.00	0.0	0.00	0.00	0.00
6084	5		0.00	0.00	0.00	0.00	0.0	0.00	0,00	0,00
6085	6		0.00	0.00	0.00	0.00	0.0	0,00	0.00	0,00
6086	7		0.00	0.00	0.00	0.00	0.0	0.00	0,00	0, 00
6087	8		0.00	0.00	0.00	0.00	0, 0	0,00	0, 00	0, 00
6100	P/L RG BUS I	AMP FRM	0.58 764	1, 47 425	0.56 389	0.67	0.36 494	0, 66 421	0, 36 380	0, 36 384
TAL NO.	MAJOR FRAMES					387				

<sup>\*</sup> Function 6002, 5012; missing data resulted from disabled telemetry resulting from IC chip failure which affected charge current directly and discharge current indirectly via the power computer program.

<sup>\*\*</sup> Function 6079; missing data resulted from logic error in master information file used in computer processing.

ATTITUDE CONTROL SUBSYSTEMS

## ATTITUDE CONTROL SUBSYSTEM (ACS)

Performance of the Attitude Control Subsystem has been excellent throughout the launch and orbital operations during this flight.

Pressure/temperature ratios have all been satisfactory. The forward scanner pressure has decreased slightly since launch (4.6 PSIA at launch, 3.50 PSIA at Orbit 10182); however, it is not decreasing at a rate fast enough to cause alarm. It should reach half pressure at about Orbit 16,000.

All pneumatic gating functions are performing well with no evidence of propellant leaks. (The (+) Pitch and (-) Roll gate history is shown in Figure 4-1. There is close correlation between gating frequency and sun intensity. Usable impulse remaining is 420.35 lb-sec. (575 lb-sec. at launch).

Rate Measuring Package "2" is still performing well. The RMP heater was turned off in Orbit 8048 to lower ACS package temperatures.

A modified momentary enable gating plan is in operation to hold the pitch flywheel speed between 400 and 500 RPM to improve lubrication of the bearings. Roll, yaw, and pitch orbit average motor driver duty cycles have been nominal during this report period (5-6% for roll; 1-2% for yaw; 6-9% for pitch), except as noted, during this report period. From orbit 9290 to 9340 the pitch CCW motor driver duty cycle rose to approximately 15% orbit average and then returned to normal. From orbit 9887 to 9910 the pitch CCW motor driver duty cycle rose to approximately 25.9% orbit average and returned to normal. Spacecraft performance was unaffected. It is postulated that since the pitch CCW motor driver duty cycle returned to normal the anomaly was connected with lubrication. Other types of bearing problems would not be expected to recover to their previous low torque requirement.

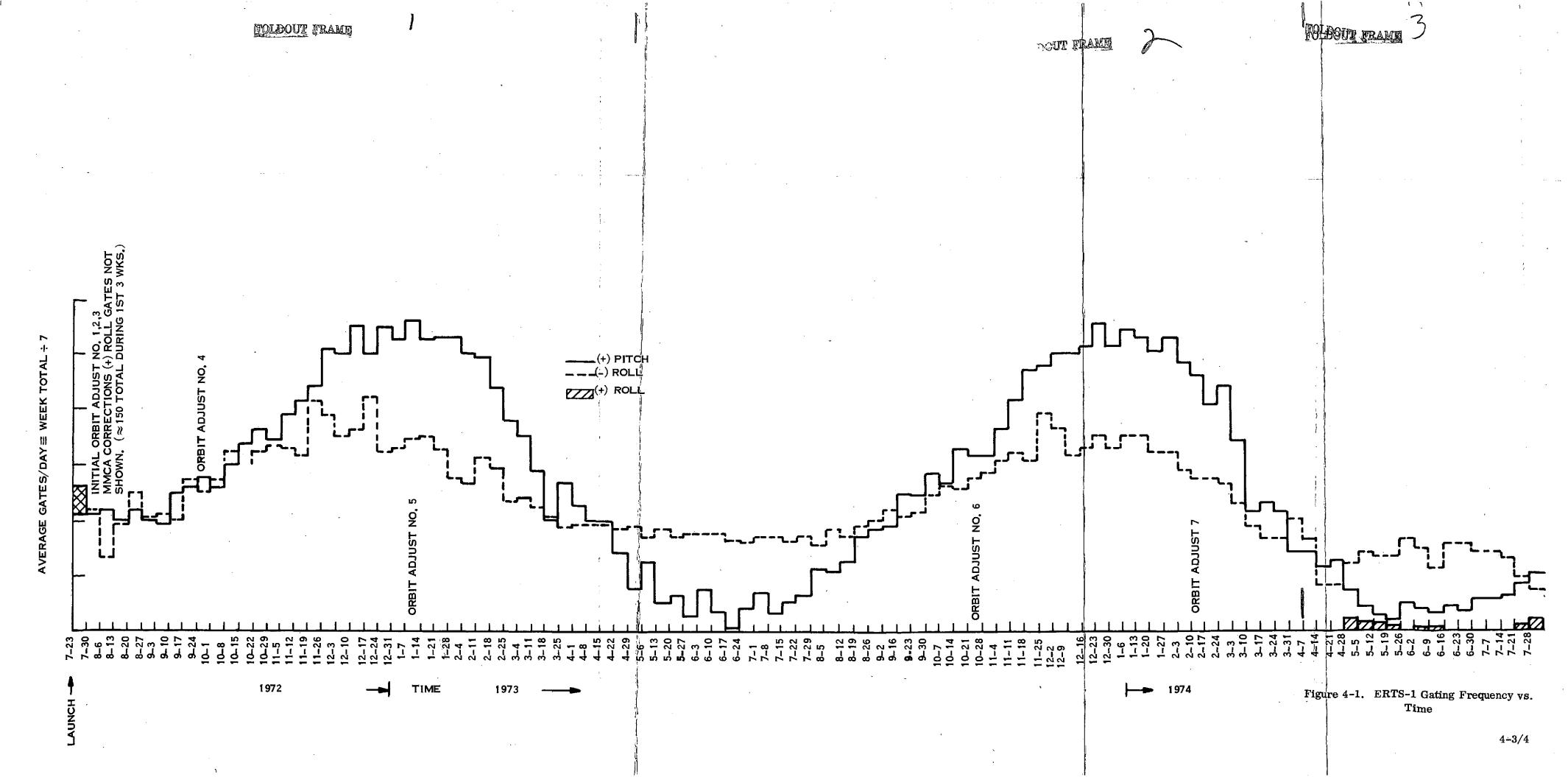
The Solar Array Drives performed well during this period.

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Table 4-1 is a summary of telemetry in the Attitude Control Subsystem.

Table 4-1. ACS Temperature and Pressure Telemetry Summary

	1	1			· · · · · · · · · · · · · · · · · · ·	rbit			
Function	Units	31	2600	5099	7650	9911	9335	9751	10182
1084 RMP 1 Gyro Temperature	DGC	44.5	24.28	23,06	25, 21	22,06	22.30	20.70	21,22
1094 RMP 2 Gyro Temperature	DGC	74.3	75,07	75,10	75,42	43.90	44.10	43.39	43,45
1222 SAD RT MTR HSING Temp	DGC	21.1	23,07	22,00	24,29	21.28	21.61	21.00	20,55
1242 SAD LT MTR HSING Temp	DGC	27.0	32,27	30.38	33,44	29,11	29.03	28.42	28.18
1223 SAD RT MTR WNDNG Temp	DGC	25.3	27,39	26,54	28, 26	25,57	25,93	25,29	24,63
1243 SAD LT MTR WNDNG Temp	DGC	28,7	34,99	32,92	35.87	31,26	31,31	30.61	30,32
1228 SAD RT HSG Pressure	· PSI	7.6	7.53	7,35	7.28	7.18	7.18	7,12	7.12
1248 SAD LT HSG Pressure	PSI	7.0	7.04	6.86	6.76	6,53	6,53	6.47	6.47
1007 FWD Scanner MTR Temp	DGC	19,8	21,35	19,88	22.26	19.36	19,47	18.84	18,46
1016 Rear Scanner MTR Temp	DGC	20,5	21,25	19,83	21.79	18.53	18.65	18.18	17.86
1003 FWD Scanner Pressure	PSI	4.6	4.52	4.02	3,84	3.55	3,50	3.50	3,50
1012 Rear Scanner Pressure	PSI	7,8	8.05	7.87	7.87	7.52	7,42	7.43	7.44
1212 Gas Tank Pressure	PSI	1988.0	1849.00	1702.34	1598.59	1487.00	1474.62	1462,25	1454.19
1210 Gas Tank Temperature	DGC	22,6	26.07	24.30	27,16	23,23	23.53	22, 89	22,56
1213 Manifold Pressure	PSI	. 56.7	57.16	57.44	57.81	58,21	58,27	58,33	58.73
1211 Manifold Temperature	DGC	21.9	25, 51	23,62	26,61	22,76	22,80	22.11	21.77
1959 CLB Power Supply Card Temp	DGC	37,1	42.22	40.54	43.34	39.75	39,93	39.09	38, 83
1057 CLB Power Supply Volts	TMV	2.8	2,79	2,78	2,79	2.79	2.78	2,77	2,78
1081 RMP 1 MTR Volts	VDC	OFF	OFF	OFF	OFF.	OFF	OFF	OFF	OFF
1082 RMP 1 MTR Current	Amps	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF
1080 RMP 1 Supply Volts	VDC	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF
1091 RMP 2 MTR Volts	VDC	-29,7	-29.63	-29,63	-29,59	-29,64	-29,63	-29,64	-29.63
1092 RMP 2 MTR Cuvvent	Amps	0.10	0.10	0.10	0,11	0.11	0.11	0.11	0.11
1090 RMP 2 Supply Volts	VDC	-23,4	-23.38	-23,41	-23.38	-23,48	-23,48	-23.49	-23,50
1220 SAD RT MTR WNDNG Volts	VDC	-4.8	-4,32	-4,25	-4.18	-4.15	-3,90	-3,84	-3,89
1240 SAD LT MTR WNDNG Volts	VDC	-4.8	-4.12	-4.09	-3,95	-3.40	~3,33	-3.43	~3,36
1227 SAD RT -15 VDC Conv.	VDC	14.9	14,90	14.88	14,88	14,90	14,88	14.88	14,89
1247 SAD LT -15 VDC Conv.	VDC	15,2	15.15	15,13	15.13	15,14	15,14	15.14	15.14
1056 CLB + 6 VDC	TMV	2.4	2,35	2,35	2,35	2.35	2,35	2,35	2,35
1055 CLB <u>+</u> 10 VDC TMV	TMV	2.75	2.75	2,75	2,75	2,74	2.74	2,74	2.74
1260 ACS Baseplate 1	DGC	25.4	29,71	27,93	31.01	26.31	26.24	25,69	25.36
1261 ACS Baseplate 2	DGC	22.9	26.42	24.73	27.76	24.00	23,99	23.38	23,00
1262 ACS Baseplate 3	DGC	23.4	25.09	23.69	26.24	22,91	23,17	22.55	21,97
1263 THO1 STS	。 DGC	-6,8	0,59	-0,97	3.97	-0,28	-1,17	-1,13	-3.41
1264 THO2 STS	DGC	-14,6	-8,81	-9,42	-3.85	-4.51	-7,72	-6.71	~8,27
1265 THO3 STS	DGC	-3.1	9.32	9.31	15.52	11,27	8, 27	8.28	7,58
1266 THO4 STS	DGC	-13,9	-2,55	2,85	4.46	-0.01	, 05	64	-1,85
1267 THO5 STS	DGC	-8,9	-0.97	-1,16	6,73	-1.64	-1.02	-1,30	-5, 17
1224 SAD R FSST	DGC	39,5	52.87	60,21	61,90	66.07	64.04	64,70	63,25
1244 SAD L FSST	DGC	27.1	45.64	51,11	56.46	55,34	52,94	53,20	53.21



# SECTION 5 COMMAND/CLOCK SUBSYSTEM

## COMMAND/CLOCK SUBSYSTEM (CMD)

Command processing for both real time and stored commands for ERTS-1 has been normal during this period.

Commanding difficulties which have been experienced have been isolated to ground transmission problems.

Missed real time commands, attributed to the logic race in the command clock design, are occasionally noted.

On rare occasions stored commands are blocked by a real time sequence being transmitted during the stored command time tag. Usually the commands interlace as expected, however, several instances have been noted when the stored command did not execute. The condition is being investigated.

The spacecraft time base, provided by the time code generator, has been well within specifications. The clock has been reset three times in orbit, at the beginning of 1973, in Orbit 5578, and at the beginning of 1974. See Figure 5-1. Clock drift is approximately 1 millisecond/orbit. A plot of accumulative drift is shown in Figure 5-2.

The changes in the subsystem are not sufficient to consider switching to alternate units from the original launch configuration. However the VHF command receiver was switched from side B to side A in orbit 10068 when the USB subsystem was switched to side B. Performance of side A is excellent and normal.

Table 5-1 gives typical telemetry values.

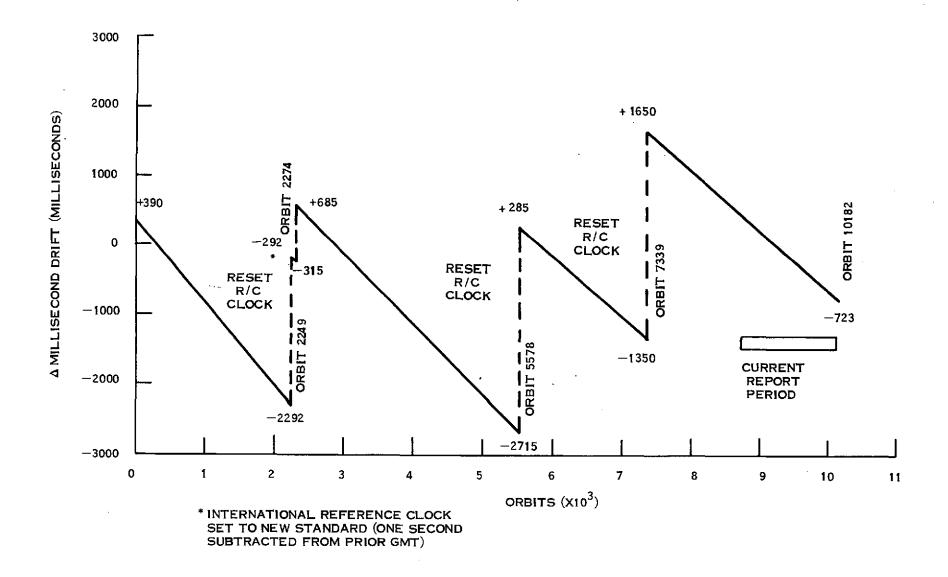


Figure 5-1. Spacecraft Clock Drift

Figure 5-2. Accumulated Clock Drift

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Table 5-1. Command Clock Telemetry Summary

							Orl	oit		_	
Function No.	Name	Mode	Units	35	2600	509 <b>9</b>	7650	8911	9335	9751	10182
8005	Pri. Power Supply Temp	-	ос	37,31	38,91	39,37	39.24	39,65	39,68	39.70	39.50
8006	Red. Power Supply Temp	_	°c	35.73	37.56	38,08	38,09	38.49	38,56	38,60	38.38
8007	Pri. Osc. Temp	_	°c	31,14	31,92	31,98	32.05	32.31	32,33	32.35	32,1
8008	Red. Osc. Temp	_	°С	30,47	31,31	31,39	31.41	31,55	31,49	31,55	31.4
8009	Pri, Osc. Output	_	TMV	0.95	0.96	0.96	0.97	0.97	0.97	0.97	$0.9^{\circ}$
8010	Red. Osc. Output	_	TMV	**	**	**	**	**	**	**	**
8011	100 kHz	Pri, - Red.	TMV	3,11	3, 11	3.10	3.11	3,11	3.11	3.11	3.1
8012	10 kHz	Pri Red.	TMV	3,10	3,08	3,07	3.08	3,08	3.08	3,08	3.0
8013	2.5 kHz	Pri, - Red,	TMV	2.95	2,95	2,95	2.95	2.95	2,95	2,95	2,9
8014	400 Hz	Pri Red.	TMV	4.40	4.40	4,40	4.40	4.40	4,40	4.40	4.4
8015	Pri, +4V Power Supply	Pri. Clk ON	VDC	4,10	4.10	4,10	4.10	4,10	4.10	4.10	4.1
8016	Red, +4V Power Supply	Red, Cik ON	VDC	3,95	3,95	3,95	3,95	3,95	3,95	3.95	3.9
8017	Pri. +6V Power Supply	Pri, Clk ON	VDC	6,06	6,08	6,07	6.07	6,08	6,07	6.07	6.1
8018	Red. +6V Power Supply	Red, Clk ON	VDC	6,00	5,95	5.94	5.94	5,94	5,94	5,94	5,1
8019	Pri6V Power Supply	Pri, Clk ON	VDC	-6.02	-6.03	-6.02	-6.02	-6,63	-6.02	-6.02	-6.0
8020	Red6V Power Supply	Red. Clk ON	VDC	-5,99	-6,00	-6,00	-6,00	-6,00	-6.00	-6,00	-6.
8020	Pri, -23V Power Supply	Pri, Clk ON	VDC	-22.38	-22,90	-22.89	-22.89	-22.90	-22,89	-22.89	-22.
8022	Red23V Power Supply	Red, Clk ON	VDC	-22.98	-23,02	-23,00	-23.00	-23.01	-23,00	-23,00	-23.
8023	Pri29V Power Supply	Pri. Clk ON	VDC	-29.13	-29,14	-29,16	-29,15	-29,15	-29.15	-29, 16	-29,
8023 8024	Red29V Power Supply	Red, Clk ON	VDC	-29,07	-29.21	-29.21	-29.21	-29,22	-29.21	-29.22	-29.
8024	CIU A -12V	CIA A ON	VDC	-12,33	-12,33	-12.33	-12.33	-12,33	-12,33	-12,33	-12.
8102	Cru B -12V	CIU B ON	VDC	-12,26	-12,26	-12,26	-12.26	-12,26	-12,26	-12.26	-12,
8103	CIU A -5V	CIU A ON	VDC	-5.32	-5.34	-5.34	-5.34	-5,34	-5, 34	-5.34	-5.
	CIU B -5V	CTU B ON	VDC	-5,31	-5,31	-5,31	-5.31	-5,31	-5.31	-5.31	-5.
8104		CIU A ON	°c	24.47	24,85	24,77	25.04	25.08	25.10	25.09	25.
8105	CIU A Temp CIU B Temp	CIU B ON	°c	24.96	25,42	25,31	25.54	25,57	25,60	25,58	25.
8106	Receiver RF-A Temp	CIU B ON	oc	**	**	**	**	**	**	**	28,
8201 8202	Receiver RF-B Temp	_	°c	27.98	28,46	28.22	28,39	28,68	28,46	28,45	**
	D MOD A Temp		°c	25,41	25, 82	25,73	25.86	26.12	25,89	25.92	37.
8203	D MOD B Temp	_	°c	35,03	35,59	35,61	35.71	35,93	35.77	35,67	26,
8204		Receiver A ON	рвм	**	**	**	**	**	**	**	-96.
8205	Receiver A AGC Receiver B AGC	Receiver B ON	DBM	-94.74	-89.91	-84.67	-89.05	90.65	-88,96	-97,12	**
8206	· ·	Receiver A ON	TMV	**	**	**	**	**	**	**	2,
8207 8208	Amp, A Output Amp, B Output	Receiver B ON	TMV	2.81	2,81	3,22	2.92	2,72	2.89	2.71	**
8209	,	Receiver A ON	TMV	**	**	**	**	**	**	**	1.
	Freq. Shift Key A OUT	Receiver B ON	TMV	1,10	1,10	1,11	1.11	1.10	1,10	1.10	**
8210	Freq. Shift Key B OUT	Receiver A ON	TMV	**	**	**	**	**	**	**	1.
8211	Amp, A Output		TMV	1,13	1,14	1.13	1,13	1,13	1,13	1,13	**
8212	Amp. B Output	Receiver B ON	TMV	**	**	**	**	**	**	**	5
8215	D MOD A -15V	Receiver A ON	1	1	5,00	5.00	5.00	5,00	5,00	5,00	**
8216	D MOD B -15V	Receiver B ON	TMV	5.00	**	**	**	**	**	**	5.
8217	Regulator A -10V	Receiver A ON	1		5,50	5,50	5.50	5.50	5,00	5.50	**
8218	Regulator B -10V	Receiver B ON	TMV	5.50	0,50	3.50	3.50	0.50			

<sup>\*\*</sup>Units not in use

SECTION 6
TELEMETRY SUBSYSTEM

## SECTION 6 TELEMETRY SUBSYSTEM

The Telemetry Subsystem was launched in the ON mode and has been operating continuously since then providing data from the spacecraft either to ground stations, the narrow band recorders, or both. Typical telemetry values are given in Table 6-1. Only memory Section 0.0 has been used in the telemetry matrix. Total performance has been excellent except for one integrated circuit chip failure, containing four functions (6012, 1011, 12238, 7010) in Orbit 4396.

Table 6-1. TLM Telemetry Summary

Function		-			Orl	bit	·			•
No.	Function Name	Unit	35	2600	5099	7650	8911	9335	9751	10182
1000	Memory Sequencer A Converter	VDC	6,35	6.34	6. 33	6.33	6, 33	6. 33	5. 39	6.33
9002	Memory Sequencer B Converter	VDC	**	**	4*	**	••	**	.**	••
9003	Memory Sequencer Temp.	o <sub>C</sub>	19.59	21.47	21.96	22,67	22.11	21, 15	21.11	21,76
9004	Formatter A Converter	VDC	5.99	5.99	5.99	5.99	5, 99	5.99	5, 99	5,99
9005	Formatter B Converter	VDC	**	++	**	**	**	**	**	**
9006	Dig, Mux A Convertor	VDC	10.01	10.07	10.04	10.07	10,07	10.06	10. 0G	10.07
9007	Dig, Mux B Converter	VDC	**	**	**	**	**	••	**	••
9008	Formatter/Dig. Mux Temp.	°C	22.50	27.34	24,89	27.97	28,19	25,00	24. 87	24,96
9009	Analog Mux A Converter	VDC	26.01	26. (8	21,18	26.18	26.18	28, 18	26, 19	28,20
9010	Analog Mux B Convertor	VDC		**	••	**	**		**	••
9011	A/D Converter A Voltage	VDC	10,00	10.07	10.07	10.07	10,07	10,07	10, 07	10, 07
9012	A/D Converter B Voltage	VDÇ	**	**	••	**	**	••	••	••
9013	Analog Mux A/D Converter	°c	25.00	27.50	26.83	29.43	28, 46	27. 26	27, 31	27.25
901-1	Preregulator A Voltage	VDC	19.93	19.99	19.95	19.19	19,99	19.95	19, 94	19, 28
9015	Preregulator B Voltage	VDC	++	**	**	**	**			
9016	Reprogrammer Temp.	°C	22.00	25.00	22.50	26.05	25,72	22.50	22,52	24,13
9017	Memory A Converter	VDC	8, 00	6.00	ñ.99	6.00	6,00	G. 00	6,00	6,00
9018	Memory A Temp.	°c	17.51	19.06	17.50	19.00	18,63	17.50	17, 50	18,98
9019	Memory B Converter	VDC	**	**	**	**	**	<b></b> .		**
9020	Memory B Temp.	°c	17, 68	19.29	17.63	19.82	19.57	17.54	17.69	19.09
9100	Reflected Power (Xmtr A)	dBm	11.95	12,75	12.32	13.11	13.14	12, 32	12.31	12.32
9101	Xmtr A -20 VDC	VDC	-19.75	-19.78	-19.76	-19.78	-19,78	-19,76	-19.76	-19,76
9102	Xmtr B -20 VDC	VDC	**	**	**	**	<b>*</b> *		••	**
9103	Xmtr A Temp.	°C	20, 95	24, 06	21,14	25.24	25, 80	21.20	21, 17	21,55
9104	Xnitr B Temp.	°c	21.69	25. 02	21,95	26.36	26, 99	21,95	21, 92	22,31
9105	Xmtr A Power Output	dBm	25. 12	25.36	25.35	25.38	25, 40	25.24	25.24	25,24
9106	Xmtr B Power Output	d Bm	++	**	**	**	**			**

<sup>\*\*</sup> Units not used since prelaunch

## SECTION 7 ORBIT ADJUST SUBSYSTEM (OAS)

### ORBIT ADJUST SUBSYSTEM (OAS)

The Orbit Adjust Subsystem has been fired seven times prior to this report period (all from the (-)X thruster). There are 64.87 pounds of hydrazine fuel remaining from an initial pre-launch fuel load of 67.00 pounds. Table 7-1 is a summary of OAS performance to date and Table 7-2 gives average telemetry values for the off quiescent state. Figure 2-2 shows spacecraft ground track drift from standard orbit tracks and the effects of orbit adjust to correct and hold the drift to pre-determined limits.

Table 7-1. Orbit Adjust Performance

Orbit	Burn Time (sec)	+ A a (meters)	Average SMA (2) (KM)	Performance · % of Plan	N <sub>2</sub> H <sub>4</sub> Used Lbs. (3)
(1)			7281.461	·	
38	4.8	12	7281.484	60.0	0.018
44	251.0	1975	7283.456	103.5	0.934
59	318.0	2381	7285.838	. 101.5	1.19
938	12.8	98	7285.877	110.0	0.039
2416	20.4	154	7285.877	106.0	0.071
6390	14.8	110	7285.786	100.0	0.048
7826	14, 8	112	7285. 763	101.8	0.048
		4		1	

<sup>(1)</sup> After Injection

Table 7-2. OAS Telemetry Values

T-vestion.		ĺ	Orbit								
Function No.	Name	Units	35	2600	5099	7650	8911	9335	9751	10182	
2001	Prop. Tank Temp.	°c	22.03	23.91	22.86	24,53	23. 69	22.86	22. 86	23, 28	
2003	Thrust Chamber No. 1 (-x) Temp, (1)	°c	29.57	28.50	29.93	27.77	31. 49	32,88	32, 75	30, 55	
2004	Thrust Chamber No. 2 (+x) Temp. (1)	°c	38.76	33.74	40.28	39.27	42.03	38.05	38, 85	38.91	
2005	Thrust Chamber No. 3 (-y) Temp. (1)	°c	34.55	46.23	34.41	47.52	38, 67	33.88	34, 10	36, 09	
2006	Line Pressure	Psia	539.29	486.87	486.74	491.10	490, 61	486, 87	486, 84	490. 61	

Wide spread of temperature is due to nozzle locations and satellite day/night transitions relative to data averaged. Typical orbital range is from 19 to 59 DGC.

<sup>(2)</sup> Semi-Major Axis

<sup>(3)</sup> Initial fuel load 67.0 pounds

## SECTION 8 MAGNETIC MOMENT COMPENSATING ASSEMBLY (MMCA)

## SECTION 8 MAGNETIC MOMENT COMPENSATING ASSEMBLY (MMCA)

The spacecraft was corrected for unbalanced magnetic moments in Orbits 73, 85, 110 and 220. Adjustments were made in the pitch positive. The unit responded well as noted in Table 8-1 and has held its charge. The current dipole values are Pitch: +2950 Pole-Cm; Roll: zero; Yaw: zero. These values are unchanged since Orbit 220. Table 8-2 gives typical telemetry for the MMCA.

Table 8-1. MMCA Telemetry Before and After Adjustment

					0	rbits		<del>-</del>	1
Function	Units	72	75	83	88	106	115	218	224
4003	TMV	3.49	3,48	3.48	3,48	3.47	3.49	3.50	3.50
4004	TMV	3. 11	3.11	3, 11	3.11	3.11	3, 11	3.11	3, 11
	Pole-Cm	≈ 0	≈0	≈0	≈0	≈0	≈0	≈0	≈0
4005	TMV	3. 13	2.87	2, 87	2.77	2.77	2.65	2.65	2,52
	Pole-Cm	≈0	1200	1200	1800	1800	2350	2350	2950
4006	TMV	3. 18	3.20	3.20	3, 20	3. 18	3.18	3. 18	3. 18
	Pole-Cm	≈ 0	≈0	≈0	≈0	≈0	≈0	≈0	≈0

Table 8-2. MMCA Telemetry Summary

			Orbits							
Number	Name	Units	35	2600	5099	7650	8911	9335	9751	10182
4001	Al Board Temp	°C	19.77	19.37	19.03	19.12	19. 23	19.03	19. 11	19, 11
4002	A2 Board Temp	°c	23.58	23.36	23. 05	23, 15	23, 17	23.07	23, 15	23.13
4003	Hall Current	TMV	3.48	3.49	3.48	3,48	3, 47	3.48	3.48	3,48
4004	Yaw Flux Density	TMV	3.11	3.10	3. 11	3,13	3,14	3.14	3.14	3.15
4005	Pitch Flux Density	TMV	3, 13	2.50	2.51	2.52	2, 52	2,52	2, 52	2,52
4006	Roll Flux Density	TMV	3.19	3.20	3.19	3,19	3.20	3,20	3,20	3,20

## SECTION 9 UNIFIED S-BAND/PREMODULATION PROCESSOR

### UNIFIED S-BAND/PREMODULATION PROCESSOR

The Unified S-Band (USB) Subsystem has operated satisfactorily since launch, despite repeated and large drops in transmitter power output. The B transmitter/receiver section of the USB dual installation was substituted for the A-section during Orbit 10068 restoring full 1.5 watts output to this subsystem from the 0.14 watts to which it had declined, as shown in Figure 9-1.

The USB-A Receiver was ON continuously from launch to mid-orbit 10068, for a total of 17, 327 hours.

The USB-A Transmitter was ON only during station passes from launch to mid-orbit 10068, for a total of 2253 hours. It was commanded ON for transmission of real time telemetry, play-back of stored telemetry, ranging data for computation of ERTS-A ephemeris, and for relay of DCS data.

The USB-B Receiver has been ON continuously since Orbit 10068 for a total of 198 hours. The USB-B transmitter has been ON for a total of 26 hours.

Table 9-1 lists telemetry values, all normal, and typical for orbits in this reporting period.

On 19 March 1974 during Orbits 8421 to 8424 (Figure 9-1), the USB-A transmitter power dropped to 0.192 watts. At this level, the range for USB relay service for the DCS subsystem had substantially shrunk from the horizon. A description of this shrinkage is given in Appendix C. When the USB output again declined in Orbit 10058 to a value of 0.140 watts, the B section was substituted. Ground stations reported an immediate 10 dB rise in AGC levels, corresponding to the telemetry-indicated rise of power output to 1.5 watts shown in Figure 9-1.

Table 9-1. USB/PMP Telemetry Values

					Telem	etry Value	)		<del></del>
	Function		L			Orbit			
No.	Name	Units	35	2566	5099	7650	9335	9752	10182
11001	USB Revr. AGC	DBM	-122.78	-126, 18	-131.99	-132.00	-121.10	-131, 18	-132,00
11002	USB Trans. Pwr	WTS	1.60	0.62	0.29	0.26	0.19	0.18	1.55
11003	Receiver Error	KHZ	21.79	-20, 87	-21.32	-21, 63	-22, 22	-22, 18	-21.46
11004	Trans. Temp.	DGC	22, 92	25, 30	22.64	25.71	23, 25	22.76	24.73
11005	Trans. Pressure	PSI	15, 91	16,09	15, 91	16, 06	15, 89	15, 82	15, 92
11007	Trans A-15VDC	VDC	-15.20	-15, 20	-15.20	-15, 20	-15, 20	-15, 20	**
11009	Ranging-15 VDC	VDC	-14.76	-14, 76	-14.76	-14,76	-14.76	-14.76	-14.60
11101	PMP A Volt	VDC	-15, 12	-15.18	-15.18	-15, 19	-15.09	-15,18	**
11103	PMP A Temp.	DGC	30.44	33,70	30,23	34, 93	31.02	30, 15	**
11102	PMP B Volt	VDC	**	**	**	. **	**	**	-15, 12
11104	РМР В Тетр	DGC	**	**	**	**	**	**	30.76
11008	Trans B-15VDC	VDC	**	**	**	**	**	**	-15, 20

<sup>\*\*</sup> Unit Not In Use.

Figure 9-2 is the recorded AGC signal at Alaska on two receivers, shown in Channels 2 and 3. Telemetry and command link was maintained via VHF shown on Channel 4. The 10 dB rise can be seen at 17:55:37 when the change-over occurred. As additional change-overs occurred in the Pre Modulation Processors and in the Command Integration Channels, USB lock was lost for about 30 seconds until it could be re-acquired by the Goldstone ground station whose horizon the spacecraft was just entering.

Figure 9-3 shows AGC readings at Goldstone for a constant reference orbit in each cycle since launch, resulting in each curve having all data points in the same range, elevation and azimuth. The AGC difference (8 dB) between the curves for the two distances shown is caused by the dual effects of doubling the distance (6 dB) and using a different section of the USB antenna pattern. The effect of the power decline of the USB transmitter can be seen, as well as the (single-point) rise after switch-over to USB-B.

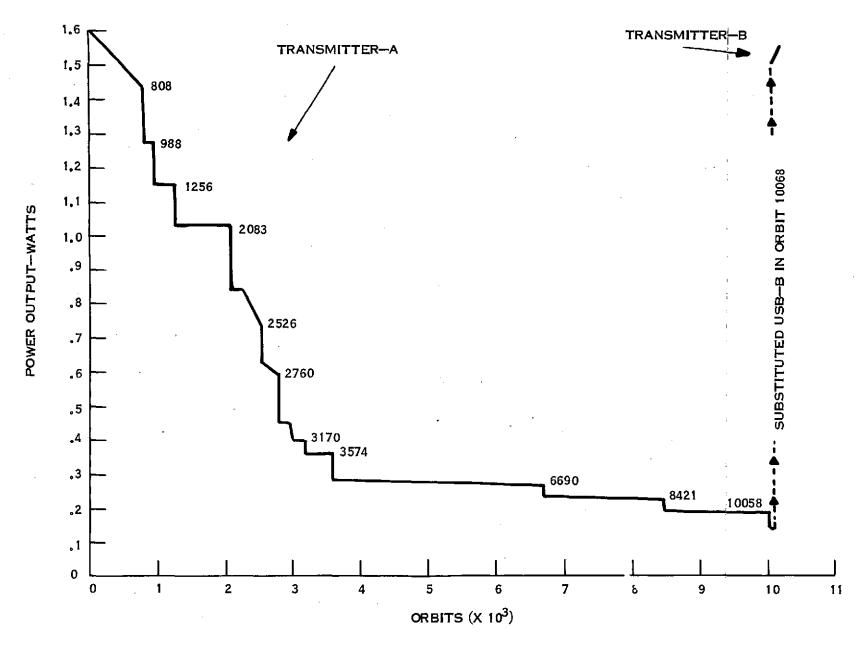
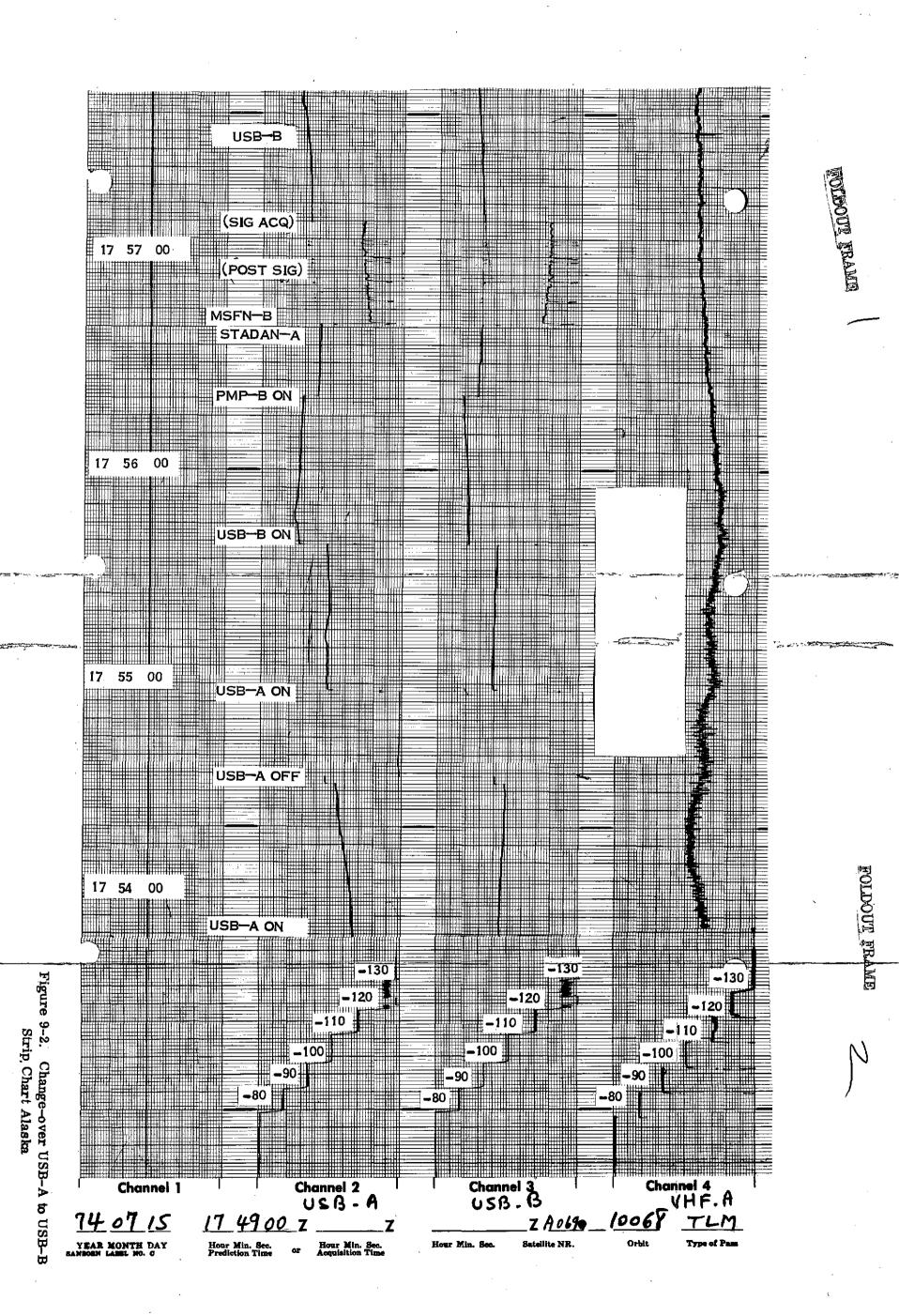


Figure 9-1. USB 2-Year Power Output History



9-5/6

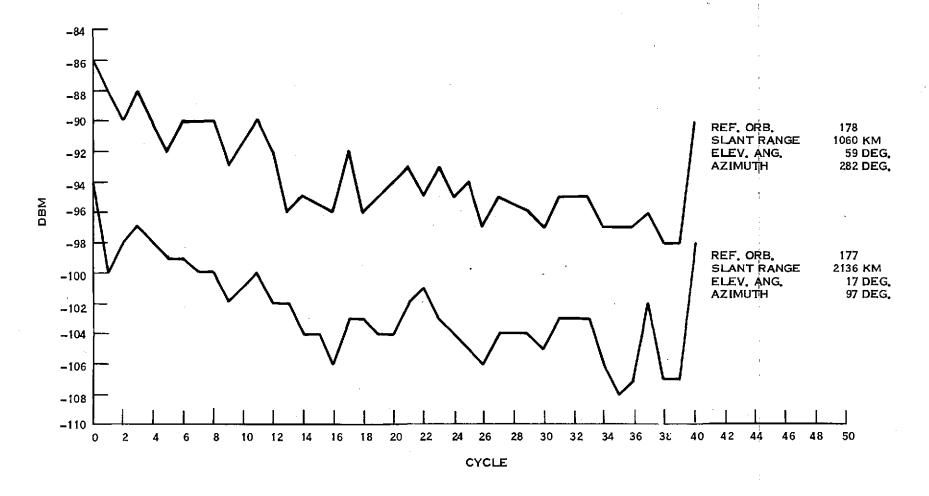


Figure 9-3. USB AGC Readings at Goldstone with 30-Foot Antenna

## SECTION 10 ELECTRICAL INTERFACE SUBSYSTEM

#### ELECTRICAL INTERFACE SUBSYSTEM

Auxiliary Processing Unit (APU) consists of Search Track Data, Time Code Data, and Back-up-Timers-which-operated satisfactorily-throughout this report period. Telemetry for the APU is shown in Table 10-1. The APU is in Normal mode.

Table 10-1. APU Telemetry Functions

			Orbit .							
Functions	Description	Unit	7	2600	5098	7650	8911	9335	9751	10182
13200	APU, -24.5 VDC	VDC	-24.90	-24.90	-24,90	-24, 91	-24.91	-24.90	-24.90	-24. 91
13201	APU, -12 Volts	VDC	-12.08	-12.08	-12.08	-12.07	-12.07	-12.07	-12.07	-12.07
13202	APU Temp.	DGC	25.49	28.50	26.95	29.21	27.65	27, 25	27.05	27.15

The Power Switching Module (PSM) contains the switching relays for power to Orbit Adjust, MSS, WBVTR No. 1 and No. 2, RBV and PRM. The MSS and WBVTR No. 1 power circuits have been operated on a regular basis throughout this report period. The power relay for the RBV remained in a failed closed condition since Orbit 196, but the RBV remained off by relays in the camera subsystem. The WBVTR No. 2 remained off due to the failure occurring in Orbit 148. All switching during this report period was normal.

The Interface Switching Module (ISM) performed all switching normally during this report period. Compensation Loads changes were exercised in this report period as reported in Table 11-2.

## SECTION 11 THERMAL SUBSYSTEM

#### THERMAL SUBSYSTEM

The Thermal Subsystem has maintained spacecraft temperature control over a satisfactory range during this report period. Table 11-1 shows average analog telemetry values from data recorded on the NBTR. During this report period, the sun angle varied as shown in Figure 3-3 and the intensity decreased as shown in Figure 3-4 for day 114 to 204. Figure 11-1 shows a typical thermal profile for average bay temperatures of the sensory ring in this report period. The values are consistent with the limits established through two years of orbital operation.

Compensation Load History is shown in Table 11-2. In Orbits 8928, compensation load number 3 was turned off when the Wide Band Electronic Unit 1 resumed normal operation. In Orbit 9898, compensation load number 3 was turned on again to keep the Wide Band Electronic unit 1 temperature in normal limits while it was off during investigation. Normal operation had not resumed at the end of this report period.

FOLDOUT TRAME

Table 11-1. Thermal Subsystem Analog Telemetry (Average Value for Frames of Data Received in NBTR Playback)

_										<del></del>		1
		Function			•	O	rbits				1	
}	Function		TT. +4.	0.0	DC00	E000	7650	8912	0005	0.7.7.1		
	No.	Description	Unit	26	2600	5098	1,090	0912	9335	9751	10182	
٠ }						-						
]	7001	THM TH01 STI	DGC	19.52	22.18	20.85	22.24	21, 81	20.53	20.62	21.65	
	7002	THM TH02 SBO	DGĆ	18.60	20.55	19.95	20.38	20, 85	19, 93	19,98	20.60	
ŀ	7003	THM TH03 STI	$\mathbf{DGC}$	18.48	21.79	20.16	20.83	21, 19	19.83	19.91	20.87	
	7004	THM TH03 SBI	DGC	19.47	21.11	20.25	21.50	20.80	20.51	20.45	20.36	ļ
ł	7005	THM TH04 STI	DGC	18.39	21.17	19.71	20.12	20.67	19,55	19,65	20.35	l
	7006	THM TH05 SBO	DGC	17.57	19.04	18.39	18.55	18.98	18.30	18.46	18.81	l
	7007	OA -X THRUSTER	$\mathbf{DGC}$	21.95	22.38	22.95	22.55	23.06	23, 32	23.37	22.90	
	7008	THM TH07~STO	DGC	15.95	17.09	16.61	16.72	17.14	16.58	16.65	16.90	ROPORTOR
	7009	THM TH06 SBI	DGC	19.38	21.05	20.35	21.04	21, 11	20.28	20,49	20.93	
I	7010	THM TH07 STI	DGC	18.61	19.79	*	*	*	*	*	*	Ιč
	7011	THM THOS STO	DGC	21.78	22.52	22.77	22.61	23, 05	23.06	23, 11	22.88	, ,
	7012	THM TH09 SBI	DGC	21.81	23.10	22.87	23.32	23, 43	23.19	23. 19	23.08	NKAME
	7013	THM TH10 SBO	DGC	18.73	19.87	19.53	20.04	19,77	19.72	19.79	19,64	S
- 1	7014	THM TH11 STI	DGC	22.37	24.52	23.35	25.01	24.09	23, 57	23.49	23, 57	
ŀ	7015	THM TH12 SBO	DGC	22.37	25.36	23.17	25.95	23, 71	23.26	23.09	23.03	ille-3
. [	7016	THM TH13 STI	$\mathbf{DGC}$	20.95	24.55	22.02	25.37	22, 97	22.09	21.95	22.47	-
- 1	7017	RBV BEAM CTR LN	$\mathbf{DGC}$	21.53	23.30	22.62	23.72	23. 31	22.90	22,86	22.84	
J	7018	THM TH14 STO	$\mathbf{DGC}$	20.38	24.77	21.40	26.10	22.39	21.29	21.27	21.93	
- 1	7019	NBR RAD OUTBD B4	$\mathbf{DGC}$	5.09	6.06	5.86	6.10	6. 17	5.91	6.00	6,00	
ı	7020	THM TH15 SBI	$\mathbf{DGC}$	21.14	26.21	23,24	27.39	24. 29	23.03	23.19 22.81	23.99 23.68	
1	7021	THM TH16 STI	DGC	20.73	25.44	22.90	26.30	23, 96	22, 65 22, 37	22.54	23.56	
ı	7022	THM TH17 SBI	DGC	20.22	25.18	22.76	25.72	23.76 25.40	24.06	24.17	25.19	
	7023	THM TH18 SBO	DGC	21.90	25.79	24.29	26.55	17.64	16.81	16, 93	17.42	i
- [	7030	THM THOS BUR	DGC	16.05	17.89	17.07	17.01 14.15	14.51	14.13	14.19	14.28	l
1	7031	THM TH06 BUR	DGC	13.59	14.49	14.17 20.75	20.83	20.93	21.03	21.05	20.74	i
I	7032	THM THIS BUR	DGC . DGC	19.92	20,61 24,59	20.75	20.83 25.25	22.58	22.12	22.06	22.76	ļ
	7033	THM TH12 BUR	DGC	21.51 19.70	24.59 24.36	21.67	25.25 25.92	23, 18	21.64	21.53	22.38	1
1	7034	THM TH15 BUR	DGC	20.11	24.36 22.45	21.36	23.10	22.59	21.24	21.12	22.02	1
[	7035 7040	THM TH18 BUR THM TH01 TCB	DGC	20.11 19.27	22.45	20.46	21.59	21.42	20.18	20.32	21.26	1
	7040 $7041$	THM THOI TCB THM THO2 TCB	DGC	17.99	20.00	19.23	19.60	20.06	19.03	19.16	19.89	1
1	7041	THM THO2 TCB	DGC	18.34	21.83	19.94	20.12	21, 22	19.60	19.84	20.92	1
l	7042	THM THOS TOB	DGC	18.95	20.71	19.94	20.03	20, 50	19.80	19.88	20.26	ĺ
	7043	THM THOS TCB	DGC	16.27	17.45	16.98	17.09	17.54	16.91	17.03	17.32	
	7045	THM THOT TCB	DGC	18.41	19.36	19.21	19.27	19.73	19.34	19.42	19.45	ļ
.	7046	THM TH09 TCB	DGC	19.38	20.52	20.37	20.51	20.87	20.57	20.59	20.64	ŀ
ı	7048	THM TH11 TCB	DGC	21.98	24.32	22.94	24.92	23.64	23, 18	23.11	23.18	
•	7049	THM TH12 TCB	DGC	21.92	25.10	22.46	25.61	23, 13	22,52	22.20	22.35	
ı	7050	тнм тн13 тсв	DGC	21.21	25.22	21.99	26.29	22.81	21.91	21, 86	22.29	ł
	7051	тнм тн14 тсв	DGC	21.38	26.19	22.88	27.41	24.04 25.27	22, 66 23, 51	22.74 23.86	23,62 25,13	ĺ
-jne		THM TH16 TCB	. <u>DG</u> C	21.30	26.65	23.95	$\begin{array}{r} 27.72 \\ \hline 26.41 \end{array}$	25. 13	23.67	1	=25:02	-,-,-
J	7053	THM TH17 TCB	DGC	21.73	25.74 22.99	24.03 22.20	23.33	23. 22	21.87	22.07	23.35	
	7054	THM TH18 TCB THM SHUTTER BY 1	DGC DEG	20.02 25.85	43.64	33.12	43.03	40.15	31, 29	32, 01	38.62	[
Ì	7060 7061	THM SHUTTER BY 2	DEG	6.62	13.88	8.65	13.85	15.00	12.11	10, 97	13,28	1
_	7062	THM SHUTTER BY 3	DEG	10.96	38.14	23.58	24.46	34, 13	22.48	22, 91	30.24	١,
	]	THM SHUTTER BY 4	DEG	30.60	38.29	35.71	35.41	39.17	36.26	36.95	37.92	A COLUMN
	7063 7064	THM SHUTTER BY 5	DEG	15.03	16.	16.25	16.25	15, 62	15.06	14.69	15,00	1
1	7064	THM SHUTTER BY 7	DEG	17.14	21.	24.64	24.14	<b>21.43</b>	21.43	20.93	21.96	
	7067	THM SHUTTER BY 9	DEG	33.26	38.45	38.44	38,73	39, 88	38.48	38, 94	39.50	
	7068	THM SHUTTER BY 10	DEG	24.68	33.65	28.68	36.36	30. 83	31,25	26.47	27,31	
1	7069	THM SHUTTER BY 11	DEG	39.66	55.79	46.89	59.06	52. 59	49.23	48.33 45.05	48.96 45.68	
	7070	THM SHUTTER BY 12	DEG	43.81	55.84	46.63	61.36	51,75 47,44	47.74 44.87	44.08	44.79	ŀ
	7071	THM SHUTTER BY 13	DEG	40.39	<b>59.</b> 02	46.38	59.61	44.26	41.03	37. 53	41.91	1
	7072	THM SHUTTER BY 14	DEG	34.20	62.55	39.70	70.80	65. 57	59.03	59.73	64.79	l
	7073	THM SHUTTER BY 15	DEG	45.40	75.54	58.74	80.38	53, 29	44.76	47.15	53, 54	1
	7074	THM SHUTTER BY 16	DEG	24.50	59.81 66.93	48.46 54.96	62.87 70.35	62.46	52.77	54.70	61.88	
	7075	THM SHUTTER BY 17	DEG DEG	39.06 29.70	48.57	43.15	49.89	49.43	40.32	41.71	51.20	] [[]
ļ	7076	THM SHUTTER BY 18 THM Q1 T ZENER V	VDC	8.19	8.19	8.19	8.19	8, 19	8.19	8, 19	8.19	18
	7080	THM Q1 I ZENER V	VDC	8.40	8.40	8.40	8,40	8,40	8.40	8, 40	8.40	
	7081 7082	THM Q2 T ZENER V	VDC	8.31	8.32	8.31	8.32	8.32	8.32	8, 32	8.32	LOTPOAL
	7083	THM Q1 S ZENER V	VDC	8.31	8.35	8.32	8.36	8, 35	8.33	8, 32	8.35	
	7084	THM Q2 S ZENER V	VDC	8.19	8.21	8.19	8.21	8, 20	8.19	8. 19	8.20	
	7085	THM Q3 S ZENER V	VDC	8.15	8.16	8.15	8.15	8.15	8.15	8, 15	8, 15	1
′.	7090	THM PSM MOUNT	DGC	21.60	23.78	22,54	24.32	23.43	22, 72	22, 71	22.98	RAME
	7091	THM IND ATTITUDE	DGC	19.40	21.07	20.42	20.95	21.22 $17.76$	20, 55 17, 54	20.65 17.57	20.88 17.47	医
	7092	THM RBV RADIATOR	DGC	15.65	17.89	17.22	18,55 22,01	22, 35	21. 93	21. 91	21.87	1-
	7093	THM RBVC CTR BM	DGC	20.30	22.49 17.10	21.61 15.71	23.01 17.61	16.42	15. 64	15, 69	16.07	
	7094	THM WBVTR ROOT	DGC	12.96	8.66	8.17	9.97	9. 29	8. 53	8, 37	8,68	
	7095	THM WBVTR RAD CT	DGC DGC	4.81 16.62	21.06	19.32	21.16	20.00	19.11	19.09	19,66	1/3
	7096	THM WBVTR STRAP THM WB MT BAY 1	DGC	20.56	22.36	19.52	21.11	21.75	18.66	18, 34	21.37	17
	7097 7098	THM WB MAT BAY 1	DGC	20.22	21.05	18.90	20.78	20.76	18.42	18.28	20, 39	1
	7099	THM WB MAT BAT T	DGC	18.60	22.32	20.55	21.49	21, 38	20.16	20. 18	21.05	1
	7100	THM WBVTR SEP 17	DGC	21,31	26.15	23.66	26.28	24,48	23.21	23, 28	24.23	
	7101	THM WBVTR 1 DENT	DGC	21.49	25 <b>.9</b> 5	23.72	25.50	24.30	23.22	23. 19	24.01	
	7102	THM WBVTR 2 BAY	DGC	17.46	20.04	18.92	19.66	19, 67	18.79	18, 89	19.32	}
	7103	THM WBVTR 2 BY 15	DGC	21.00	25.65	23.16	26.44	24. 18	22.96	23, 08	23, 82	1
	7104	THM WBVTR 2 CTR	DGC	19.35	23.50	21.51	23,60	22.21	21.30	21, 31	21.81 19.79	
	7105	THM NBTR B SEP 6	DGC	18.06	20.17	19.30	20.22	19, 99 23, 40	19.31 22.31	19.48 22.33	22,89	1
	7106	THM NBTR B SEP 1	DGC	20.82	24.88	22.35	25.78 22.86	23.40	21.05	21.06	21.34	ľ
	7107	THM NBTR BM CTR THM MSS MOUNT 14	DGC	19.37 19.18	22,44 23,89	21.04 21.15	24.79	22, 27	21.09	21.17	21.70	J
	7108 7109	THM MSS MOUNT 14 THM OA -Y THRUSTER	DGC DGC	19.18	28.11	23.80	29.56	25. 22	23,69	23. 81	24.69	I
	7109 7110	THM OA -Y THRUSTER THM MSS WBVTR BM	DGC	18.14	21.29	20.06	21.57	20, 90	20.08	20.21	20.53	
	7111	THM OA +X THRUSTER	DGC	20, 30	23.43	19.92	21.55	21.47	19.40	19.34	21.22	{
	7130	THM AVX P1 T	DGC	15.69	11.23	8.49	12.76	-3, 34	6.34	8.35	-18, 90	
	7131	THM AVX P2 T	DGC	10.63	3.63	1.59	23,20	0.39	1.07	2, 56	.41	
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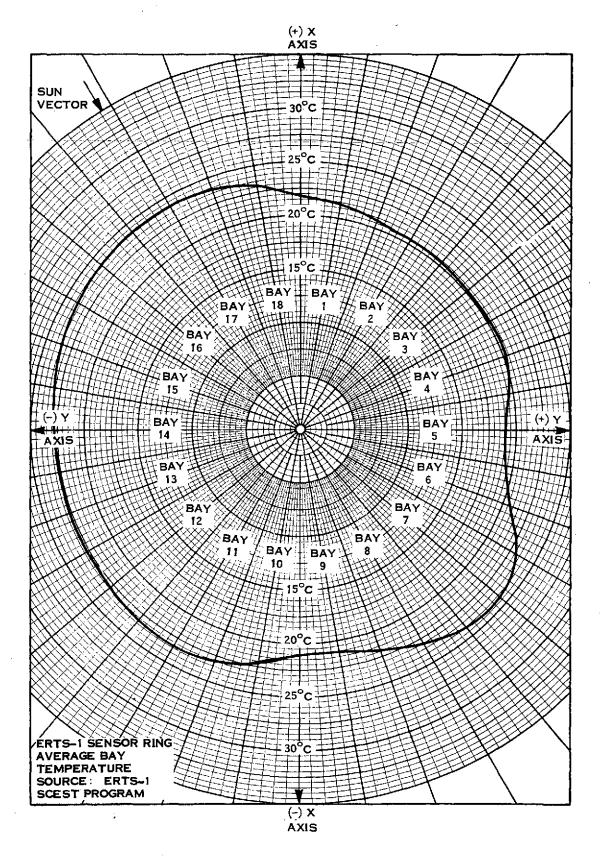


Figure 11-1. Sensory Ring Thermal Profile

Table 11-2. Compensation Load History

		Com	pensatio	Load St	atus *			
ORBITS	1	2	3	4	5	6	7	8
Launch	0	0	0	0.	0	0	0	0
2	0	0	x	x	х	0	х	ж
6	x	×	ж	х	х	0	x	x
118	0	0	0	0	0	0	0	0
156	х	ж	x	x	х	. 0	х	x
194	0	0	0	0	0	0	0	0
197	x	x	х	x	х	0	х	x
701	x	x	0	х	x	0	′x	x
1410	x ·	x	0	x	x	0	0	x
3484	x	x	x	ж	х	0	0	x
3644	x	x	0	ж	х	0	0	x
3646	x	х	x	x	ж	0	0	x
4177	×	х	0	х	x	0	0	x
6872	x	x	х	х	х	0	0	х
6966	x	x	0	x	x	0	0	x
8291	x	x	х	x	х	0	0	x
8348	x	x	0	x	х	0	0	x
8449	x	х	х	x	x	0	0	x
8472	x	х	0	x	х	0	0	x
8538	x	х	х	x	х	0	0	x
8928	x	x	0	' <b>x</b>	x	0	0	x
9898	х	х	х	х	х	0	0	х

<sup>\*</sup>NOTE:

x = ON

<sup>0 =</sup> OFF

NARROWBAND TAPE RECORDERS

#### NARROWBAND TAPE RECORDERS

The Narrowband Tape Recorder Subsystem continued to operate in a completely satisfactory manner. Since-Orbit 1-the-two recorders A and B-have alternated in Record and Playback modes, generally switching roles each orbit. There is a nominal one minute overlap in Record for continuity.

Since launch, each recorder has had an ON time of 9217 hours and an OFF time of 8308 hours. Each recorder was in the Playback mode for 369 hours; in the Record mode for 8848 hours.

Table 12-1 shows typical telemetry values since launch. They are normal and show no significant trends.

Table 12-2 is a significant sample of the data in this reporting period showing the performance parameters of the Narrowband Recorders. It includes data to evaluate the entire link, including the radio downlink transmitting data from the recorders and the effect of ground station processing. The "mean data rate", nominally 24 kilobits, reflects the motor speed. The slightly slower speed has no effect on fidelity, but only increases operating time by less than one percent. The standard deviation is a measure of effects that would cause "wow" and "flutter" in a major frame. Occasional high values are attributed to transmission link noise. The performance appears excellent and is as good as it has been at any time since launch.

Table 12-1. Narrowband Tape Recorder Telemetry Values

	Function		Ту	pical Teleme	try Values - (	Orbits	
No.	. Name	6	1951-1959	3750-3751	5199-5200	7480-7481	9865-9866
10001	A - Motor Cur. (ma)						
	Record	190.10	189.47	189.20	188.76	186.31	186.31
	P/B	180.00	177.63	178.69	176.64	172.10	172,10
10101	B - Motor Cur. (ma)						
ļ	Record	193.26	192.79	193.04	195,60	194.79	195.79
	P/B	188.18	189.47	185.44	189.58	186.31	189,47
10002	A - Pwr Sup. Cur. (ma)						
	Record	320.56	339.81	338.20	342.48	339.81	339.81
	P/B	535.78	563.11	568.38	567.30	569.56	569.56
10102	B - Pwr Sup. Cur. (ma)				!		
	Record	317.62	333.75	336.05	341.87	343.50	346.75
	P/B	570.78	567.50	555.63	565.95	574.00	567.50
10003	A - Rec. Temp. (DGC)	25.47	26.25	24.40	24.56	24.20	22.80
10103	B - Tec. Temp. (DGC)	24.58	25.38	23.41	23.99	24.54	24,77
10004	A - Supply (VDC)	-24.47	-24.50	-24.44	-24.41	-24.62	-24, 62
10104	B - Supply (VDC)	-24.44	-24.57	-24.51	-24.57	-24.57	-24.29

Table 12-2. Narrowband Recorder Subsystem Performance

Orbit	%	Data	Data	ı Rate	R C D	0-1:4	%	Data	Data	Rate	R C
No.	Bad	Missing	Mean	Std. Dev.	R	Orbit No.	Bad	Missing	Mean	Std. Dev.	D R
9150	0,00	0,00	-23.84	0.02	В	9947	0, 00	0.31	-23.84	0.02	В
9151	0.00	0.00	-23.86	0,02	Α	9948	0, 01	0.26	-23,86	0.02	A
9152	0.00	0.00	-23,84	0.02	В	9949	0.24	0.00	-23.81	0.59	В
9153	0,01	0.77	-23.86	0.02	Α	9950	0.01	0.00	-23.86	0.02	Α
9154	0,00	0.00	-23.84	0.00	В	9951	0.25	0, 00.	-23,84	0.60	В
9250	0,00	0.00	-23.88	0.03	Α	10062		0.00	-23.86	P. 02	A
9251	0,00	0.51	-23,84	0.02	В	10063		0. 25	-23,84	1,35	В
9252	0,01	0,25	-23.86	0.02	Α	10066		0. 13	<b>-23, 88</b>	0, 43	A
9253	0, 01	0.00	-23,84	0.02	В	10067		0. 29	-23, 85	0.46	В
9254	0.01	0,00	-23.86	0.02	A	10069	0, 52	0. 13	-23, 88	0.94	A
9357	0.00	0.00	-23.87	0.02	Α	10143	0,00	0.27	-23, 86	0.02	A
9358	0.00	0.00	-23.84	0.02	В	10144	0.23	0.00	-23.90	0.06	В
9359	0.01	0.01	-23.86	0.02	Α	10145	0.01	0.00	-23,86	0.03	A
9360	0.00	0.00	-23,84	0,02	В	10146	1.44	1.02	-23,84	1.51	В
9361	0, 00	0.00	-23.86	0,02	Α,	10147	0, 00	0, 21	2.98	0.00	A
9470	0.00	0.00	-23, 84	0, 02	В		Sa	mple Fron	n Prior Or	bits	
9471	0, 05	0,00	-23.87	0, 27	Α					Γ	
9472	0,00	0.26	-23.84	0.02	В	953	0.00	0.00	-23.82	0.02	
9474	0.00	0.52	-23,84	: 0, 02	В	1320	0.01	0,00	-23.82	0.03	1 1
9475	0.00	0.24	-23.86	1.17	Α	2091	0.21	0.23	-23.85	0.57	1
	ľ					2496	0.00	0,25	-23.85	0.60	
9550	0,00	0,13	-23,86	0.03	В	4056	0,00	0.13	-23,85	0,03	
9551	0.13	0.70	-23.88	0.45	Α	6050	0.01	0.00	-23,87	0.03	
9552	0.01	0,00	-23,84	0.02	В	6953	0,26	0.00	-23.84	0.61	
9553	0.00	0.00	-23,86	0.02	Α	7650	0.00	0.00	-23.84	0.02	
9554	0.00	0.26	-23.84	0.02	В	8750	0.00	0.00	-23, 87	0,02	
9640	0.08	0.14	-23.85	0.04	В	1					
9641	0,00	0.27	-23.86	0.03	Α						
9642	0.01	0.47	-23.84	0.02	В	1					
9643	0.00	0.00	-23.86	0.02	Α					•	
9644	0.00	0.26	-23.84	0,02	В						İ,
9750	0.01	0.00	-26.86	0, 02	A						
9751	0,01	0,00	-23,84	0.02	В	1 1					
9752	0.00	0,00	-23.86	0.02	A						
9753	0.00	0.26	-23.84	0.02	В						
9754	0.23	0,48	-23.86	0.59	A						
9851	0.01	0.23	-23.87	0.02	A						
9852	0.00	0.00	-23.84	<b>0.02</b>	В	] ]					
9853	0, 25	0.00	-23.86	0.61	Α						
9854	0, 25	0.00	-23.85	0.61	В						
9857	0,00	0, 25	-23.88	0.03	A						

WIDEBAND TELEMETRY SUBSYSTEM

#### WIDEBAND TELEMETRY SUBSYSTEM

The Wideband Telemetry Subsystem has operated successfully since turn-on in Orbit 12. This Subsystem consists of two independent and similar 10/20 watt S-Band FM transmitters WPA-1 and 2 with associated filters, antennas, modulators and signal conditioning equipment.

WPA No. 1 was used with RBV input until Orbit 196 when the RBV power input circuit failed. WPA-1 was used again, this time with MSS input, between Orbits 1890 and 2039 because its operating frequency was less likely to interfere with the Apollo-17 launch operations. The cumulative ON-time for WPA No. 1 is 31 hours, 55 minutes and 9 seconds. When used after Orbit 20 it operated in the 20-watt mode.

WPA No. 2 has been used with MSS input since its initial turn-ON in the 10 watt mode during Orbit 12. It was changed to the 20 watt mode in Orbit 30, and has operated at this power ever since. It was not used between Orbits 1890 and 2099. The cumulative ON time for WPA No. 2 is 1379 hours, 6 minutes and 25 seconds.

Table 13-1 gives the telemetry values for both Wideband Power Amplifier units. All values are normal and show no significant trends.

Figure 13-1 shows the power delivered to Goldstone from two selected points in space (identical azimuth, elevation and slant ranges) as a function of time. Variations in equipment performance, calibration procedures, and readout accuracy probably cause the curves to have a saw-tooth appearance. The large variations in AGC levels have been attributed to equipment substitutions or adjustments. Within the limits of repeatable calibration and equipment adjustment the power delivered to Goldstone appears to have been generally constant since launch. The power output of the WPA-2 as measured by telemetry (Table 13-1) has remained level since launch at about 43.5 dBm.

PIR-U-ERTS-1N23-109 (see Appendix D) shows the extreme range of 3705 Kilometers over which the Wide Band Telemetry Subsystem transmitted MSS data to the Prince Albert ground station. Due to the altitude of the Prince Albert Station, it was able to receive good quality data at an elevation angle of 0.8 degrees below the horizon.

Table 13-1. Wideband Modulator Telemetry Values

WBPA-1

	Function				rbits	
Number	Name		26	1894	1944	2095
12001	Tmpt TWT Coll.	(DgC)	35.7	39,20	39,90	39.90
12002	Helix Current	(Ma)	6,08	6.49	6.58	6.78
12003	TWT Cath. Curr.	(Ma)	45.89	43.54	43.48	45.01
12004	Forward Pwr	(DBM)	43.18	42.88	42,61	43.15
12005	Reflected Pwr	(DBM)	34,95	34,99	34.80	35.21
12227	Loop Str. AFC ConVolt (1)	(MHz)	-0.39	-1,29	-0.86	-0.67
12229	Mod Temp VCO	(DgC)	21.93	20.31	20.88	20,39
12232	+15 VDC Pwr Sup A (2)	(TMV)	2.69	2,69	2,65	2.62
12234	-15 VDC Pwr Sup A	(TMV)	5,98	5.96	5,73	5.78
12235	+5 VDC Pwr Sup A	(TMV)	3.94	3.94	3.94	3,95
12238	-5 VDC Pwr Sup A	(TMV)	5.28	5,26	5,18	5.12
12240	-24 VDC Unreg Volt A	(TMV)	5.56	5,51	5,42	5.49
12242	Inv. Temp	(DgC)	20.60	23,43	24.71	24.04

\_\_WBPA-2

Function			Orbits							
Number	Name		33	2595	4096	7650	9335	9752	10182	
12101	Temp TWT Coll. (Max)	(DgC)	35.38	34.80	34,24	33,65	32,50	32,50	35,96	
12102	Helix Current	(Ma)	7,32	7,46	7.70	7.74	7.47	7.38	7.71	
12103	TWT Cath, Cur.	(Ma)	44,30	42.52	43.85	41.72	40.62	41.34	42,79	
12104	Forward Pwr	(DBM)	43.57	43.35	43,57	43.52	43,39	43,46	43,47	
12105	Reflected Pwr	(DBM)	31.59	32,11	32,79	32.83	31,89	32.37	32.91	
12228	Loop Str AFC Con Volt (1)	(MHz)	1,11	-1.01	-0.78	-1.10	-1.41	-1,21	-1.14	
12229	Mod Temp VCO	(DgC)	21,70	24.04	20.88	20,55	22,18	20,37	22, 25	
12232	+15 VDC Pwr Sup A (2)	(TMV)	2,68	2.58	2.69	2.68	2,69	2.69	2.69	
12234	-15 VDC Pwr Sup A	(TMV)	5,90	5.71	5.98	5.94	5.98	5.99	5.91	
12236	+5 VDC Pwr Sup A	(TMV)	3,97	3.91	4.01	4.01	3.94	4.01	4.02	
12239	-5 VDC Pwr Sup A	(TMV)	5.24	5,05	te	lemetry	point defe	ective		
12240	-24.5 VDC Unreg Volt A	(TMV)	5,43	5,33	5,52	5,51	5.56 l	5,59	5,43	
12242	Inv. Temp	(DgC)	23,03	22,95	22,96	24.10	22,55	22,89	23.99	

<sup>(1)</sup> Satisfactory if not zero or -7.5

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<sup>(2)</sup> B Power Supply not yet used in orbit

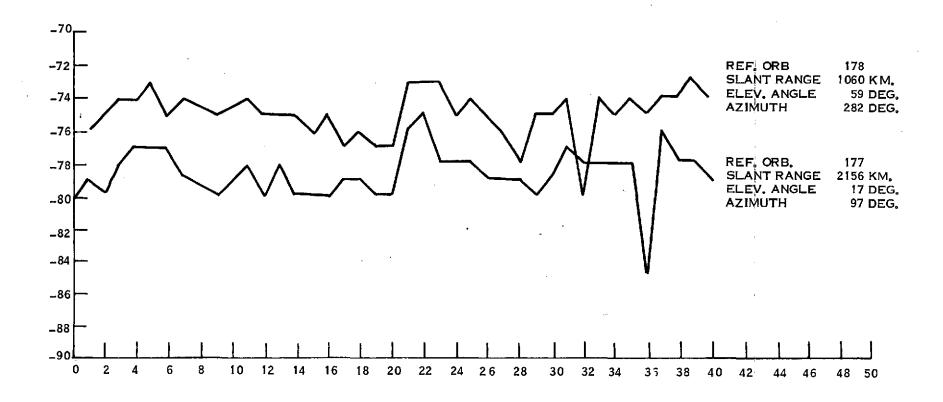


Figure 13-1. AGC Readings at Goldstone with 30-Foot Antenna Wide Band Power Amplifier

ATTITUDE MEASUREMENT SENSOR

#### ATTITUDE MEASUREMENT SENSOR

Telemetry output of the AMS continues to be normal and in  $\pm$  0.30 degree agreement with the ACS Subsystem.

Table 14-1 gives typical AMS telemetry values.

Table 14-1. AMS Temperature Telemetry Summary

Function							Orbit			
No.		Units	35	2600	5099	7650	8911	9335	97 52	10182
3004	Case - Temp 1	°C	18.92	20.05	19.42	20,29	20,05	19,88	19,78	19.71
3005	Assembly - Temp 2	°c	19.15	20.27	19.76	20.68	20.34	20.17	20.06	19,96

WIDEBAND VIDEO TAPE RECORDERS

#### WIDEBAND VIDEO TAPE RECORDERS

The Wideband Video Tape Recorder Subsystem consists of two components. WBVTR-1 and WBVTR-2. WBVTR-2 failed in Orbit 148 after 9 hours, 26 minutes and 33 seconds of satisfactory flight performance.

WBVTR-1 operated with RBV through Orbit 196 after which it was re-configured to operate with MSS. The WBVTR-1 has had 4 major disruptions in its service, generally characterized by high headwheel current (above 0.70 amperes) and high Minor Frame Sync Error counts (above 300). These disruptions occurred during:

Orbit 3469 on 29 March 1973

Orbit 8253 on 7 March 1974

Orbit 8845 on 19 April 1974

Orbit 9881 on 2 July 1974

After Orbit 9881, the tape recorder has temporarily been removed from operational service for engineering tests. The history of WBVTR-1 since Orbit 9000 is summarized in Appendix E. It is currently being operated in a test mode, cycling thru Records and Playbacks to provide data for selecting effective corrective measures.

In Figure 15-1 the usage of the tape by footage is shown.

Telemetry values for all functions are shown in Table 15-1. Values for WBVTR-2 are also shown for convenience and completeness.

Some of the telemetered functions have different values for different operating modes: Playback, Standby, Rewind and Record. These are shown in Table 15-2, showing stable operations since launch. It would appear the tape recorder itself is still in good operating condition, but that the video tape is both damaged and beginning to deteriorate.

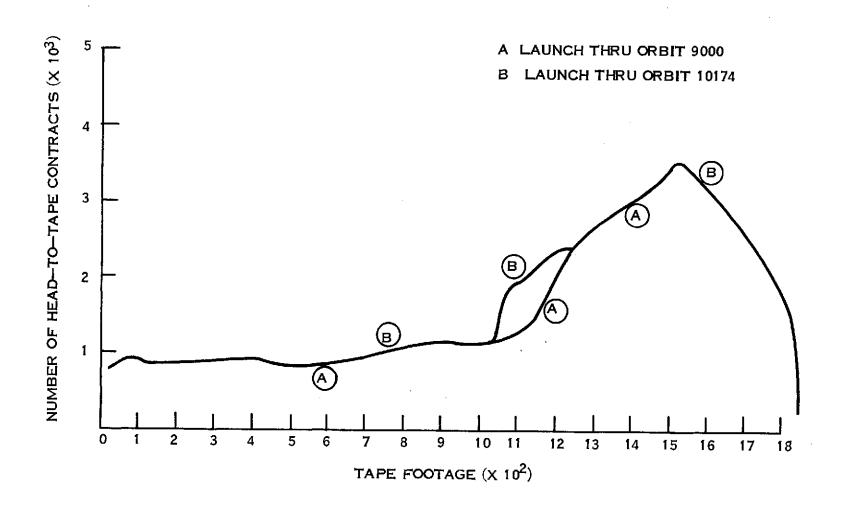


Figure 15-1. Tape Usage by Footage

Table 15-1. WBVTR Telemetry Values

WBVTR-1 Functions			Telemetry Value in Orbits								
Number	Name		15	2599	5029	7650	9435	9878	10088		
13022	Pressure Trans	(PSI)	16.12	16.38	16.11	16.12	15.98	15,97	15.98		
13023	Temp Trans	(DgC)-	19-50	25.05	21-84	23.78	21.25	20.74	20.81		
13024	Temp Elec	(DgC)	22.78	25,34	20.44	21,91	19.00	17,41	23.72		
13026	Capstan Speed	(%)	100.51	98, 25	101.93	101.11	97,77	97.34	102.84		
13027	Headwheel Speed	(%)	95.16	96.84	95.17	93.14	92.05	90,93	93.47		
13028	Capstan Mot I	(Amp)	0.25	0.26	0.27	0,24	0.25	0,24	0.28		
13029	Input P/B Volt.	(VPP)	0.72	0.41	0.45	0.46	0.48	0,59	0.33		
13030	Headwheel Mot I	(Amp)	0.55	0.55	0.54	0,54	0.55	0,57	0.55		
13031	Rec Input I	(Amp)	3,15	3.31	3.68	3,16	2.77	2.95	2.82		
13032	Lim Volt Out	(VPP)	1,44	1,42	1.45	1.45	1,36	1.36	1,17		
13033	Servo Volt	(%)	50,03	50.23	50.74	50.74	50.16	50, 25	47.71		
13034	+5.6 VDC Conv	(VDC)	5,66	5.71	5.68	5,78	5,79	5,64	<b>5.6</b> 5		

	WBVTR-2 Functions		Ţ <del>-</del>	Orbit N	umber	
Number	Name		15	. 64	103	147
13122	Pressure, Trans	(PSI)	15,99	16.25	16.25	16.11
13123	Temp Trans	(DgC)	18.46	19.19	20.72	21.09
13124	Temp Elec	(DgC)	21.50	22.00	24.00	21,92
13126	Capstan Speed	(%)	99.91	100.53	100.80	99.38
13127	Headwheel Speed	(%)	94.16	95.48	97.64	98.78
13128	Capstan Mot I	(Amp)	0.17	0.24	0.24	0.28
13129	Input P/B Volt	(VPP)	0.66	0.63	0.62	0.6
13130	Headwheel Mot I	(Amp)	0,55	0.59	0.52	. 0.58
13131	Rec Input I	(Amp)	3.70	3,53	3.07	3.43
13132	Lim Volt Out	(VPP)	1.34	1.41	1,41	1,39
13133	Servo Volt	(%)	49.97	49.60	49.80	49.48
13134	+5.6 VDC	(VDC)	5.47	5.64	5.58	5.59

Table 15-2. Function Values by Mode in Orbit

	Orbits								
Function/Description	913	2379	3781	4876	7385	7953	9866		
13029 - Input P/B Voltage									
Record	0	0	0	0	0	0	0		
Playback	0.40	0.45	0.58	0.53	0.48	0.48	0.67		
Rewind	0	0	0	0	0	0	0		
Standby	0	0	0	0	0	0	0		
13028 - Capstan Motor Current,									
Record	0.23	0.24	0,26	0,23	0,26	0.25	0.25		
Playback	0.25	0.25	0.26	0.26	0.28	0.23	0.28		
Rewind	0,23	0,20	0.20	0.17	0.17	0.18	0.18		
Standby	0	0	0	0	0	0	0		
13030 - Headwheel Motor Current									
Record	0.58	0.55	0.58	0.58	0.58	0.58	0.60		
Playback	0.56	0.55	0.62	0.56	0,55	0.58	0.59		
Rewind	0.47	0.44	0.46	0.45	0.43	0.45	0.46		
Standby	0.47	0.44	0.44	0.44	0.44	0.44	0.44		
13031 - Recorder Input Current									
Record	3.70	3,63	3.46,	3.40	3.40	3.30	3,30		
Playback	3.85	3,89	3,74	3.76	3.69	3,56	3.59		
Rewind	2,20	2,18	2,07	1.89	1.94	1.85	1.85		
Standby	1.96	2.08	1.78	1.73	1.88	1.98	1,85		
13033 - Servo Voltage	ļ				<u> </u> 				
Record	0	0	0	0	0	0	0		
Playback	50.30	50.37	50.70	50.78	50.76	50.96	50,86		
Rewind	0	0	0	0	0	0	0		
Standby	0	0	0	.0	0	0	0		
13026 - Capstan Motor Speed			<u> </u>	-	!	1.			
Record	98.50	96.70	102,88	103.41	103.41	105.09	104.53		
Playback	98,40	97.20	101.3	102.40	101,16	104.53	103.41		
Rewind	101.70	101.1	99.20	98.90	99.48	98,36	98.36		
Standby	0	0	0	0	0	0	0		
13027 - Headwheel Motor Speed							,		
Record	97.10	100.0	94.23	93.64	93.06	91.88	91.88		
Playback	97.10	97.80	93.69	92,93	93.06	90.70	91.29		
Rewind	100.72	100.70	95,10	93.60	93.64	91,88	91.88		
Standby	100,70	102.80	95,41	96.00	95,41	90.12	93.65		

# SECTION 16 RETURN BEAM VIDICON SYSTEM

### RETURN BEAM VIDICON

The Return Beam Vidicon (RBV) Subsystem operated normally fron turn-on in Orbit 19 to Orbit 196 when it failed to respond to a turn-off command because of a probable failure of a relay in the Power Switching Module. The RBV itself was not the cause of the failure, nor was it affected by the failure. The RBV has not been reactivated since Orbit 196, but it is capable of operation through individual component power switching. An assessment of the RBV performance was given in ERTS-1 Flight Evaluation Report 23 July to 23 October 1972. For completeness and convenience, the telemetry values are repeated in Table 16-1.

Table 16-1. RBV Telemetry Values

	FUNCTION	ORBITS								
NO.	NAME	T/V VALUE	26	85	149	196				
14001	CCC Board Temp. (DgC)	. (1)	18.61	20.04	19.30	19.5				
14002	CCC Pwr. Sup. Temp (DgC)	(i)	19.93	21.58	20.70	21.2				
14003	+15 VDC Sup. (TMV)	3.95	3.69	3,95	3.78	3.9				
14004	+6V-5.25 VDC Sup. (TMV)	3.05	2.84	2.93	2.98	3.0				
14100	VID OUT CAM 1 (TMV)	1.06	1.04	1.15	1.13	1.1				
14200	VID OUT CAM 2 (TMV)	1.09	1.05	1.26	1.23	1.2				
14300	VID OUT CAM 3 (TMV)	1.05	1.03	1.21	1.19	1.2				
14102	Comb. Align I Com 1 (TMV)	3,95	3.67	3.94	3.87	3.9				
14202	Comb. Align I Com 2 (TMV)	3.92	3.90	3.91	3.89	3.9				
14302	Comb. Align I Com 3 (TMV)	4.04	3.75	4.03	3.80	4.0				
14103	Cam 1 Elec Temp. (DgC)	(1)	20.84	23.37	22.64	25.				
14203	Cam 2 Elec Temp. (DgC)	(1)	18.64	21.06	20.62	22.8				
14303	Cam 3 Elec Temp. (DgC)	(1)	21.05	23.61	23,23	25.				
14104	Cam 1 LV Pwr Sup T. (DgC)	(1)	21.71	23.94	23.49	25.				
14204	Cam 2 LV Pwr Sup T. (DgC)	(1)	18.38	20.63	19.40	23.				
14304	Cam 3 LV Pwr Sup T. (DgC)	(1)	20.75	23.02	22.73	25.				
14105	Cam 1 Def. + 10 VDC (TMV)	4.01	3.73	4.00	3.77	4.0				
14205	Cam 2 Def. + 10 VDC (TMV)	4.00	3.71	3.98	3,77	3,9				
14305	Cam 3 Def. + 10 VDC (TMV)	3.97	3.95	3.95	4.02	3.9				
14106	Cam 1 + 6V -6.3 VDC (TMV)	3.71	3.45	3.70	3,61	3.				
14206	Cam 2 + 6V -6.3 VDC (TMV)	3.69	3.42	3.67	3.49	3.6				
14306	Cam 3 +6V -6.3 VDC (TMV)	3.73	3.47	3.72	3.47	3.				
14107	Cam 1 Telec I (TMV)	2.62	2.50	2.54	2.55	2.0				
14207	Cam 2 Telec I (TMV)	2.65	2.53	2.56	2.41	2.0				
14307	Cam 3 Telec I (TMV)	2,64	2.54	2.51	2.45	2.0				
14108	Cam l Vid Fil I (TMV)	2,47	2.30	2.36	2.38	2.4				
14208	Cam 2 Vid Fil I (TMV)	2.54	2.37	2.52	2.39	2.				
14308	Cam 3 Vid Fil I (TMV)	2.61	2.44	2.60	2.53	2.0				
14110	Cam 1 TARVOLT (TMV)	3.43	3.42	3.42	3.45	3.4				
14210	Cam 2 TARVOLT (TMV)	3,36	3.13	3.22	3,26	3.1				
14310	Cam 3 TARVOLT (TMV)	3.47	3.23	3.46	3.45	3.4				
14113	Cam l Vert Def V (TMV)	2.96	2.75	2.90	2.85	2.9				
14213	Cam 2 Vert Def V (TMV)	3.00	2.86	2.98	2.86	3.0				
14313	Cam 3 Vert Def V (TMV)	3.45	3.45	3.47	3,37	3.4				
4114	Cam 1 Vid FPT (DgC)	(1)	18.15	20.77	17.91	20.9				
14214	Cam 2 Vid FPT (DgC)	(1)	20.62	20.11	20.52	20.6				
14314	Cam 3 Vid FPT (DgC)	(1)	18.54	20.88	19.08	20.2				
4115	Cam 1 Foc Coil T (DgC)	(1)	17.71	21.67	18.74	19.7				
14215	Cam 2 Foc Coil T (DgC)	(1)	17.70	21.60	19.25	19.9				
14315	Cam 3 Foc Coil T (DgC)	(1)	18.03	22.09	19.88	20.5				

<sup>(1)</sup> Thermo-Vacuum temperatures for these functions were not reported.

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

# SECTION 17 MULTISPECTRAL SCANNER SUBSYSTEM

#### SECTION 17

#### MULTISPECTRAL SCANNER SUBSYSTEM

The Multispectral Scanner Subsystem (MSS) has operated satisfactorily since initial turn-on in Orbit 20. The MSS has imaged over 27% of the earth's surface between the latitudes of 81.42°, including over 78% of the land masses, and 7% of the oceans with a cloud cover of 30% or less. Many of these scenes were repeatedly imaged, some in the United States as many as 40 times, although the cloud cover of some of these repetitive scenes exceeded 30%. A very large percentage of every continent has been imaged. Figure 17-1 is a computer derived map showing how many scenes were imaged at each geographic location since launch. Along the right-hand edge of the map is listed the frame number - frame 1 being at the northern-most extreme, frame 61 centered on the equator, and frame 121 at the southernmost extreme, thus giving latitude. Along the top of the map is the number of the reference orbit which fixes longitude. The land masses are distorted to fit this map projection.

Figure 17-2 shows how many scenes were acquired during this reporting period.

Table 17-1 shows typical telemetry values during this quarter. All functions are normal. The maximum MUX temperature to date has been 33.25°C which occurred in August 1973, when the MSS was accidentally left ON at LOS, and was turned OFF by the 32-minute back-up timer. The calibration lamp current has remained at 1.12 TMV from pre-launch to the present.

Time Code extracted from de-muxed data was observed and found normal.

The response history of each sensor to a selected input radiance level is shown in Figure 17-3 (1) thru (8). Only one radiance level for each sensor has been selected for graph presentation, but the other five levels selected in the computer program to determine the cal wedge shape have been analyzed and found to be consistent with the data presented.

In general, the graphs show an early gradual decrease in sensor response from launch to Orbit 1000, and essentially unchanged response thereafter. The notable exception is sensor 13.

LAST SCUEDULED FRAMED UBDATT-(5) AUG 024*72 LAST FRANCE RECEPTOR UBDATT-(7) AUG 024*72 LAST FRANCE RECEPTOR UBDATT-(7) AUG 024*72 LAST FRANCE RECEPTOR UBDATT-(1000) DATA LEED FROM CYCLE 01 TO 800 THE UBLATE FRANCE RECEPTOR UBDATT-(1000) THE UBBAT	

FOLDOUT FRAME

FOLDOUT FRAME

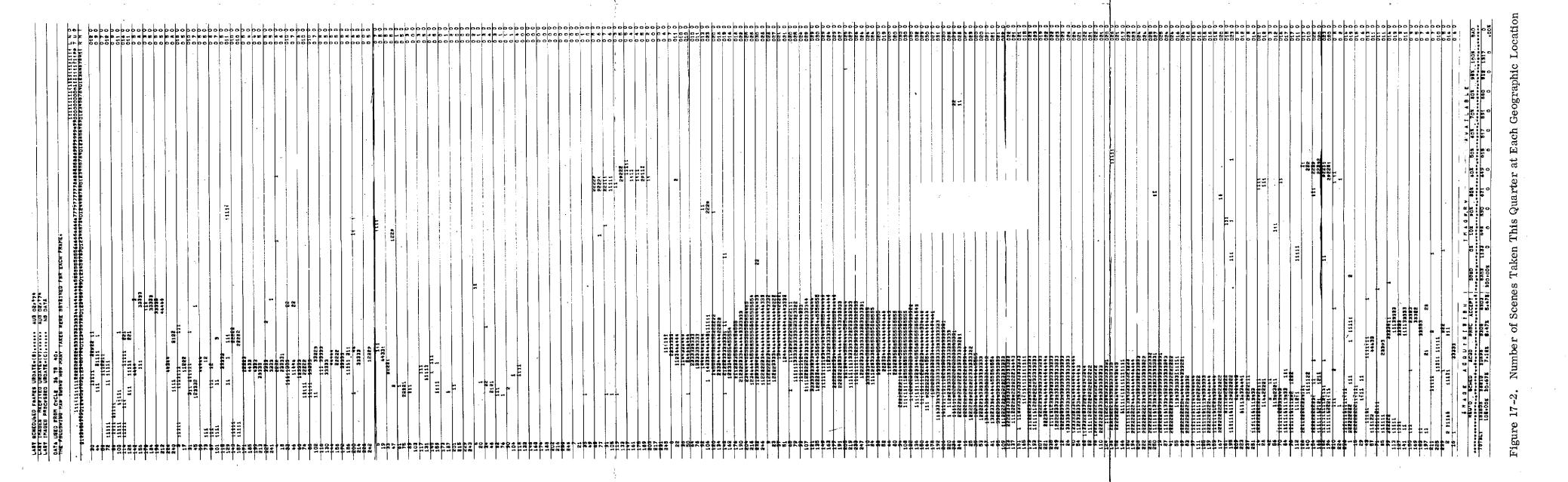
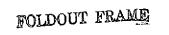
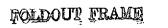


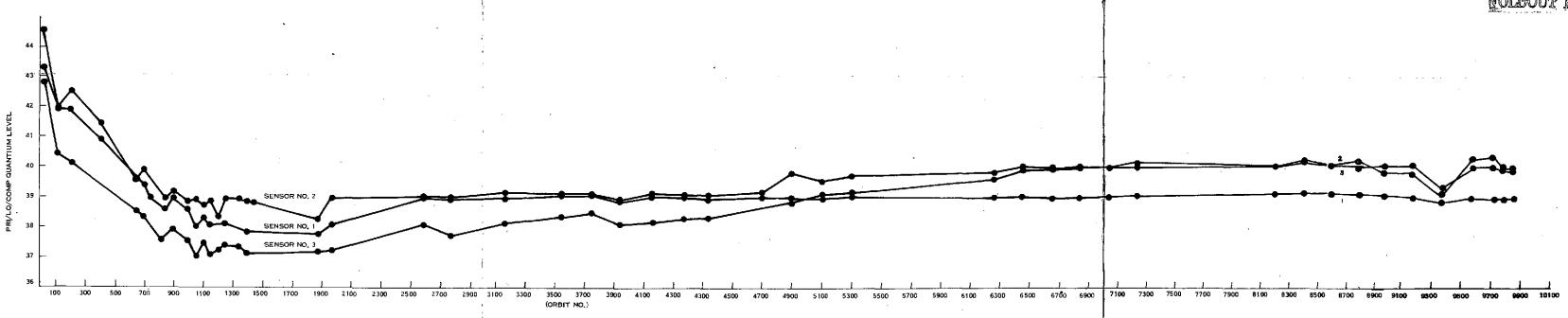
Table 17-1. MSS Telemetry Values

Function					Telemetr	y Values	in Orbits	3	
No.	Name		20	2599	5060	7650	9335	9752	10182
15044	FOPT 2 T	(DGC)	17.46	21.03	19.84	21,78	20.13	20.10	20.46
15046	ELEC CVR T	(DGC)	19,37	23,53	21.83	24.39	22.00	22.13	22.73
15048	SCAN MIR REG T	(DGC)	16.35	22.84	19.77	23.06	20.08	20.02	21.18
15050	SCAN MIR DR. COIL T	(DGC)	15.94	21.97	19.30	22.47	19.58	19.71	20.65
15052	ROT SHUT HSG T	(DGC)	16.91	20.88	20.07	22.11	20,52	2 0.54	20.68
15043	FOPT 1 T	(DGC)	17.67	21.17	20.01	21,90	20.31	20.28	20.65
15045	MUX PWR CASE T	(DGC)	21.19	26.84	22,03	25.91	21.93	22.43	24.09
15047	PWR SUP T	(DGC)	17.41	21.95	20.00	22.26	20.22	20.25	21.00
15049	SCAN MIR DR. ELC T	(DGC)	16.12	22,76	19.41	22.74	19.66	19.79	20.98
15051	SCAN MIR HSG T	(DGC)	15.60	21.46	19.05	22.29	19,32	19.22	20.16
15040	MUX -6 VDC	(TMV)	4,03	4,03	4.03	4.03	4.03	4.03	4.03
15042	AVE DENS DATA	(TMV)	1.67	2.52	2.13	1,99	2.05	2.09	2.27
15054	CAL IAMP CUR A	(TMV)	1.12	1,12	1.12	1.12	1,12	1.12	1.12
15056	BAND 2 <u>+</u> 15 VDC	(TMV)	5.10	5.10	5,10	5.10	5.10	5.10	5.10
15058	BAND $4 + 15$ VDC	(TMV)	5.10	5.10	5.10	5.10	5,10	5.10	5, 10
15060	+ 12 -6 VDC REG	(TMV)	4.82	4.92	5,02	5.02	4.77	4.75	4.90
15062	+ 19 VDC REC OUT	(TMV)	4.80	4.90	4.90	5.03	4.77	4.77	4.89
15064	BAND 1 HV A	(TMV)	5.10	5,12	5.16	5.12	5,12	5.12	5.12
15066	BAND 2 HV A	(TMV)	4.50	4,52	4.52	4.52	4.52	4.52	4.52
15068	BAND 3 HV A	(TMV)	4.60	4.63	4.62	4.62	4.62	4.62	4.62
15070	SHUT MOT CON OUT	(TMV)	2.43	2.46	2.44	2.49	2.37	2.33	2.44
15041	S/D CONV REF V	(TMV)	5,93	5.82	5.93	5.78	5.67	5.93	5, 80
15053	SCAN MIR REG V	(TMV)	4.42	4.53	4.51	4.59	4.39	4.35	4.49
15055	BAND 1 <u>+</u> 15V	(TMV)	4.97	4.97	4.97	4.97	4.97	4.97	4.97
15057	BAND $3 \pm 15V$	(TMV)	5.00	5.00	5.00	5.0Դ	5.00	5.00	5.00
15059	-15 VDC TEL. (TM)		5.02	5.02	5.02	5.02	5.02	5.02	5.02
15061	$\pm$ 5 VDC LOGIC REG (TMV)		4.82	4.80	4.81	4.86	4.84	4.85	4.79
15063	-19 VDC REG OUT	(TMV)	3.43	3.50	3.39	3.57	3,57	3.38	3.48
15071	SCAN MIR DR. CLK	(TMV)	1.93	1.97	1.97	2,03	1.92	1,92	1.96









BAND NO. 1 QUANTUM VS. ORBIT WORD NO. 300

Figure 17-3(1). Quantum vs. Orbit

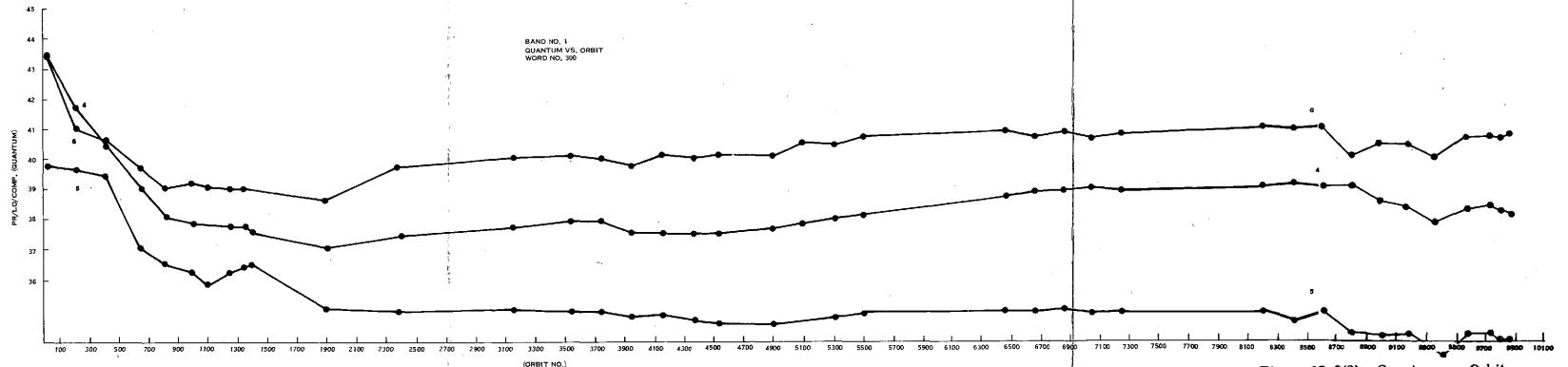
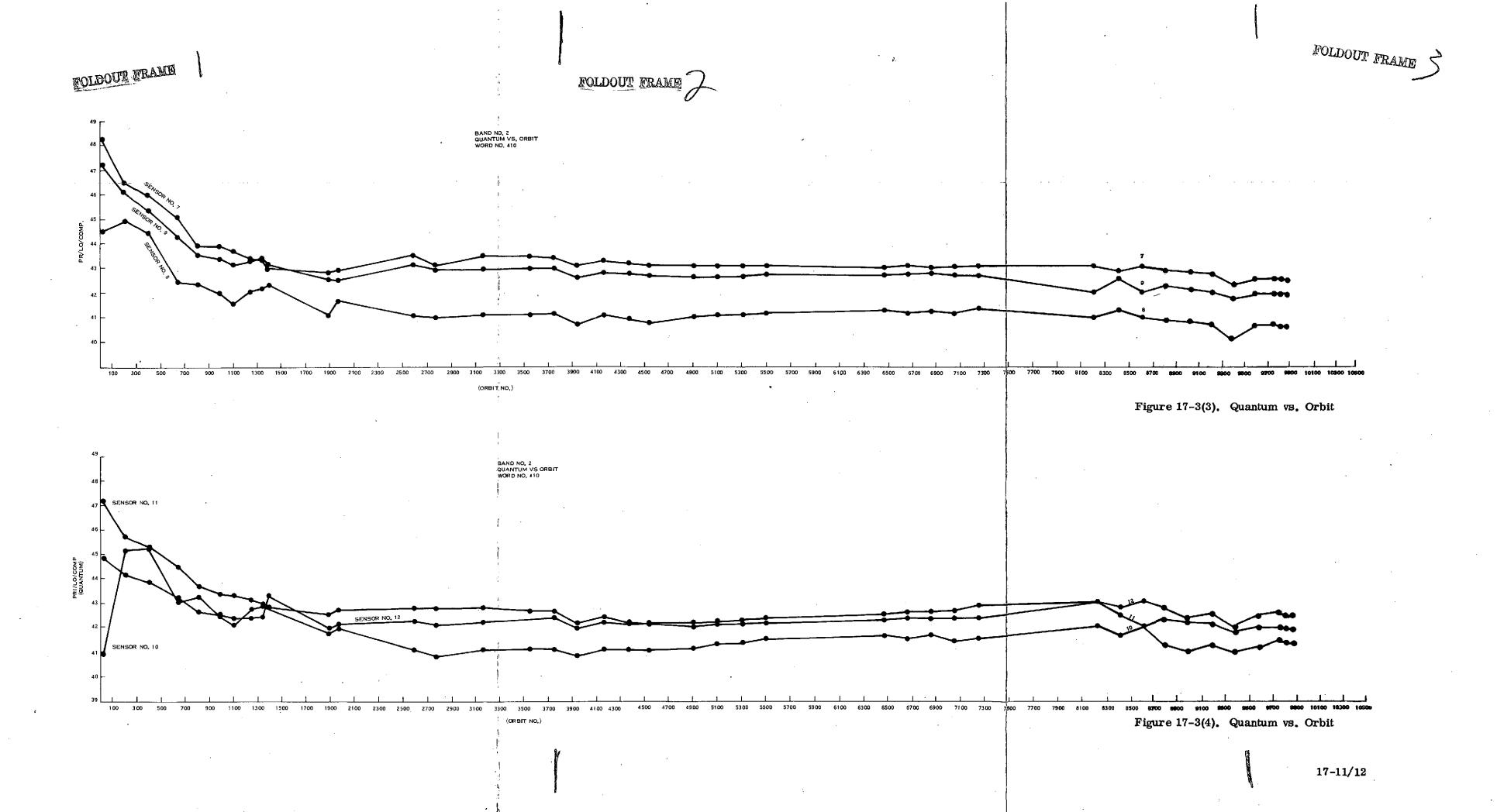
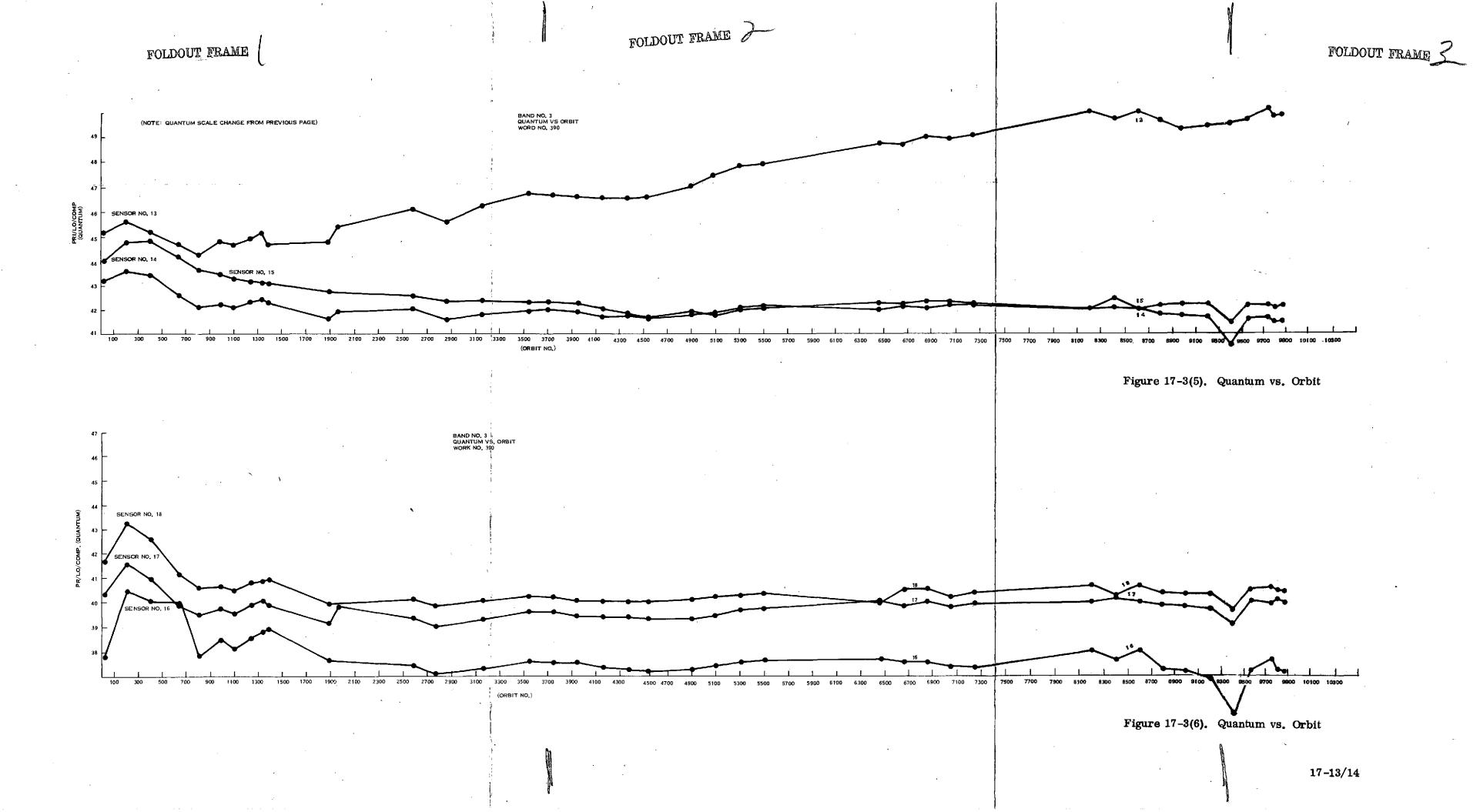


Figure 17-3(2). Quantum vs. Orbit





The response of this sensor has gradually increased about 10%, so that it saturates at a lower radiance level than the other sensors, posing a processing problem for high radiance scenes (clouds, snow and sometimes desert).

The history of the Line Length Word vs. Orbit Number is shown in Figure 17-4. It is satisfactory and stable.

Sun calibrations are performed every two weeks (see Table 17-2) and continue to show normal performance. The 76 Sun Calibration Orbits are listed in Table 17-2.

Table 17-2. Sun Calibration Orbits

21	1012	2278	4161	6657	8943
47	1207	2375	4370	6852	8999
89	1303	2389	4537	7047	9208
103	1400	2473	4705	7242	9389
131	1497	2585	4900	7437	9585
214	1595	2668	5095	7633	9724
326	1692	2766	5304	7829	9766
423	1790	2964	5499	8038	9808
521	1877	3159	5861	8220	9850
619	1985	3351	5891	8413	9892
730	2082	3543	6072	8608	9975
814	2166	3742	6268	8803	10171
915	2180	3938	6463		

A study (PIR-1H05-EA-434 dated 8/5/74) conducted by Dan Schwartz at GE Valley Forge examines the performance of the MSS Subsystem during the sun-cal orbits since Orbit 5000. It concludes that, except for a temporary decrease of cal wedge sensitivity in the vicinity of Orbits 9200/9400, performance has been exceptional. There may have been a decrease in SNM (signal-to-noise at level 63) for some of the sensors over time in orbit, but even if true, the decrease is small and must be examined further in terms of possible quantization microstructure effects. There are no factors evident which would preclude continued use of the data with confidence.

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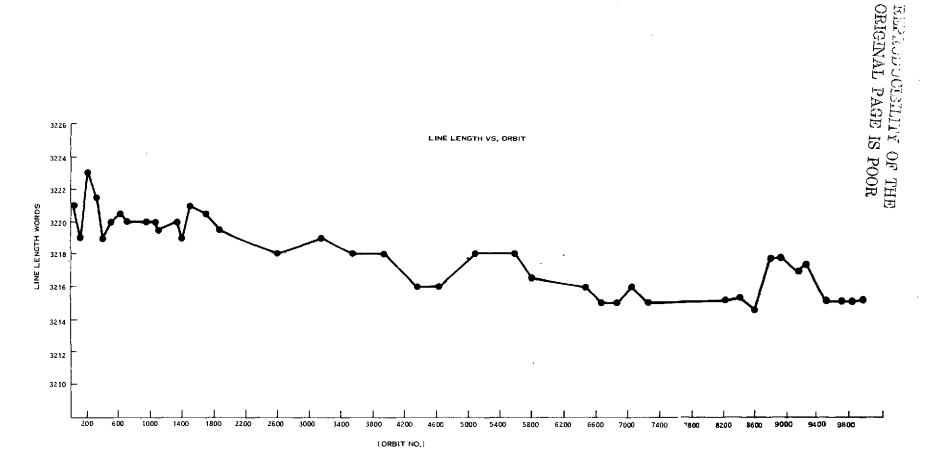


Figure 17-4. Line Length vs Orbit

SECTION 18

DATA COLLECTION SYSTEM

#### SECTION 18

#### DATA COLLECTION SUBSYSTEM

The Data Collection Subsystem (DCS) has operated satisfactorily since turn-ON in Orbit 5. External interference is minimal and has not affected data collection during this reporting period.

Only Receiver 1 has been used to date. Since turn ON this receiver has operated continuously for over 17,516 hours.

Since turn-ON in Orbit 5, this subsystem has received 945, 451 messages, of which 871,009 (92.1%) have been perfect. Periods of heavy interference have added false messages to both "total" messages and "imperfect" messages, diluting the apparent "error" rate, and making the percent perfect figure an unreliable figure of merit.

All telemetry functions have been normal as shown in the typical values of Table 18-1.

Figure 18-1 shows the total number of DCS messages received per 18-day cycle since launch. The number of active platforms is also plotted on the same time scale. It can be seen that when the number of active platforms reached about 100, the DCS messages received per 18 day cycle reached 28 thousand.

After cycle 31 there was a drop in the number of DCS messages received to the level of 23 thousand per 18-day cycle. This drop is explained by the drop in USB transmitter power as shown in the lower right hand portion of Figure 18-1. The USB provides the down-link in the DCS relay chain. When its power dropped to below 0.25 watts, the USB/DCS coverage began shrinking back from the horizon reducing the area coverage to about 80%, corresponding to the percentage message loss from 28 to 23 thousand. This loss of area coverage is described in Appendix C. There it is pointed out that the up-link comprising the DCP and the ERTS DCS receiver showed no loss of range, operating daily

to distances in excess of 2000 miles. The link even operated to 2260 statute miles (3637 kilometers),  $1^{0}$  below the horizon.

Though there was reduced coverage of possible DCS messages the DCS subsystem has exceeded specification requirements at all times as messages from each DCS platform were received at ground stations each day and the data link was established at antenna angles below 5° elevation. In Orbit 10068 the USB subsystem was switched from side A to side B. Power output of the USB side B transmitters is 1.58 watts. When sufficient data is accumulated it is expected that the USB/DCS coverage will show expanded coverage similar to initial flight conditions observed in earlier life of the spacecraft when power output was 1.5 watts.

Table 18-2 shows the qualitative performance of the DCS subsystem and Table 18-3 gives statistics of messages received.

Value in Orbits No. Name Units 15 2599 4811 7650 9335 9752 10182 16001 Revr 1 (DBM) -124.09-124.39-123.36 -123.01 **-124.** 49 -123.64-123.63Sig Str 16002 Revr 1 (DGC) 22, 72 24,07 23, 74 24. 62 23,84 23.66 23.71 Temp 16003 Revr 1 (VDC) 12,02 12.02 12.01 12.01 12.01 12.02 12.02 Inp Volt

Table 18-1. DCS Telemetry Values

Table 18-2. DCS Qualitative Performance

System Threshold	3500 km
Grazing Angle Effects	Not discernible
Adjacent DCP Interference	Not seen
Ground Transmission System	Satisfactory
Probability of Perfect Reception of any Messages During Window*	98.9%

<sup>\*</sup>Window means "at times when the spacecraft is simultaneously within the horizon of the DCP and the ground receiving station".

Table 18-3, DCS Statistics

Through Orbit 10182		-
DCS Platforms (DCP's) Shipped	220	
Maximum DCP's Received per Day	110	ŧ
Total Messages Received at OCC	945, 451	
Total Messages Rejected at OCC	74, 422	
For This Quarter		
Maximum Messages per Day (5/25/74)	1523	
Number of Orbits with Message Counts Exceeding:		•
400	. 27	
500	. 0	
Number of Current Users	43	

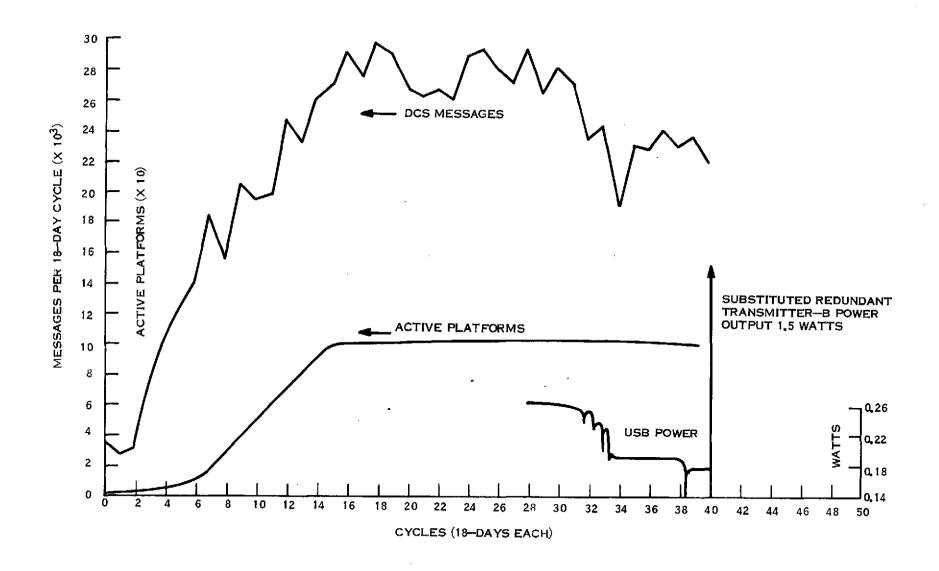


Figure 18-1. DCS Message Receipt History

APPENDIX A

### OBSERVATORY ANOMALIES AND OBSERVATIONS

Date	Anomaly/Observation	How Observed	Comments
7/24/72	Sun Sensor Temperature High	Off-Line	No Action Required For ERTS-1; ERTS-B Redesigned
7/24/72	Solar Paddle Temperature Excursions Greater Than Expected	Off-Line	No Action Required For ERTS-1; Math Model Corrected
7/25/72	USB Power Output Decreasing	Off-Line	Will Switch to Side B When Necessary; Under Investigation for ERTS-B
8/03/72	WBVTR No. 2 Power Converter Shorted	Real Time & Off-Line	Turned All P/L Off During Pass. Formed NASA/GE/RCA Evaluation Committee. Disconnected since Anomaly. Redesigned For ERTS-B
8/03/72	Decrease in Solar Array Current	Off-Line	Evaluate Degradation Effect Due to Solar Flare Activity
8/06/72	RBV Power Transient PSM Turn-Off Failure	Real Time	Turned off PRM. NASA/GE, RCA Evaluation Committee Formed; Disconnected Since Anomaly; Redesign PSM For ERTS-B
8/10/72	DCS Reject Messages Rose to Over 40% of Total Messages for 15 Days	Off-Line	External Interference; Located Source; No Serious Interference Since.
8/10/72	MSS Cal Wedge Levels Decreasing	Off-Line	Leveled Off After Orbit 1000; At Or About 53 Below Earlier Values
8/03/72	Incorrect Time Tags in Comstor 'B' Cell 12	Real Time	Reload Cometors and Verify; (Discontinued Active Use of Cell 12)
12/04/72 12/06/72	Pitch Motor Drive Duty Cycles Roll Increased for Short Yaw Period	Off-Line	Evaluate - Prepared Contingency Plan Under Investigation For ERTS-B
3/29/73	WBVTR NO. 1; High BER	Real Time	Formed NASA/GE/RCA Committee; Lapped Heads; Now in Operational Use. Temporarily Restricted to Last 600 Feet (600 Seconds) of Tape
4/08/72	Slow Leak in Forward IR Scanner Pressure	Off- Line	Not Expected to Interfere with Normal Operations
5/20/72	Defect in Signal of Left Cosine Pot at S/C Midmight	Off-Line	Not Expected to Interfere with Normal Operations
6/03/73	Failure of Integrated Circuit Chip and TLM of Functions 6012, 1011, 12238 and 7010	Real Time & Off-Line	Thm Failure only. S/C Operations Normal
11/5/73	WBVTR-1 Tape Unit Pressure Drop	Real Time	Defect in Pressure Instrumentation which Causes Occasional Rapid Pressure Drop in TLM - Returns to Normal
11/13/73	Solar Array Drive	Real Time	Slight Peaks on Drive Voltage Ripple which Picked up Limit Flag - Returned to Normal
11/28/73	High Head Wheel Current, WBVTR-1, During Rewind	Real Time	Resumed Operations After Investigation WBVTR-1 Performed in a Nominal Manner
12/20/73	Pitch Motor Driver Duty Cycle Increased	Real Time	Similar to Entry 12/4/72 except more Sustained
12/22/73	RMP-1 and RMP-2 Showed Excessive Noise/Output	Real Time	Condition Lasted for Several Orbits and Returned to Normal
2/20/74	Pitch Wheel Stopped During Sun Transient	Off-Line	During a sun transient in orbit 8040 the pitch flywheel was changing directions. As it passed thru zero speed, the pitch flywheel stopped and did not resume operation until 2 minutes had elapsed in spite of application of 100% clockwise pitch motor driver duty cycle during that interval.
3/5/74	WBTR #1 High BER HIGH HW-1	Real Time & Off-Line	Limited Usage of Tape Footage
3/7/74	WBVTR-1-high HWI	Real Time & Off-Line	Suspended operation pending study
3/21/74	WBVTR-1-high HWI	Heal Time & Off-Line	Suspended operation pending study
3/27/74	WBVTR-1-MFSE count high	Off-Line	Suspended operation pending study
4/2/74	WBVTR-1-MFSE count high	Off-Line	Suspended operation pending study
5/21/74	Pitch CCW Motor Driver Duty Cycle Increased	Real Time & Off-Line	Similiar to 12/4/72 entry. Returned to normal.
7/2/74	Pitch CCW Motor Driver Duty Cycle Increased	Real Time & Off-Line	Similiar to 12/4/72 entry. Returned to normal.
7/2/74	WBVTR-1-high HWI and MFSE	Real Time & Off-Line	Suspended operation pending study
		L.	

APPENDIX B

#### SPACECRAFT ORBIT REFERENCE TABLES

FROM JULY 1972 THRU SEPTEMBER 1975

ORBIT O THRU 15928

FLIGHT DAY 0 THRU 1142

JULY 1972

Date	GMT Day	Flight Day	Spacecraft Orbit	Reference Orbit	Ref Day	Cycle
23	205	0	0-3	150-153	11	
24	206	1	4-17	154-167	12	
25	207	2	18-31	168-181	13	
26	208	3	32-45	168-181*	13	
27	209	4	46-59	182-195	14	0th
28	210	5	60-73	196-209	15	
29	211	6	74-87	210-223	16	
30	212	7	88-101	224-237	17	
31	213	8	102-115	238-251	18	1

\*Shift due to initial orbit (prior to orbit adjustments)

AUG-1972

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	- 25	i	299	Í	94	i	1301-	1314	i	182-195	ï	14	i	5	
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4   309   104   1441= 1454   71= 84   6   6   6   5   310   105   1455= 1468   35= 98   7   6   6   311   106   1469= 1481   39=111   8   6   7   312   107   1482= 1495   112=125   9   6   8   313   108   1496= 1509   126=139   10   6   9   314   109   1510= 1523   140=153   11   6   10   315   110   1524= 1537   154=167   12   6   11   316   111   1536= 1551   168=181   13   6   12   317   112   1552= 1565   162=195   14   6   13   13   6   14   319   114   1580= 1593   210=223   16   6   14   319   114   1580= 1693   210=223   16   6   14   319   114   1580= 1693   210=223   16   6   16   15   320   115   1594= 1607   224=237   17   6   16   16   321   116   1608= 1621   238=251   18   6   17   322   117   1622= 1435   1= 14   1   7   18   323   118   1636= 1649   15= 28   2   7   19   324   119   1650= 1663   29= 42   3   7   12   12   1692= 1705   71= 84   6   7   12   1326   120   1664= 1677   43= 56   4   7   12   1326   120   1664= 1677   43= 56   4   7   12   1326   123   1706= 1719   85= 98   7   7   124   329   124   1706= 1719   85= 98   7   7   124   329   124   1706= 1719   85= 98   7   7   126   331   126   1747= 1760   126=139   10   7   126   331   128   1776= 1788   154=167   12   7   129   334   129   1769= 1802   168=181   13   7		· • 3 · • i							ŀ
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22   327   122   1692-1705   71-84   6   7     23   328   123   1706-1719   85-98   7   7     24   329   124   1720-1732   99-111   8   7     25   330   125   1733-1746   112-125   9   7     26   331   126   1747-1760   126-139   10   7     27   332   127   1761-1774   140-153   11   7     28   333   128   1775-1788   154-167   12   7     29   334   129   1789-1802   168-181   13   7	i						,		
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26   331   126   1747 = 1760   126 = 139   10   7	j	25	-				-	• • • • • •	
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+	12	347	1 142 1	1971- 1983	1	99-111	-	8	8	ļ
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	15	350	145	2012 - 2025	1	140-153	1	11	1: 8	l
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1	18	353	1 148	2054- 2067	H	182-195	- 1	14	8	ļ
	1 <del>9 </del>	354	149	- 2066- 2081	1	196+209		15	8	!
1	20	355	150	2082- 2095	1	210-223	ļ	16	8	!
. 1	21	356	151	2096- 2109	ļ	224-237	J	17	8	į.
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	53 - 1	358	153	2124- 2137	1	1- 14	. !	1 1	9	ļ
	24	359	1 154 1	2136- 2151	ļ	15- 28	Ţ	5	9	!
	<u>2</u> 5	360	1-155	- 2152- 2165	ı	29- 42	1	3	9 :	ļ .
ļ	26 1	361	156	2166- 2179	ı	43= 56	1	4	9	!
1	- 27 I	362	157	2180- 2193	1	57- 70	į.	5	9	ţ
	28	363	158	2194- 2207	1	71= 54	ļ	6	9	ļ
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17	- (	15	1 15	176	İ	2445= 2458	ł	71- 84	1	6	10
18	1	16	1 16	177	i	2459- 2472	ı	85≖. 98	1	7	10 I
19   19   180   2500- 2513   126-139   10   10   20   20   181   2514- 2527   140-153   11   10   21   21   21   182   2528- 2541   154-167   12   10   22   22   183   2542- 2855   168-181   13   10   23   23   184   2556- 2569   182-195   14   10   24   24   24   185   2570- 2583   196-209   15   10   25   25   186   2584- 2597   210-223   16   10   25   25   186   2584- 2597   210-223   16   10   26   26   26   187   2598- 2611   224-237   17   10   27   27   27   188   2612- 2625   238-251   18   10   26   26   28   28   29   190   2640- 2653   15- 28   2   11   29   29   190   2640- 2653   15- 28   2   11   30   30   30   191   2654- 2667   29- 42   3   11	- (	17	17	178	l	2473- 2485	1	99-111	1	8	10 I
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25   25   186   2584= 2597   210=223   16   10   126   26   187   2598= 2611   224=237   17   10   127   27   188   2612= 2625   238=251   18   10   128   28   189   2626= 2639   1= 14   1   1   11   129   29   190   2640= 2653   15= 28   2   11   130   30   30   191   2654= 2667   29= 42   3   11	١			-	ı		1		1	14	
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31   31   192   265a+ 2681   43+ 56   4   11	1		•	191	l	2654- 2667	ŧ	29- 42	1	3	11
	ļ	31	31	152	İ	265a- 2681	ŀ	43 <b>-</b> 56	ı	4	11

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1		1 667	- <sub>'</sub>	FITGHT	1	SPACE	CRAFT	٠ .	REFERENCE	4-	REF	4	CYCLE	4
1	DATE			DAY	i	ยลธ		į	URBITS	i	- ·	i	NO.	Ì
•				~						-				•
- 1	1	1 32		193	1	2682-		1	57 <b>-</b> 70	1	5	1	11	1
- [	5	1 33	ļ	194	1	2696=		-	71 = 84	Į.	6	L	11	j
1	. 3	1 34	J	195	t	2710-		1	85+ 98	1	7		11	ļ
- 1	4	1 35		196	ſ	2724-	2736	1	99-111	Ţ	8	1	11	1
i	5	1 36	•	197	1	2737-	2750	ł	112-125	1	9	į	11	1
ı	6	37	-	198	1	2751-	2764	ı	126-139	t	<b>1</b> Ü	į	11	1
Ţ	7	1 38	1	199	1	2765-	2778	1	140=153	1	11	1	11	1
ļ	ä	1 39	ŀ	200	1	2779-	2792	J	154-167	1	12	1	11	1
ţ	Э	1 40	- 1	201	1	2793-	2206	1	168=181	- [	13	1	11	1
1	10	41	1	505	1	2807-	5450	1	182-195	1	14	ı	11	ţ
ļ	11	1 42	- 1	503	1	2821-	2834	1	196-209	1	15	1	11	1
1	12	1 43	ı	204	1	2635=	2448	1	210+223	1	16	ļ	11	1
1	13	1 - 44	ţ	205	1 .	2849=	2×62	ŀ	224-237	1	17	t	11	1
1	14	1 45	)	206	ł	2863=	2×76	1	238-251	Ŧ	18	1	11	1
į	15	1 46	ł	207	1	2877=	2×90	Ì	1 = 14	1	1	1	12	j
-	16	1 47	- [	208	1	2891=	2904	1	15- 28	1	2	1	12	
1	17	1 48	ł	20 <b>9</b>	1	2905-	2918	1	29= 42	1	3	t	12	1
i	18	1 49	1	210	1	2919-	5335	1	43+ 56	İ	4	Ì	12	1
1	19	F 50	ļ	211	1	2933-	2946	1	57- 70	ŧ	5	į	12	1
1	20	51	j	212	1	2947-	2960	1	71= 84	1	6	i	12	Ī
1	21	1 52	ļ	213	į.	2561=	2974	1	85= 98	1	7	1	12	1
i	55	1 53	1	214	i	2975•	2987	1	99-111	1	Ä	1	12	)
-	53	1 54	ł	215	1	2936=	3001	1	112-125	1	9	1	12	i
1	24	1 55	ŀ	216	1	3002-	3015	1	126-139	1	10	ı	12	1
1	25	56	þ	217	1	3016-	3029	t	140+153	1	11	i	12	1
1	26	l 57	- (	218	1	3036-	3043	1	154-167	ı	īž	ĺ	12	i
1	27	58	ļ	219	1	3044-	3057	1	168-161	ŀ	13	ļ	12	j
ł	26	59	1	220	1	305გ-	3071	1	182+195	ŀ	14	ł	12	1
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•	DATE	GMT DAY	FIIGHT     DAY	SPACEC BR31	RAFT I	REFEREN URBIT		REF Day	1	CYCLE N6.	1
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	j 4	63	1 224 1	3114=	3127	238+29	1 1	18	1	12	1
	) ··· - 5 · ··	64	1 225 1	3128-	3141	1 = 1	4	1	ı	13	1
	1 6	65	1 226 1	3142-	3155	15- 2	8 1	5	ŀ	13	1
	J <b>7</b>	166	1 227 1	3156=	3169 1	29- 4	2 1	3	1	13	1
	<b>b</b>	1 67	1 228 1		3183 1	<b>43=</b> 5	6 1	4	i	13	1
-	ļ 9	68	1 - 229 1	-3184-	3197 1	<b>57</b>	0 1	5	ļ	13	ŧ
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	i ~ · <b>11</b> ·····	1 70 -	1 - 231 +	3212-	3225 I	გ5≖ 9	8 1	7	į	13	1
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~	<u>1</u> 3	172	+ 533+		3252 1	112-12	5 1	- <del>9</del>	ł	13	1
	14	73	1 234 1		3266 I	126+13	9 1	10	1	13	1
	15	74	1 235 1		3280	140-15	3	11	ł	13	ş
i	16	75	1 536, 1		3294	154=16	7 1	12	1	13	1
	1 17	76	1 237 1		3308 I	168-18	1	13	1	13	I
i	16	77	1 238 1		3355 1	182-19		1 4	ı	13	Ţ
	19	i78	I 535 -I		3336 +	196-20	9 1	15	1	13	ł
İ	20	79	1 240 1		3350 l	210-22		16	ı	13	ļ
	21	1 - 80	I - 241		3364	224-23		17	i	13	ł
+	22	l 81	1 242 1		3378	238+25	1 1	<b>1</b> 5	Į	13	ļ
. :	23	1 82	243 1		3392 1	1 - 1		1	ł	14	1
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ļ	36	89	1 250 1		3489	99=11	-	8	l	14	ļ
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		91	~~ 252	1	3504=	3517	i	126-139	. 1	10	-	14	1
i	1 2	ı 92 i	253	i	3518-	3531	i	140*153		11	i	14	i
1	· 3	ı 93 i	254	i	3532-	3545	į	154-167		12	ì	14	i
1	4	94 (	255	ĺ	3546-	3559	Ì	168-161		13	i	14	i
-	5	I 95 I	256	1	3560-	3573	İ	182-195		14	Ĺ	14	Ė
- 1	6	96	257	1	3574-	3587	ı	196=209	1	15	ı	14	1
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- (	۵	98	259	J	3602=	3615	ł	224-237	ļ	17	Į	14	1
1	11 9 1	99	260	1	3615-	3429	ı	233+251	- 1	18	1	14	1
١	10	l 100 l	261	1	3630=		J	1 = 14	J	i	1	15	-
ı	11	- 101	595	1	3644=	3n57	ţ	15= 28	1	Ş	1	. 15	1
ı	12	102	263	J	3658-	3671	ł	29- 42	1	3	1	15	1
- 1	13	1-103 t	264	<b>†</b>	3672=	3585	ŧ	43+ 56		4	ı	15	t
•	14	104		1	3685-		1	57- 70	- 1	5	ł	15	1
- 1	15	105	266	1		3713	ł	71- 84	1	6	1	15	1
!	16	106	267	1		3727	ı	à5≖ 98	1	7	1	15	1
ļ	17	107	568		-	3740	ļ	99+111	1	8	ŀ	15	1
!	18	108	269	•	3741-	3754	1	112-125		. 9	1	15	ł
1	19	109	270	ļ		3768	1	126-139		10	İ	15	1
Į	20 1	110	271	1		3782	!	140-153		11	1	15	!
F	21 1	111 /	272	1	3783=		1	154-167	ł		1	15	!
1	22   23	113	273	1		3410	!	168-161	1	13	!	15	!
1	24	114	274 275	1	-	3×24	1	182-195	!	14	1	15	!
	25I	115	276	1	<del>-</del>	3438 3452	I	196-209		15	1	15	!
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í	27	117	278	ı i	-	3480 3480	Ŧ L	224-237	ŀ	17	1	15	1
1	26	118	278 279	1		3x3U 3x94	,	238=251	!	18	1	15	1
1	29	119	200	1		3494 3498	f J	1= 14 15= 28	l l	1	!	16	!
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1 - 1   121   282   3923 = 3936   43 = 56   4	
1 2 1 122 1 283 1 3937 - 3950 1 57 - 70 1 5 1	
1 3   123   284   3951 = 3964   71 = 84   6	16 I
1 4   124   285   3965 - 3978   45 - 98   7	16
1 5   125   286   3979-3991   99-111   8	16
6   126   267   3992-4005   112-125   9	16
1 7   127   268   4006-4019   126-139   10	16
8   126   289   4020= 4033   140=153   11	16
9   129   290   4034= 4047   154=167   12	16
10   130   291   4048   4061   168   181   13	16 I
11   131   292   4062-4075   182-195   14	16 I
1 12   132   293   4076- 4089   196-209   15	16 I
1 13   133   294   4090-4103   210-223   16	16 I
1 14   134   295   4104- 4117   224-237   17	16 I
1 15   135   296   4118 4131   238-251   18	16
1 16   136   297   4132  4145   1 14   1	17 I
1 17   137   298   4146+ 4159   15+ 28   2	17 I
1 15   138   299   4160- 4173   29- 42   3	17 I
1 19   139   300   4174= 4187   43= 56   4	17 I
1 20   140   301   4186 4201   57 70   5	17 I
1 21   141   302   4202-4215   71-34   6	17 I
1 22   142   303   4216- 4229   85- 98   7	17
1 23   143   304   4230- 4242   99-111   8	1 <u>7</u>
1 24   144   305   4243- 4256   112-125   9	17 I
-1 - 25   145   306   4257 - 4270   126 - 139   10	17 I
26   146   307   4271= 4284   140=153   11	17
27   147   308   4285- 4298   154-157   12	17
26   148   309   4299- 4312   168-181   13	17
29   149   310   4313- 4326   182-195   14	17
30   150   311   4327- 4340   196-209   15	17
1 31   151   312   4341- 4354   210-223   16	17

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1 3	į	154	1	315	t	4383=	4396	į	1 - 14	1	1	ı 18 l	l
<u>   - 4</u>	- 1	155	1	316	ļ	4397-	4410	1	15* 28	1	. 2	1 18	ł
5	- 1	156	1	317	1	4411-	4424	1	29• 42	1	3	1 18	ı
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1 7	. 1	158	1 ;	319.	1	4439-	4452	ţ	57+ 70	1	5	18	ł
1 8		159	1	320	1	4453=	4466	1	71- 64	1	6	i 18 I	١
9		160	1	321	1	4467-		1	85= 98	1	7	i 18 I	ı
1 10	1	161	1	322	]	4481=	4493	1	99-111	1	8	18	ı
1 11	- 1	162	1	323	1	4494-	4507	1	112-125	t	9	1 18 1	ı
1 12	- 1	163	1	324	1	450 <u>8</u> =	4521	1	126=139	1	10	-18	ı
1 13		164	1 .	325	1	4522-	4535	t	140-153	t	11	i 18 i	i
1 14	1	165	1	326	1	4536=	4543	1	154-167	1	12 `	18	ı
1 15	- 1	166	-	327	1	455ú=	4563	t	168*151	1	13	ı 18 I	ı
1 16	- (	167	ļ	328 -	1	4564=	4577	ļ	182-195	1	14	ı <u>1</u> 8	1
1 17	- 1	168	ļ	329	1	457a=	4591	1	196+209	1	15	18 !	ļ
1 16	- 1	169	}	330	1	4592=	4605	1	210-223	1	16	i 18 i	ŧ
1 19	t	170	ł	331	ł	4606=	4519	ŧ	224+237	1	17	ı 18 I	ĺ
1 20	- 1	171	}	332	1	4620-	4633	1	238-251	1	18	18	ł
21	į	172	ł	333	1	4634=	4647	-	1 = 14	1	1	l 19 l	t
55	- 1	173	1	334	1	4646-	4561	1	15- 28	1	2	ı 19 I	ı
1 23	- 1	174	}	335	1	4662-	4675	1	29= 42	1	3	i 19 i	ł
1 24	- 1	175	†	336	1	4676-	4689	1	43- 56	1	4	ı 19 l	ļ
1 25	1	176	ŧ	337	ł	4690-	4703	ł	57- 70	ŧ	5 5	ı 19. i	j
1 26	- 1	177	1	338	1	4704=	4717	i	71= 84	İ	6	ı 19 i	
1 27	1	178	†	339	ı	4718=	4731	ŧ	85 <b>=</b> 98	1	7	19 1	Į
35	1	179	ļ	340	1	4732-	4744	1	99-111	1	8	i 19 i	J
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	<b>-1</b>	182	t 343-	100	4773=	4786	+	140+153	3 -1	11	1	19	t
	1 2 (	183	344	1	4787=		1	154-16	7	12	١	19	1
	) "3:	184	345	1	4801 <del>-</del>		-	168=18:		13	Į	19	
	4	155	346	1	4815-		1	182=198		14	1	19	1
- 1	5	186	1 - 347	1	4829-		ŀ	196=209		15	ł	19	}
	6	187	1 348	!	4843=		ı	210+223		16	ļ	19	1
	J	188-	349		<b>4857</b> =		t	224-237		17	ı	19	į.
	8 1	189	350	ļ	4871=		1	238=251		18	1	19	1
	9 9	150		1	4835=		!	1- 14		1	ŀ	20	1
	10	151	352	!	4899-		1	15= 28		2	ŀ	20	!
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· · · · · · · · · · · · · · · · · · ·	14	-1 <del>9</del> 4	356	1	4941=		1	57* 70		5	!	50	!
	15	196		l.	4969-		1	71- 84		6	!	20	
ì	16	157	358	1	4983=	_	1	85= 98 99=111		7	1	20	1
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i	16	199	360	ì		5023	1	126=139	-	10	1	20 20	) 
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į	20 i	201	362	i		5051	i	154-167	,	12	<u>'</u>	50	r I
į	21	202		i		5065	ì	168-181	-	13	;	20	; l
į	52	503	364	ĺ	5046=		i	182-195		14	<u>'</u>	20	í
į	23	264-		į.	5080-		i	196-209		15		20	i i
İ	24 i	205	366	i	5094=		í	210-223		16	, 	20	1
- 4	<del>25</del> 4	- 2 <sub>U</sub> 6	367	į.	510a=		i.	-224-237		- 17	í	20	ì
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	· 29 · I	210	371	l		5177	1	ع+ +و <u>د</u>		3	i	21	ŀ
ı	30 (	211	372	ł	517a=		1	43= 56		4	i	21	İ
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i	3	215	37		5234-	_	i	99•1		8	1 21	i
ì	i. – 1	1 216	i 37:		5247•	5260	i	112-1		9	i 21	1
1	5	1 217	37		5261-		i	126-1	-	10	21	1
1	, 5	218	37		5276=		i	140-1		11	1 21	1
	7	219	380		5289-	-	i.	154-1			21	+
ï	8	1 550	38		5303-		i	168-1		13	1 21	1
í	9	221	38	_	5317-		1	182-1	95 J	14	1. 21	1
ï	10	1 222	38:		5331 •	5344	İ	196-2	ú9 Í	15	1 21	1
ĺ	11	1 223	1 38		5345-	-	i	210-2		16	21	1
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1	1	1 244	t -	~ 4U5	1	5638•	5651	1	1-14	1	· 1 ~	23	- 1
1	2	1 245	1	406	1	5652=	5665	-	15- 28	1	2	1 23	j
ł	3	246	ļ	407	1	5666=	5679	1	29- 42	1	3	1 23	1
ł	•	1 247	ı	408	ł			J	43- 56	í	4	1 23	- 1
ł	5	248	ł	409	ł	5694=	5707	- 1	57 <b>-</b> 70	•	5	1 23	1
ŧ	6	1 249	1	410	1	5708-	5721	+	71 - 84	1	6	1 53	1
· (	7	1520		411	ţ.	572 <i>2=</i>	5735	1	85- 98	t	7	1 23	1
- 1	8	1 251	1	412	1			-	99-111	1	8	1 23	-
l	9	1 252	1	413	1	5749-	5762	1	112-125	ŀ	9	1 23	1
ı	10	253	Į	414	1	5763 <b>-</b>	5776	1	126-139	1	10	1 23	1
H	11	1 254	1	415	1	5777 <b>~</b>	5790	ŧ	140=153	1	11	1 23	- 1
į	12	255	1	416	1	57 <del>9</del> 1 =	5204	1	154+167	1	12	1 23	- 1
1	13	256	ı	417	1	5805=		1	168-131	ļ	13	1 23	ŀ
ı	14	257	ı	418	1	5819-	5432	1	182•195	i	14	1 23	}
ł	15	258	-	419	1	5833=	5846	-	196-209	F	15	1 23	1
- (	16	1 259	ſ	420 *	1	5847-	5860	İ	210-223	ì	16	23	1
ŧ	17	1 290	ŧ	421	ł	5841 -	5874	1	224+237	j	17	23	1
- 1	18	1 261	1	422	1	5875-	5488	1	238=251	j	18	23	- 1
ł	- 19	1 505	ŧ	423	ł	5889+	5902	ı	1- 14	ł	1	24	- 1
-1	20	1 263	ļ	424	1	5903 <b>-</b>	5916	1	15- 28	1	2 (	24	. [
j	21	264	1	425	İ	5917 <del>-</del>	5930	1	29- 42	ı	3 !	24	1
ı	22	500	1	426	1	5931 <b>-</b>	5-144	i	43+ 56	ļ	4	24	-
ŧ	23	266	ŧ	427	1	5945-	5958	ı	57- 70	f	5 1	24	1
ŧ	24	1 267	1	428	1	595y <b>-</b>	5972	ŀ	71- 84	t	6 1	24	- 1
ł	25 -	568	ł	469	1	5973-	5986	1	85- 98	ŧ	7	24	ļ
1	26	1 269	1	430	1	5987-	5999	1	99+111	ŀ	8	24	1
+	27	1 270	1	431	ŧ	6000-	6013	1	112-125	Ì	9 1	24	j
-	29	271	i	432	1	6014-	6027	1	126-139	İ	10	24	
ł	25	272	1	433	1	602a=	6041	1	140-153	ł	11 1	24	- 1
1	30	273	ļ	434	1	6042-	6055	1	154-167	1	12 1	24	- {
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i	i	_	1	GMT	ŧ	FL	IGHT	ı	SPACE	CHAFT	1	REFERENCE	1	REF	CYCLE	ı
,		ATE		DAY			DAY	1	อิสธิ		1	ORBITS	i	DAY		i
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		1		27#	ŀ		435	- 1	6056=	6069	1	168-181	1	13	1 24	-
	)	2	ŧ	275	- 1		436	.	6070-	6083	ł	182-195	4	14	1 24	J
1	-	. 3	F.	276	1	-	437	1	6084=	6097	1	196-209	J	15	1 24	1
ļ	)	4	ŀ	277	ı		438	1	6098-	6111	1	210-223	1	16	1 24	- 1
i	l	5	1	278	1		439	1	6112-	6125	1	224+237	1	17	1 24	ŧ
i	l	6	1	279	- 1		440	1	6126=	6139	1	238-251	1	18	1 24	1
;- · ·	<b>-</b> ·	7		-590	• 1	·	441	1	6140=	6153	- [	1 = 14	1	1	1 25	1
	1	8	ŀ	281	1		442	1	6154=	6167	1	15= 28	1	2	ı 25	t
f	}	9	†	595	ŧ		443	1	6168=	6181	Į.	29- 42	1	3	1 25	1
	}	10	ļ	593	1		444	-	6182-	61,95	1	43= 56	ļ	4	1 25	١.,
	"	11	ŧ	264	1		445	1	6196=		1	57 <b>-</b> 70`	1	5	1 25	- 1
· 1	1	12	ŧ	285	ł		446	1	621ú-	6253	1	71 = 84	-	. 6	1 25	ł
-		13	· F	596			447	İ	6224-	6237	1	85- 98	ļ	. フ	1 25	ł
1		14	H	287	- F		448	1	623s=	6250	ı	99-111	ļ	8	25	1
- 1	) ·	15	İ	288	į.		449	i	6251-	6264	1	112-125	1	9	ı 25	1
1		16	İ	289	1		450	1	6265=		-	126-139	1	10	25	1
		17	ł	290	ŧ		451	1	6279 <b>-</b>		1	140-153	1	11	1 25	1
-		18	F	291	ł		452		6293-		1	154+167	1	12	1 25	-
1		19	l.	292	1		453	ł		6320	ł	168=181	ı	13	ı 25	ŧ
į		50	1	593	ļ		454	1	. –	6334	t	182-195	1	14	ı 25	, I
1		21	1	294	ļ		455	, 1	633a=		-	196-209	ļ	15	1 25	- [
į		55	ļ	255	!		456	1	6349-	6.462	1	210-223	ŀ	16	1 25	-
(		23	1	596	1		457	i	6363-	6376	1	224-237	ł	17	ı 25	- (
1		24	1	297	-		458	1	6377=	6390	ı	238 <b>-</b> 251	1	18	ı 25	ŀ
		52	1	298	Ţ		459	!	6391=	6404	1	1 = 14	1	1	1 26	ţ
- 1		26	1	299	!		463	!	6405=	6418	1	15 • 28	1	2	1 26	l
- {		27	1	300		,	461	!	6419=	6432	ı	29- 42	1	3	1 26	1
į		59	ı	301	ţ		462	1	6433-	6446	1	43= 56	1	4	1 26	ļ
(		29	ŧ	302	•		463	1	6447=	6450	t	57 <b>-</b> 70	1	5	1 26	
(		30	1	303	!		464		6461=	6474	1	71 - 64	1	6	1 26	ļ
ı		31	ţ	304	ł 	* **	465 		6475=	6483		#5 <b>-</b> 98	. 1	7	1 26	. ]

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	DATE	GMT DAY		SPACE		REFERENCE ORBITS		EF I	CYCLE No.	
	1	305	466	6489 <b>-</b>	6501	99+111	ļ <sup></sup>	8 1	26 24	1
	3	1 306 1 307	467    468	6516=	6515   6529	112=125 126=139	1	9   10	26 26	1
		1 307 1 308	1 469	6530=	6543	140=153	1	11	26	<u>'</u>
	4  5	1-309	1 470	6544=	6557	154-167	1	12 1	26	-
	1 6	310	471	6558+	6571	168=181	1	13	26	i
- +		-311-	_	6572	6585 T	182-195		14	. 26	] } -~
!	8		1 473	6586	6599 I	196-209	1	15	26	1
		, 312  -313		660u=		210-223	1	16	26	!
	10	·	475	6614=	6627	224=237	¦ .	17	26	<u>'</u>
		. 315 - 315	476	6628=		238+251	i	18	56	į
	12	316	1 477	6642=	6655	1= 14	ì	1 1	27	i
- 1	12   13	-317 -	· · · · · · · · · · · · · · · · · · ·	6656=	6669	15- 28	i .	2 1	27	i
	1 14	318	479	6670=		29- 42	i	3 i	27	i
	15	319		_	6697	43- 56	i	4 1	ŽŹ	i
	16	320	481	6698=	6711 I	57÷ 70	i	5 1	27	i
	   <u>1</u> 7	321	482 -	6712=	6725 H	71- 84	i	6 1	27	i
i	18	322	i 483	6726=	6739 i	85= 98	i	7 1	27	ì
	19	323	- 484	- 674U=	6752 1	- 99-111	į	á i	27	į
i	20	324	1 485	6753=	6766	112-125	1	9 1	27	1
	21	325	- 486 -	6767=	6780 I	126-139	İ	10 i	27	Ì
ĺ	22	326	487	6781=	6794	140-153	1	11 1	27	1
- · ·	23 -	327	1488 I	6795=	6808 1	154-167	1	12	27	1
	24	1 328	1 489 (	6809=	6822 1	168-181	1	13	27	ŀ
A 1940 - 1/4F	25	1-329	1490	6823+	6236 1	182+195	1 -	14	27	ŀ
	26	330	1 491 1	6837-	6350 I	196-209	•	15 I	27	1
	27	331	1 492 - 1	6851-	6864 1	210-223	1	16 I	27	1
İ	28	1 332	1 493 (	6865=	6×78 1	224-237	†	17 I	27	1
	1 25	333	l- 494 - (	6879=	6892 1	238=251	1	18 F	27	ļ
	30	334	I 495 I	6893=	6906	1- 14	1	1 1	28	1
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ı	1	335	1 496	1	6907-	6920	1	15= 28	1	.5	28	i
i	ē	336	1 497	i	6921-		i	29- 42	ì	3	28	i
i	3	337	498	i	6935-	6948	ì	43= 56	i	4	28	i
i	4	338	1 499	i	6949-	6962	i	57- 70	i	5	88	İ
i	. 5	339	1 500	j	6963-	6976	i	71= 84	i	6	28	ĺ
Ì	6	1 340	501	ĺ	6977-	6990	i	85- 98	Ĺ	7	28	Ī
1	7 ~	1341	1 502	1	6991-	7003	1	99-111	t	8	28 -	<b> </b>
١	8	342	503	l	7004-	7017	1	112-125	1	9	28	1
)	9	r 343	t 504	ŧ	7018-	7031	i	126-139	1	10	28	t
1	10	344	505	1	7032-	7045	-1	140-153	1	11	28	1
ł	11	i 345	1 506	1 .	7046=	7059	1	154-167	1	12	28	t
į	12	346	507	1	7060-	7073	1	168=181	1	13	28	1
	13	l" 347°′	1 508	1 1	7074=	7087	1	182-195	1	14	28	ŧ
	14	I 348	509	1	7088-	7101	- [	196-209	1	15	58	1
ŧ	15	349	510	1	7102-	7115	-	210-223	Ì	16	28	١.
į	16	350	511	1	7116=	7129	-	224-237	1	17	28	1
1	17 ***	351	512	i i	7130-	7143	- 1	238+251	1	18	58	l
-	ا 15	352	513	1	7144-	7157	t	1 = 14	1	1 1	29	1
ł	19	353	514	<b>†</b>	7158-	7171	ł	15- 28	ı	. S	29	1
١	20 (	354	515	i	7172-	7185	ŧ	29- 42	ţ	3	29.	ı
ţ	21 .	355	516	!		7199	-	43= 56	1	4	29	ļ
-	55 (	356	517	}	7200-	7213	1	57- 70	1	5 (	29	!
ŀ	23	357	518	!	7214=	7227	1	71 = 84	1	6 1	29	
1	24	358	519	!	7228-	7241	ł	85= 98	1	7	29	ļ
}	25	359	520		7242=	7254	1	99=111	ŧ	. 8 I	29	1
ļ	26	360	521	ļ	7255-	7268	1	112-125	!	9	29	!
•	27 1	361	1 522	1	7269=	7282	ļ	126-139	!	10 !	29	
ı	28 I	362	1 523	1	7283-	7296	!	140-153	ľ	11 1	29	!
ŧ	29	363	524	1	7297-	7310	1.	154-167	ļ	12	29	
١	30	364	525	1	7311-	7324	1	168-181		13	29	i
1	31	365	526	} 	7325~	7338	!	162-195	!	14	2 <b>9</b>	i

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1	1 1	1 1	527	t	7339- 7352	Ì	196-209	1	15	29
ı	S 1	2 (	528	ł	7353- 7366	1	210-223	ŀ	16 1	29
1	3 1	3 (	529	1	7367- 7380	1	224-237	1	17	29
-	4 (	#	530	1	7381 - 7394	-	238-251	١	18	29 I
J	5 1	5	531	1	7395- 7408	- 1	1 - 14	ı	1 1	30
1	6 1	6	532	i	7409- 7422	ł	15- 28	1	2 1	30 j
ł	· 7 ···	7 1	533	-	7423- 7436	1	29- 42	i	3 1	30
- 1	ර	8	534	1	7437- 7450	J	43 <b>-</b> 56	ļ	4 1	30 I
1	9	9, 1	535	1	7451- 7464	1	57 <b>-</b> 70	Į	5 1	30 (
1	10	10	536	1	7465- 7478	- [	71 - 84	1	6 1	30 1
1	11	11	537	1	7479- 7492	1	85÷ 98	ļ	7 1	30 I
1	12	12	538	1	7493- 7505	1	99-111	ı	8 1	30 1
ŧ	13	13	539	1	7506- 7519	1	112-125	ŧ	9 1	30 1
ł	14	1#	540	1	7520+ 7533	1	126-139	1	10 1	30
1	15 l	15	541	ŧ	7534- 7547	1	140-153	1	11	30 l
1	16	16	542 -	1	7540- 7561	1	154-167	1	12	30 1
ł	17	17	543	1	7562- 7575	1	168-161	1	13	30
1	18	18	544	1	7576- 7589	1	182-195	1	14 1	30
1	19 1	-19	545	ŧ	7590+ 7603	1	196-209	1	15 1	30
1	20	20	546	1	7604- 7617	1	210-223	ļ	16 1	30 1
1	21	21	547	ł	7618 <b>-</b> 7631	1	224-237	1	17	30 I
1	55	22	548	1	7632- 7645	i	238-251	t	18 1	30
1	23	23 (	549	ı	7646 7659	ļ	1 = 14	İ	1 1	31 I
1	24 1	24	550	ì	7660- 7673	1	15= 28	1	2 1	31 1
1	25 i	25	551	į	7674- 7687	ŀ	29- 42	1	3 1	31 I
1	26	ا 6 ع	552	1	7638 - 7701	1	43 - 56	1	4 1	31
ŧ	27	27 1	553	i	7702- 7715	ŧ	57- 70	ŧ	5 l	31 (
ı	28	28	554	1	7716- 7729	1	71= 84	1	6 1	31
1	29	29	555	Í	7730- 7743	1	ห5 <b>=</b> 98	1	7 1	3 <u>1</u>
1	30	30 1	556	1	7744- 7756	1	99-111	1	8 1	31 l
ł	31	- 31 1	557	ł	7757- 7770	1	112-125	١	9 1	31
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-	r - <b>t</b>	1 35 . (	558° ~	1	7771=	7784	1	126-139	ı	10 1	31	
	2	1 33	559	1	778a-		1	140-153	Ì	11	31	
-	- 3	1 34 1	560	1	7799=		-1	154=167	1	12 1	31	
ļ	4	1 35,1	561	ı	7813-	7826	-1	168=181	-	13	31	
1	5	36	562	1	7827-	7×40	1	182-195	1	14	31	
l	6	1 37	563	1	7841+	7854	1	196-209	1	15	31	
· '[	7 7	1 - 38 -	. J	t	7855-		- 1	210=223	ŧ	16	31 i	,
	ا ا	1 39 1	565	1	7869-	-	1	224=237	į	17 1	31	
- 1	9	1 +0 1	566	)	7883-	7496	ţ	238-251	,1	18 (	31 l	
ı	10	1 41 1	567		7897 <b>-</b>	7910	1	1 = 14	1	1	32	
	11	42 1	568	ĺ	7911-		1	15= 28	1	2 1	32	
- 1	12	1 43	569	İ	7925 <b>-</b>		1	29 + 42	ł	3 1	32	
- 1	13	44			7939-	7952	1	43 <b>-</b> 56	ı	4 1	32	
ı	14	1 45 1	571	l	7953-	7966	1	57 <b>-</b> 70	F	5 1	32	
Ì	15	1 46 1	572	)	7967-	7980	ł	71 = 84	1	6 1	32 1	
ا	16	1 47 1	573	!	7981=		-	85* 98	ŧ	7	35 1	
,	17	1 48	574	٠.	7995-		ŧ	99-111	1	8	32	
ŀ	18	1 49 1	575	l	8008-		ļ	112-125	1	9 1	32	
	- 19	1 50 1	576		<b>-</b> 5508		ł	126=139	ł	10 1	32 1	
ŀ	.50	51	577		a03a=		1	140-153	1	11 1	32	
ļ	21	52	578		8050-		!	154-167	Ť	12 1	35 1	
ļ	2 <u>2</u>	53	579	l	8064=	80 <b>77</b>	-	168-181	1	13	32	
į	23	54	580 l		8075 <del>-</del>	- 4,	ł	182-195	1	14	35 1	
ļ	24	55	561		8092-		1	196-209	1	- <b>1</b> 5 T	32	
•	25	56	582°		8106-		1	210-223	1	16	3 <b>5</b> l	
!	26	1 57	,583 l		8120-	8133	1	224=237	1	17	35	
1	27	) 56 l	564		8134=	8147	1	238=251	1	18 (	32	
1	28	1 59 I	585 I		8143=	5151	[	1 = 14	1	1 1	33 i	
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		1 - 60-1	586	8162- 8175		15+ 28 ···	1, 2,5 1	33 1
	į Ž	61	587	8176- 8189	1	29- 42	3 1	33
	3	1 - 62 - 1	588 1-	8190- 8203	-1	<b>43 •</b> 56	1 4 1	<b>33</b>
i	1 4	63	589 1	8204- 8217	ŧ	57 <b>-</b> 70	1 5 1	33 1
	5	1 - 64 -	1 595 T	8218- 8231	- 1	71- 84	1 6 1	33 (
	6	65	l 591 l	8232- 8245		85= 98	1 7 1	33 -
	j7		15 <del>9</del> 21	-8246= 8258	1.	99-111	1 8 1	33
	8	1 67 !	1 593	8259- 8272	-	112-125	I 9 I	33 (
	h	1 68	594	8273- 8286		126-139	1 10 1	33
	10	1 69	1 595	8287- 8300		140-153	111	33
	f 11	70	596	8301- 8314	_	154-167	1 12 1	33
	12	71	597	8315= 6328		168-131	1 13	33
	1900	172		-8329+-6342		182 <b>-1</b> 95	1 14 1	33
	1 14	1 73	599	8343- 8356		196-209	15 1	33
. ^	15	1 74-	600 -	8357- 8370		210-223	1 16 1	1 33 t 1 33 t
	16	, , –	601	8371= 8384 8385= 8396		224 <b>-</b> 237 238 <b>-</b> 251	1 17     18	33     33
	17	1····76 · I 77 ∣	l 603 l	8399= 8412	-	1+ 14	, 10 i	34
	18  -1 <del>5</del>	//    78	1 603 1 1604 - +	8413- 6426		·· 15= 28	2	34
	• –	· -	605 I	8427 8440		29- 42	1 3 1	34
	20   21	• • •	1 606 1	6441~ 8454		43= 56	1 4 1	34 I
_	55	1 51	1 607 1	8435= 8468	-	57 <b>-</b> 70	, <del>,</del> ,	34
	. 23	1 82	608	8459- 6482		71 - 84	6	34 1
	1 24,	1 83	1 609 1	8483- 8496		a5= 98	7	34 I
	25	84	610	8497- 8509		99-111	1 8	34 1
	26	85	611	a510= 8523		112-125	9	34 1
	27	56	1 612 1	8524- 8537		126-139	10	34 j
	20	87	613	8538= 8551		140-153	1 11	1 34 J
	. 29.	88	614	8552- 8565		154-167	1 12	34
	1 30		1 015 1	8566- 8579		168-141	13	34
	31 -	90		8580= 6593		182-195	1 14	34 1
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	2 1 92	618	8608= 8621	210-223	1 16 1	34
	3 93	619	8622- 8635	1 224-237	i 17 i	34
	4   94	1 620 1	8636- 8649	1 238-251	1 18	24
	595	621	8650- 8663	1 1 14	1 1	35
	6 1 96	1 622 1	8664- 8677	15- 28	1 2 1	35
• •	97	t	"8678+"8691	29- 42	1 31	35 1
	6   98	624 1	8692- 8705	1 43- 56	1 4 1	35
		625	8706- 8719	57= 70	1 5 1	35 I
.	10   100	1 656 1	8720- 8733	1 71 84	<u>il</u> 6 l	35 I
	11 101	1 627 1	8734- 8747	85= 98	7 7 1	35 I
-	12   102	1 828 1	874a <b>-</b> 8760	I 99 <b>-111</b>	1 8 1	· 35
	13   103	1 629 1	8761- 8774	1 112-125	1 9 1	35 I
l	14   104	630 1	8775- 8788	126-139	1 10 1	35
	15 105	631	8789- 8802	1 140-153	1 11 1	35
1	16   106	635	8803- 8816	1 154-167	1 12 1	35
	17	1 633 1	8817 <del>-</del> 8830	168=181	1 13 1	35
ļ	18   108	634	8831- 8844	1 182-195	1 14 1	35
	19-1-109-		8845= 8858	196-209	1 15 1	
l	20   110	636	8859- 8872	210-223	16 1	35
_ [	21 111	637	8873- 8886	1 224-237	. 1 27 1	35
	22   112	638	8887- 8900	238-251	181	35
	23   113	639	8901- 8914	1 1- 14	1 1	36
1	24   11#	1 640	8915= 8928	1 15= 28	2 1	36
	25 - 115	641	8929= 8942	29-42	3 1	36
	26   116	1 642 1	8943- 8956	1 43- 56	4	36
- 1	27   117	643	8957- 8970	57- 70	1 5 1	36
	28   116   29   119	644     645	8971= 8984 8985= 8998	71 = 84	1 6 1	36
	30   120	1 646 I	8985= 8398 8939= 9011	85= 98	1 7 1	36
	30   160	! 076	0222 2011	99-111	6   <b>-</b>	36

MAY, 1974

and the same transfer of the s

_				_					·			<b>-</b>		_		
i		1	GMT	1	F	IGHT	1	SPACE	CHAFT	1	REFERENCE	1	REF		YCLE	1
ì	DATE	i	DAY		• •	DAY	i		IIS	ŧ	BRBITS	ï	DAY	• •	NO.	i
							·		413	·		 		' :		
ŀ	· ··· •	t	121	ı		647	1	9012=	9025	1	112-125	ì	9	 I	36	1
i	Ž	i	122	i	•	648	i	9026=		i	126-139	ì	10	i i	36	i
i	ā	į.	123	į		649	i	9040-		i	140-153	i	11	i	36	i
Ì	4	ŀ	124	ı		650	1	9054-	9067	1	154=167	i	12	j	36	i
1	5	ı	125	1		65i	ì	9068=	9081	1	168-181	i	13	ì	36	ì
i	6	1	126	ţ		652	j	9082-	9095	i	152-195	ì	14	Ì	36	i
ŀ		<b>.</b>	127	٠. ا		653	1	9096-	9109	j	196-209	Ì	15	i -	36	İ
ŧ	8	ŧ	128	I		654	1	9110-	9123	1	210-223	1	16	i	36	1
ı	9	ı	129	Ŧ		655	1	9124-	9137	ł	224-237	1	17	ı	36	1
-1	10	į.	130	1		656	ŧ	9138=	9151	ŧ	238+251	١	1a	ĺ	36	İ
1	11	1	131	Ŧ		657	1	9152-	9165	1	1 - 14	1	1	ı	37	1
ı	12	ı	132	1		658	1	9166=	9179	1	15- 28	1	2	l	37	j
1	-13	ŀ	133	ŧ		659	1	- 9180 <b>-</b>	9193	ł	29- 42	4	3	٠ ا	37	1
ł	14	ŧ	134	1		660	1	9194=	9207	1	43- 56	ł	4	l	37	J
ŧ	15	ı	135	ŀ		661	1	9208-	9221	1	57- 70	1	5	ı	37	1
1	16	ŧ	136	ŧ		662	1	9222-		1	71 * 84	ŧ	6	l	37	1
į	17		137	H		663	ı	9230-		1	85= 98	1	7	l	37	ŧ
- 1	18	ł	138	İ		664	İ	9250-		ı	99~111	1	8	l	37	1
ł	19	ł	139	ł		665	ł	9263-		ŀ	112-125	1	9 (	ŀ	37	1
j	50	ł	140	ı		666	İ		9290	1	126-139	1	10	1	37	1
1	21	1	141	ŀ		667	1	9291=	9304	İ	140-153	1	11	i	37	i
Ţ	55	!	142	ļ		668	1	9305-	9318	1	154-167	I	12	J	37	1
ł	23	1	143	Ţ		669	ı	9319-	9132	i	168-181	1	13	l	37	ļ
1	24	ł	144	1		670	1	9333-	9346	1	182-195	1	14	ı	37	ļ
!	25	1	145	!		671	+	9347-	9360	ł	196-209	ı	15		37 -	ĺ
į	26	ļ	146	ļ		672	Į	9361-	9374	!	210-223	1	16	l	37	
1	27	1	147	ŀ		673	j	9375=	9388	1	224-237	H	17	!	37	1
I	28	Į.	148	[		674	1	9389-	9+02	!	238-251	1	18		37	1
1	29	1	149	ļ		675	ţ	9403-	9416	ļ	1- 14	1	1		38	
ļ	30	<b>!</b>	150	1		676	!	9417=	9430	!	15- 28	!	5		38	!
1	31	† <del>-</del> -	151	; -		677	<b>‡</b>	9431-	9444	!	29+ +2	ł	3 (		38	į

JUN# 1974

4.		GMT I	- FI-IGHT	SPACE	CRAET 4	REFERENCE	J. REF J	CYCLE I
1	DATE	DAY	DAY	1 18KB	ITS 1	eRBITS	I DAY I	NO .
•			· · · · · · · · · · · · · · · · · · ·					
1	1	152 1	678	9445=		43+ 56	1 4 1	38 (
ļ	2	153	679	9459~		57 <b>-</b> 70	1 5 1	38 1
- 1	3 1	154	680	9473-		71 = 84	1 6 1	38
ŀ	4 !	155	681	9487-		85- 98	7 !	38 I
ŀ	· 5 · t	156	652	9501-		99=111	1 8 1	38
ļ	6 1	157	683	9514~	9527	112-125	9 1	38
Ī	7	158	684	9528=		126-139	1 10 1	38
!	8 1	159	685	9542=	-	140-153	111	38 i
-	9	160	686 I	9556=		154-167	1 12 1	38
	10	161	687 J	9570 <del>-</del>		168+181	1 13 1	38 J
` <b>!</b>	11 1	162	688	9584=		182-195	1 14 1	38 j
!	12 1	163	689	9598=	_	196 <del>-</del> 209	1 15 1	38
Ţ	13	16	~690 I	9612*		210-223	1 15 1	
!	14	165	691	9626=		224+237	1 17 1	38
!	15 I	166	692	9640=		238-251	1 18 1	38
	16	167	693 - 1	9654-	9667	1- 14	1 1	39
1	* 17 · · ·	168	694	9668=		15= 28	1 2 1	39
1	18	165	695 I	9682=		29= 42	1 3 1	39
1	19	170   171	696	9696=		43= 56	4	39
!	20		697	9710-		57 <b>-</b> 70	5 1	39 I
!	21	172	698	9724=		71= 84	1 6 1	39
ŀ	55	173	699	9738=	9751	85-95	7 1	39 I
1	23	174	700 1	9752		99=111	1 3 1	39
ŀ	24	175	701 (	9765-		112-125	1 9 1	39
1		176	702	9779=	9792	126-139	10 i	39
ļ	26	177	703 1	9793•		140-153	1 11 1	39
-	27 +	178	704	9807=		154=167	1 12 1	39
ļ	28	179	705	9821 •	9834	168-181	1 13 1	39
ļ	25	160	· 706	9835		182-195	1 14 (	39
ı	30 I	181	707 I	9849=	9862	196-209	15	39

JUL>1974

		·				·	- <b>-</b>		
		I GMT	Filight	SPACECRAFT	- <del>-</del> -	REFERENCE	I REF	I CYCLE I	
ì	DATE	1 DAY	DAY	#RBITS	·i	SREITS	I DAY	NO .	
						*******			
	<b>-</b>	1-182-	I708	9863- 9876	1	210+553	1 16	i 39 t	-
1	2	183	1 709	9877- 9x90	1	224+237	1 17	1 39 1	
	···· 3 ···	1-184	1 710 (	9891 - 9904	1	238-251	18	1 39 1	
ı	4	1 155	1 711 1	9905- 9918	į	1- 14	1 1	1 40 1	
1	5	1-186	1 712 i	9919- 9932	ł	15- 28	1 2	1 40° F	
١	6	1 187	1 713 4	9933- 9946	1	29- 42	1 3	1 40 I	
		1-188 -	+714	9947- 9960	1	" #3 <b>=</b> 56"	1 - 4	r ~ 40 ~	
	ä	189	715	9961 - 9974	ļ	57 <b>-</b> 70	1 5	1 40 1	
	9	1-190	716	9975- 9988	ł	71 - 84	1 6	1 40 1	
ļ	10	191	717	9989-10002	1	55+ 98	7	1 40 1	
	11	192	718 - 1	10003-10015	1.	99-111	1 8	1 40 1	
!	12 - 13	1 193	719	10016-10029	!	112-125	9	1 40 1	
	-	1-194	720	10030-10043	†	126=139	1 10	1 40 1	-
	14 15	1 195	721 (	10044-10057	!	140=153	1 11	1 40 1	
· · · · · · · · · · · · · · · · · · ·	16	196   197	722    723	10058=10071	!	154=167	1 12	1 40 1	
	17	198	724	10072=10085 -10036=10099	1	168 <b>÷</b> 181	13	1 40 1	
i	18	199	725	10130-10133	1	1×2+195 196+209	14   15	1 40   1 40	
4	19	200	1 726 - 1	-10114-10127	.I.	210-223	16		
i	20	201	727	10128=10141	ì	224-237	17	1 40	
	21	202	728	10142-10155	-	238=251	18	1 40 1 1 40 1	
i	25	203	1 729 I	10156-10169	i	1= 14	1	, 40 ; , 41	
- i	23	204	i 730 i	10170-10183	i	15= 28	5	; <del>41</del>	
i	24	205	731	10134-10197	i	29- 42	3	41	
+	25	206	1- 732	10190-10211	. į.		- 4	41	
i	26	207	733	10212-10225	i	57 <b>+</b> 70	5	41	
j	27	805	734	10226-10239	į.	71 = 64	6	41	
ı	28	209	735 1	10246-10253	i	á5= 98 i	7	41	
· · · }	- 29	210	736	10254-10266	1 -	99-111	8	41	
- 1	30	211	737	10267-10280	i	112-125	9	41	
- }	31	212	7.38	10281-10294	ĺ	126=139	10	41	
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AUG. 1974

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1		I GMT	- t-Fi	IGHT	-	SPAC	ECRAFT	1	REFERE	TOCE I	REF	1 CYCLE	ŀ
ŧ	DATE	I DAY	"	DAY	ŧ	₿R	BITS	1	0RBI	TS I	DAY	NB+	1
-		1 213		739		10296	-10308	·	140-1	53 1	11	1 41 <sup>-</sup>	ľ
¦	Ş	1 21#	Ï	740	İ		<b>-10332</b>	1	154-1		12	41	Í
ĺ	· 3	1 215	1	741	İ	10323	-10336	1	168-1	81 J	13	1 41	ŧ
- 1	4	1 216	1	742	ŀ		-10350	1	182•1		14	+1	1
Ţ	5	1 217	)	743	- 1		-10364	1	196•2		15	1 41	•
1	6	1 218	1 .	744	. [		-10378	-	210-2		16	41	!
1	7	1-219	<b>†</b>	745	- 1		-10392	1	224-2	•	17	1 41	!
- {	8	1 550	l	746	ţ		-10406	ļ	538-5		18	1 41	l
-	9	1 221	ı,	747	į		-10420	1	•	14	1	1 42	ļ
1	10	522	!	748	l :		-10434			28 1	2	1 42	•
ţ	11	1 553	1	749	!		-10448	ļ	29•,		3	1 42	} !
ı	12	1 224	!	750	!		-10462	!		56 I	4	1 42	
ţ	13	1 225	1	751	T		-10476	Ţ	57•	70	- 5	142	!
- 1	14	1 226	j	752	!		-10490 -10504	1		34 I 98 I	- 6 - 7	1 42	1
1	15	1-227	!	753	. !		-10504	i	99•1		a a	1 42	l l
1	16	1 228		754 ` 755	1		-10517 -10531	!	1.12-1		9	1 42	!
1	17	1 230	!	755 756	-		-10531 -10545	- [	126=1		10	1 42	l I
L	18 19	1 231	, , , , , , , , , , , , , , , , , , ,	757	- 1		-10559	- 1	140-1		11.	• • •	į
ı I	20	535	i	758	ì		-10573	i	154-1		12	1 42	i
	21	1 233	i	759		<b>.</b> – –	-10587	ì	168=1		13	1 42	i
j	55	1 234	i	760	i		-10601	ì	182-1	_	14	42	i
'n	- 23	1 235		761	i		-10615	í	196-2		15	1 42	ı
i	24	236	i	702	i		-10629	i	210-2	23 i	16	1 42	İ
	~ <u>2</u> 5 ~	+ 237		763	1	10630	-10643	ł	224-2	37	17	1 42	į
í	26	1 238	1	764	ĺ	10644	-10657	-1	238=2	51 i	18	1 42	į
i	- 27	1 239	1	765	İ	10658	-10671	1	1 -	14	1	1 43	
ı	25	1 240	ł	766	ļ	10672	-10585	- 1	15-	28 1	2	1 43	
i	29	1 241	1	767	ł	10686	+10699	- 1	29-	42 1	3	1 43	
i	<b>3</b> 0	1:242	•	768	į	10700	-10713	j	43=	56 1	4	1 43	١
- 1	31	1 243	<b> </b> · · · ·	769	* ‡	10714	-10/27	1	5 <b>7-</b>	70 1	5	1 43	ļ
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SEP.1974

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	1	GMT	1	FI IGHT	1	SPAUECRAFT	1	REFERENCE	I REF I	CYCLE	ŀ
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	I DATE I	UM!	<u>'</u>	05	. <u>'</u>	000113	_ ' :	UNDIIO			· -
	ls 1 1	244		770	1	10728-10741	 1	71- 84	1 6 1	43	į
,	1 + 1	245		771	1	10742-10755		85= 98	, 6 i	43	ì
	) 2     3	546	1	772	1	10756-10768	- 1	99-111	1 8 1	43	Ϊ.
	3	247	ï	773	į	10769-10782	i	112-125	, <u>, , , , , , , , , , , , , , , , , , </u>	43	ï
	, , , , , , ,	248	1	774	1	10783=10782		126=139	1 10 1	43	i
	, p	249	!	775	ì	10797-10810	1	140-153	111	43	ì
	, 6 , 1 7 - 1	520	,	776	- I	10811-10824	1	154-167	12 1	43	i
	8 1	251	Ţ	777	1	10821-10824	-	168=181	1 13 1	43	ì
	1 0 1 1 9 1	252	•	7778	-	10839=10852	-	122-195	1 14 1	43	!
,	•		1		!		!			43	!
1	10	253	•	779	!	10853=10866	- [	196-209	15 (		1
	11	254	1	780	!	10867+10880	!	210-223	1 16 1	43	!
	12	255	1	7ŏ1	!	10881=10394	- !	224-237	1 17 1	43 43	•
	- 13	256	•	782	ŀ	10895-10908	!	238-251	18 1		1
	14	257		783	1	10909-10922	- [	1-14	1 1	44	1
	15	258	1	784	1	10923=10936	-	15= 28	1 5 1	44	!
	1 16	259		785	!	10937-10950	1	29- 42	] 3	44	į
	l 17 i	500	ł	7 <b>5</b> 6	1	10951=10964	1	43= 56	4 1	44	1
	1 15 1	261	Ŧ	787	1	10965-10976	- 1	57* 70	5 1	44	!
	- 19 -	565	1	768	1	10979-10992	- 1	71- 84	6	44	!
1	1 50 1	563	1	789	- [	10993-11006	- 1	55 <b>~</b> 98	7 1	44	ļ
!	21	50#	ţ	790	ŀ	11007-11019	ļ	99-111	8 1	44	!
	1 55 1	265	ŧ	791	ı	11020-11033	-	112-125	1 9 1	44	ļ
	i 23 i	564	ŧ	792	İ	11034-11:)47	١	126-139	1 10 1	44	1
	1 24 1	267	1	793	1	11048-11061	- 1	140-153	11 1	44	ł
- :	25 - I	269	·· 🛉	794	1	11062-11075	ŧ	154-167	1 12 1	44	1
	26	269	ł	795	1	11076=11089	1	168-181	131	44	ŀ
	l 27 I	270	ł	796	1	11090-11103	- [	182-195	14	44	1
	28	271	ł	797	Ĺ	11104-11117	- 1	196-209	15	44	ı
	l 29 I	272	ŧ	798	1	11118-11131	1	210-223	1 16 1	4#	١
	) <b>3</b> 0	273	ŧ	799	1	11132-11145	-1	224-237	17	44	I

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	GMT.	FI IGHT	SPACECRAFT   REFERENCE   REF	CYCLE I
I DATE	DAY	DAY	BRBITS   BRBITS   DAY	NЕ I
71	274	800	11146+11159   238-251   18	44
1 2	275	<b>8</b> 01	11160-11173   1- 14   1	45
117 3 71	276	802	11174=11187   15+ 28   2	45 <u> </u>
	277	803	11188-11201   29- 42   3	45
··• 5 · · · [	278	804	11202-11215   43- 56   4	45
1 6 (	279	805	11216-11229   57-70   5	45 I
···   ···· · · · · · · · · · · · · · ·	280	806	11230-11243   71-84   6	45 I
1 8	281	807	11244-11257   85- 98   7	45 I
9 (	585	808	11258-11270   99-111   8	45   45
10	283	809	11271-11284   112-125   9	45 I
1 11	284	810	11285-11298   126-139   10	45
1 12	285	811	11299-11312   140-153   11	45 I
13	286	~ 812	11313-11326   154-167   12	45 I
1 14 1	287     288	813 814	11327*11340   168*181   13   11341*11354   182*195   14	45 I
15	589	815 -	11355-11365   196-209   15	45 I
1 16 1	290	816	11369=11382   210=223   16	45 1
	291	817	11383=11396   224=237   17	45 I
1 18	555	818	11397-11410   238-251   18	45 I
1 20	293	819	11411+11424   1+ 14   1	46
21	294	820	11425-11438   15-28   2	46
1 22 1	295	820 ( 821 (	11439-11452   29- 42   3	46
- 23	296	822	11453-11466   43- 56   4	46 1
1 24	297	823	11467-11480   57- 70   5	46 I
25	298	824	11481-11494   71- 84   6	46
1 26	299	ø25	11495-11506 1 85- 98 1 7 1	46 İ
27	300 I	£26	11509-11521   99-111   8	46
1 26	301 I	827 I	11522-11535   112-125   9	46
29	302	828	11536-11649   126-139   10	46
1 30	303	829	11550+11563   140+153   11	46
31	304	830	11564-11677   154-167   12	46 I
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		I GMT	FI IGHT	I SPACECRAF	T I REFERE	NCE I REF	I CYCLE I
	DATE	I DAY	F DAY	1 ORBITS	· I · BRBI	ITS I DAY	/   N8
•			****				
	1	305		1 11578 - 1159			
	1 5	306	1 832	1 11592-1160			
	† 9 ···	1 307 1 308	833	1 11606-1161			
	l <b>▼</b>   5	309	834	1 11620-1163			• • • • •
			835	1 11634-1164			
	l 6     <b>7</b>	310	1 836	1 11648+1166			
	, ,	311-	·	1 11662-1167		141	•
	&  9	312	838	1 11676-1168		28   3	
	•	313	839	1 11690=1170		42   3	
	10	31 <del>4</del> 315	840	1 11704-1171		56 1 4	
	1 11	–	841	1 11718-1173			
	12   <del>1</del> 3	316 - 317	1 842 1843	1 11732-1174	- • •	84   6	
	14	318	844	+ 11746=1175			
	17    15	319	! 074 845	11760-1177			
	1 16 I	320	646	1-11773-1178			
	17	321	1 647	11787=1180   11801=1181			
	16	355	1 848	11815=11×2			
	-19			+ 11829=1184		· · · · · · · · · · · · · · · · · · ·	
	20	324	1 850				
	- 21 H	325	l 851	1 11843-1185		, -	• • •
	ן צָל ן	326	l 652	11857=1187   11871=1188			•
	23	327	1 653				
	24	328	1 854	1 11885-1189		- , - ,	
	25	359	1 855	1 11899-1191			
1	26	329 02E	1 856	1 11913-1192	- ·		• • •
	27	331	l 557	11941-1195	- · • -		
ļ	26	332	1 658	1 11955-1196	_	42   3	
	29	333	وده ا ووج ا		· · · · · ·	56   4	, , , , , ,
1	30 I	334		1 11969-1195		70 f 5	. ,
	VC	JJ7	გნე	1 11983-1199	6   71 <b>-</b>	84 I 6	48 1

1		L.GMT I	F. IGHT 1	SPACECHAFT	l	REFFRENCE	ı	REF I	CYCLE I	
1		DAY	DAY	GRBITS	1	ORBITS	Ť	DAY I		
•	PARES.	i ku Hebebbe								•
	1	335	861	11997-12010	1.	85 <b>-</b> 98	1	7 1	···· 48 ··· (	
Ì	5	336	862	12011-12023	1	99-111	1	8 1	48 (	
1	3	337 1	863 1	12024-12037	1	112-125	1	9 I	48	
	4	338	864 i	12036-12051	1	126-139	ŧ	10 1	4.8	
. 1	5	1 339 1	865	12052-12065	1	140-153	Ì	11	48	ii
	1 6	1 340	866 I	12066-12079	1	154=167	1	12	48	
i	7	1 341	867 1	12080-12093	1.	168-151	1	13 1	48	Ī
.	1 b	1 342 1	868	12094-12107	-	182-195	1	14 1	48	1
	9 -	1 343 (	869	12106-12121	1	196-209	1	15 I	48 i	 
	10	1 344	l 870 l	12122-12135	1	210,-223	1	16 1	48 1	) }
	1 11	1 345	l 871 l	12136-12149	1	224-237	!	17	48	 
	12	1 346	l 872 l	12150-12163	1	238-261	1	18	48	r L
	⊩ ″ <b>13</b>	1 347	873 1	12164-12177	1	1 - 14	Ĭ.	1 !	49	
	i 14	1 348	I 874 I	12178-12191	!	15= 28	!	2	49   49	) L
	15	1 349	8 <u>7</u> 5	12192-12205	!	29= 42	!	3 1	49   49	<i>}</i>
	16	1 350	876	12206=12219	1	43P 56	!	4 ]	49	) 1
	1 17	351	877	12220-12233	!	57- 70	1	5 1	49	j L
	18	352	878	12234-12247	ļ	71= 84 85= 98	1	6 I	49	
	19	1-353	· ····879	12248-12261	!	99+111	1.	. /! 8 i	49	, 
	1 50	1 35#	1 880 I	12262 <b>-</b> 12274   12275 <b>-</b> 12286	,	112-125	1	9 1		]
	21	1 355	851	12289-12302	1	126=139	1	10 1	49	i I
	1 55	1 356	882	1 12303-12316	1	140=153	į	11 1	49	i
	1 - 23	1 357 1 358	1 884   1 884	1 12317-12330	i	154-167	i	12 1	49	İ
	1 24	1 350 1 359	664    865		i	168-181	i	13 i	49	ł
	125	1 360	l 886 1	1 12345-12358	i	182-195	i	14	49	ĺ
	26   27	1 360 1 361	1 857	12359-12372	i	196-209	i	15	49	İ
	1 28	1 361	1 558 I	12373-12376	i	210-223	i	16	49	ĺ
	1 29	1 363	1 869	1 12337-12400	i	224-237	i	17	49	1
	1, 29	364	890	12401-12414	i	238-251	i	ាំ ខ្ញុំ	49	į
	30  - 31	1 365	ł 891	1 12415=12428	i	1= 14	ì	1	50	1
	1 21	, 363		, ,_,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						_

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Ī	)	I GMT I	Filight	1	SPACECRAFT	1	REFERENCE	1	REF I	CYCLE	ī
i	DATE	DAY	DAY	i	BRBITS	İ	ORBITS	İ	DAY I	N8 •	i
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1	1 1	<u> </u>	892	ł	12429-12442	İ	15 - 28	1.	5 1	50	t
- (	2	1 2 1	893	ļ	12443-12456	!	29- 42	- I	3 1	50	ļ
-	. 3	1 3 1	894	- !	12457-12470	-	43- 56	ł	4 1	50	1
	4	4	895	!	12471-12484	-	57- 70	- 1	5	50	ł
1	5	1 51	896		12485-12498	-	71 * 84	-	6 1	50	!
	6	1 6 1	897	. [	12499-12512	-	85 <b>+</b> 98	- [	7 1	50	!
- 1	·· 7	7   8	- 898 - 898		12513-12525	•	99=111	!	8 (	50	!
	8	1 9 1	899	!	12526-12539	!	112-125	ı	9 1	50 50	!
	9	•	900	١	12540-12553	!	126=139	-!	10 1	50 50	!
	10	10   11	901 902	!	12554=12567 12568=12581		140=153 154=167		11	50	!
1	11	12	902 903	1	12582=12595	1	1545167 1685181	ŀ	12   13	50 50	1
1	13	13	904	1	12596-12609	1	182-195	1	13 T	50 50	) 
,	14	1 14	905	1	12610-12623	;	196-209	T t	15	50 50	Į į
!	15	15	906	1	12624-12637	1	210-223	1	16 1	50 50	1
'	16	1.16	907 -	1	12636=12651	i	224+237	!	17	50 50	1
ï	17	17 1	908	ì	12652-12665	i	238+251	ľ	18 1	50 50	ì
i	18	181	909	i	12666-12679	i	1 = 14	í	1 1	51	i
	15	19	910	i	12630-12693	į	15= 28	i	i s	51	i
i	50	1 05	911	i	12694-12707	i	29= 42	i	3 1	51	i
į	21	21	912	i	12708-12721	i	43- 56	i	4 1	51	ĺ
j	22	1 22	913	i	12722-12735	İ	57+ 70	Ĺ	5 1	51	j
ł	23	ا 3 ا	914	1	12730-12749	1	71 + 84	1	6 1	51	1
ļ	24	1 24 1	915	١	12750-12763	1	85+ 98	1	7 1	51	ļ
1	- 25	25	-916	1.	12764-12776	ŧ	99-111	ł	8 1	- 51	j
ł	26	ا 65 ا	917	1	12777-12790	1	112-125	1	9 1	51	1
ı	27	27 1	918	ŀ	12791-12804	ł	126-139	-	10 1	51	1
1	26	1 83	919	1	12805-12×18	1	140-153	-	11	51	t
ł	29	29	920	1	12819=12432	i	154-167	ŀ	12 1	51	ł
- 1	30	30	921	1	12833-12346	ŀ	168+181	-	13	51	1
1	31	31 -1	922	1	12847-12460	•	182-195	ł	14 1	51	1

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,	DATE I		FI IGHT DAY	T I	SPACEC		REFERENCE 9RBITS		REF 1 DAY I	CYCLE I	
	1 1	35	923	1	12861-1	2874 1	196-209		15	51 1	
	1 2 1	33	924	ı	12875-1	2488 1	210-223	. [	16 1	51 I	
	1 3 1	34	925	1	12889-1	1 SCFS	224-237	1	17	51	
	4	35	926	1	12903-1	2916	238-251	i	18 1	51 l	
•	1 · 5	36	927	1	12917-1	2930 1	1= 14	- [	1 1	52 I	
	6	37	928	1	12931-1	2944	15= 28	-	2 1	52 I	
	l ~ 7~~1	38-	929	1 "	12945~1	•	29= 42	-	3 1	52	
	&	39	930	1	12959-1	2972   1	<b>43=</b> 56	T.	4 1	52 I	
	9 1	40 1	931	İ	12973-1		57- 70	1	5 1	52 I	
	l 10 l	41	932	1	12987-1		71= 84	-	6 I	52 I	
i	11	42	933	i	13001-1		85+ 98	-	7 1	52	
	12	43	934	j	13015-1		99=111	l	8 I	52	
	1 13 1	4# 1	935	ļ	13028-1	3041	112-125	1	9 1	52	
	14 1	45 1	936	ł	13042-1	3055 I	126-139	ł	10 1	52 I	
1	15	46	937	1	13056-1		140•153	1	11	52 1	
	16 1	47 1	938 ~	ŀ	13070-1		154-167	1	12	52	
(	17-1	48	939	1	13054=1	3097 🗼	168-181	1	13 1	52 I	
-	18 I	49	940	1	13098-1	3111 H	182+195	1	14 1	52 1	
. {	<b>1</b> 9	50	941	1	13112-1		196 <b>-</b> 209	1	15	52	
- 1	50	51	942	l	13126-1	3139	210-223	-	16 1	52 I	
(	21	52	943	ļ .	13140-1	3153	224-237	t	17 I	· 52 +	
- [	22	53	944	ŀ	13154-1	3167	238-251	ŀ	18	52 I	
1	23	5# 1	945	ļ	13168-1		1- 14	1	1 1	53	
1	24	55 I	946		13182-1	3195 I	15• 28	-	5	5 <b>3</b> )	
- 1	25 - 1	56	947	į	13196-1	3209	29- 42	f	3	53 I	
ļ	26	57 1	948		13210-1	3253 1	<b>43-</b> 56	t	4 I	53 )	
١	27	-58 I	949		13224-1		5 <b>7- 70</b>	1	5 I	53	
Į	28 1	59 1	950	l	13235-1	3251 l	71= 84	1	<b>6</b> 1	5 <b>3</b>	

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		GMT	I FI IGHT	I SPACECPAFT	I REFERENCE I	REF	CYCLE I
	DATE	DAY		6RBITS	BRBITS	DAY	NO •
	tt t	- 60	1951	13252-13265	h85≠ 198 li	7 1	53 1
	1 2 1	61	1 952	13266-13278	99-111	์ ลิ่	53 i
-	1 . 3 1	. 62 -	953	1 13279-13292	1 112-125	9	53 i
	1 4 1	63	1 954	13293+13306	1 126-139	10 i	53 i
	<b>5</b>	- 64	955	13307-13320	1+0-153	11 i	53 i
	6	65	956	13321-13334	1 154-167	12	53 I
	) 7+-	66	957	13335=13348	1-158-181	13 1	53
	8 1	67	958	13349+13362	132 <b>-</b> 195	14	53 (
	9 1	- 68	1 559	13363-13376	196-209	15	53 I
ĺ	10	69	960	13377-13390	1 210-223 1	16	53 I
.	11	70	1 - 961	13391-13404	1 224-237	17	53 I
ĺ	12	71	962	13405-13418	238-251	18	53 !
	├ 1:3···→	72	I963	13419=13432	! ••• <b>1</b>	1 1	54
1	14 (	73	964	13433-13446	15= 28	2 1	54 1
	15 -	- 7 <u>4</u>	965	13447=13460	29- 42	3	54
Ì	1 16 1	75	966	13461-13474	43 <del>-</del> 56	4 1	54
	17	76		13475 <b>-</b> 13486	l ~ 57 <b>~</b> 70   l	· 5 I	54
ļ	18	77	968	13489-13502	71-84	6 1	54
	19	7&-	969	13503=13516	) - £5≠ 98	- 7 I	54
j	50	79	970 1	13517-13529	99 <b>-</b> 111	8	54
- †	21	. 80	971	13530+13643	112-125 +	9 1	54 I
ļ	<b>25</b>	81	972	. 13544-13557 (	126 <b>-1</b> 39	10 1	54
.	23 -+	62	!···· 973 !	13552-13571	140-153	11	54
ļ	24	83	974	13572-13585	154 <b>-</b> 167	12	54
	25	84	1975	13586=13599	F 168+181 I	13	54
ļ	26	5ه	976 1	13600-13613 (	182 <b>-</b> 195 (	14	54
1	27 4	86	977	1361+-13627 (	196-209	15	54 (
ļ	28	87	978	13628-13641	210-223 I	16 +	54
}	59	88	979	13642-13455	224-237	17	54 I
!	30 I	89	980	13650-13669	238-251 (	18 (	54
. 1	·· 31	90	981	13679=13583	1- 14	1 1	55 I
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GMT   FF1GHT   SPACECRAFT   REFERENCE   REF   CYCLE   DATE   DAY   DAY   ORBITS   ORBITS   DAY   NO.	٠.										
DATE   DAY   DAY   0RBITS   0RBITS   DAY   N0.	1	-	-GM-T	· FI IGHT	- 1-	SPACECHAFT		REFERENCE	- I-	REF I	CYCLE
2	-1	_			ĺ		i		ĺ		
2											
3	- [	1		982	1	13684=13697	ŧ	15 <b>=</b> 28	ļ	5 1	55 · +
4	j	2			1		į	29- 42	- 1	3 1	
5	1	3 1	• -		- 1		ı	43= 56	1	4 1	-
6		4		·	ı		1	57 <b>→</b> 70	1	5 1	
7	1	5			4	13740-13753	-	71 = 84	1	6 1	55 I
8	١	6	. –	l 987	1	13754-13767	1	85* 98	- 1	7 1	55 I
9	- 1				1		ľ	99-111	1	8 1	
10	ı						ļ	112-125	1		
11	-		-	•	1		į		.1	10 (	
12	-				1		ł		- 1	11	
13	ţ				1		ŧ		1		
14	1			-	İ	- · · · · · · · · · · · · · · · · · · ·	ł	- ·· <del>-</del>	1		
15			-		†		1		ı	14	
16	ı				l		-		1	<b>1</b> 5 I	-
17	- 1	15		<b>-</b> .	1 -	<b>- -</b>	1	210+223	ı	16 I	
16	- 1				1		1		- 1		
19	· t				1		ŧ	· · - · •	ł		
20	ı	-					1		1		
21	- j			· · · · · <del>-</del>			i		ŧ		
22   112   1003   13977-13990   57+70   5   56   23   113   1004   13991-14004   71-64   6   56   24   114   1005   14005-14018   85-98   7   56   25   115   1006   14019-14031   99-111   8   56   26   116   1007   14032-14045   112-125   9   56   27   117   1008   14046-14059   126+139   10   56   28   118   1009   14060-14073   140-153   11   56   29   119   1010   14074-14087   154-167   12   56	- 1				1		l	<del>-</del>	1	3 1	,
23   113   4004   13991-14004   71=84   6   56   24   114   4005   14005-14018   85=98   7   56   25   115   4006   14019-14031   99=111   8   56   26   116   4007   14032-14045   112=125   9   56   27   117   4008   14045-14059   126=139   10   56   28   118   4009   14060-14073   140=153   11   56   29   119   4010   14074-14087   154=167   12   56	1				j		t		1		
24	- 1				1		ł		-	•	
25   115   1006   14019=14031   99=111   8   56   26   116   1007   14032=14045   112=125   9   56   27   117   1008   14046=14059   126=139   10   56   28   118   1009   14060=14073   140=153   11   56   29   119   1010   14074=14087   154=167   12   56	1				!		-1		ı		-
26   116   1007   14032-14045   112-125   9   56   27   117   1008   14046-14059   126+139   10   56   28   118   1009   14060-14073   140-153   11   56   29   119   1010   14074-14087   154-167   12   56	ļ				!		1		-		
27   117   4008   14046-14059   126+139   10   56   26   118   4009   14060-14073   140-153   11   56   129   119   4010   14074-14087   154-167   12   56				· <del>-</del>	1		1		1		
28   118   1009   14060-14073   140-153   11   56   129   119   1010   14074-14087   154-167   12   56	•	- '			!	· ·	1		- 1		
1 29   119   1010   14074-14087   154-167   12   56					l	***	ţ		į		
	•				!		1		1	•	
1 30   120   1011   14088-14101   168-181   13   56	ļ			-	1		!	. – – – .	I		
	- 1	30 I	120 !	1011	 	14088-14101	1	168=181	-	13 !	56 l

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ł		ŧ		1	FI IGHT	1	SPACECHAFT	1	REFERENCE	1	REF I	CYCLE	7
	DATE	1	DAY	ı	DAY	ı	ORBITS	١	GREITS	i	DAY	N6 •	i
- 1	1	1	121	1	1012	. <del></del> .	14102-14115	·	182-195			*******	
i	ž	i	122	i	1013	i	14116-14129	- }	196-209	1	14	56	ţ
i	3	i	123	i	1014	i.	14130-14143	1	210-223	1	15	56	!
i i	4	i	12#	i	1015	-	14144-14157	1	224-237	1	16	56	. !
i	5	i	125	i	1016	i	14158-14171	-	238-251	!	17	56	!
i	6	i	126	ì	1017	i	14172-14185	!	<b></b>	!	18	5 <del>6</del>	1
i	7	ì	-127		1018	1	14186=14199		1= 14	!	1 1	57	- [
i	á	ì	128	1	1019	!		!	15- 28	1	5 1	57	- 1
ï	9	i	129	i	1020	!	14200=14213	!	29+ 42	1	3 1	57	ı
i	10	i	130	ï	1020	; 1	14214=14227	f	<b>43-</b> 56	1	4 1	57	ł
- ¦	11		131	'		1	14228-14241	1	57 <b>-</b> 70	1	5 1	57	t
1	12	F	132	Ţ	1022	!	14242-14255	1	71 - 84	1	6 1	57	1
I i	- ::	1		1	1023	1	14256-14269	į	85= 98	F	7 1	57	1
- !	14	+	133	!	1024	!	14270-14282	1	99-111	t	8 1	57	ł
- !	_	!	134	ļ	1025	!	14283=14296	1	112-125	ł	9 1	57	1
-!	15	ļ	135	!	1026	1	14297-14310	1	126-139	1	10 1	57	ł
	16	i	136	İ	1027	ı	14311-14324	ı	140=153	F	11	57	1
!	17	!	137	!	1028	İ	14325-14338	ı	154=167	1	12 (	57	ì
!	18	ļ	138	!	1029	1	14339-14352	1	168=181	1	13	57	1
. !	19	ŧ	139	1	1030	ı	14353-14366	1	182-195	ļ	14	57	į
	50	į	140	1	1031	ì	14367-14380	1	196-209	1	15	57	1
ı	21	í	141	1	1032	į	14381-14394	1	210-223	1	16 i	57	Ĺ
1	55	ļ	142	1	1033	i	14395=14408		224-237	i	17 i	57	i
!	23	ļ	143	1	1034	ŀ	14409-14422	1	238-251	İ	18	57	i
1	24	I	144	ļ	1035	į	14423-14436	1	1 = 14	ł	1 1	58	ì
•	25	1	145	1	-1056	1	14437-14450	F	15- 28	ı	2 1	58	i
ł	26	ł	146	1	1037	ì	14451=14464	1	29- 42	1	3 1	58	i
ļ	27	1	147	F	1038	İ	14465=14478	ļ	43- 56	í	4 !	58	í
ı	28	1	148	1	1039	1	14479-14492	1	57- 70	ļ	5 1	58	ĺ
1	29	-	149	)	1040	i	14493-14506	ŧ	71= 84	ĺ	6 i	58	i
1	30		150	t	1041		14507-14520	ł	85- 98	, 	7 1	58	i
ı	31	ŧ	151	ı	1042		14521=14533	1	99-111	ŀ	έİ	58	i
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7	TMS !		SPACECRAFT I	- RESERENCE	l REC I	CYCLE
i	DATE - DAY		_	-		
T	DATE TO DATE		9-1-1-3	·6-NO-1-1-0-	p: -1249-7-	
<sub>.</sub>	1-1 152	1 1043	14534-14547	112-125	1 7 9 1	58 1
ï	2   153	1 1044	14548=14561	126-139	10 i	58 i
i	3   154	1 1045 1	14562-14575	140-153	111	58
i	4   155	1 1046 1	14576-14689	154-167	12 1	58 I
i	5   156	1 1047 L	14590+14603	168-181	13 1	58 1
i	6   157	1 1048 L	14604-14617	182-195	14	58 1
i	7-1 158	1049	14618=14631	196-209	15	58
i	8   159	1 1050 1	14632=14645	210-223	1 16 1	58 (
i	9   160	1051	14646#14659 1	224-237	1 17 1	58 1
i	10   161	1 1052 1	14660=14673 1	238*251	18	58 I
1	11   162	1 1053 I	14674-14687	1 - 14	f. 1 i	59 I
İ	12   163	1 1054.	14688=14701	15- 28	1 2 1	59 I
ł	13   164	1 1055 1	14702-14715	29- 42	3 1	· 59 I
. 1	14   165	1 1056 I	14716-14729	43= 56	1 4 L	59 I
1	15 1-166	1 1057 1	14730-14743	57 <b>-</b> 70	1 5 1	59 I
- 1	16   167	1 1058 - 1	14744-14757	71- 84	1 6 1	59 I
-	17   168	1 - 1059 - 1	14756-14771	85 <b>+</b> 98	1 7 1	59 I
-1	18   169	1 1060 - 1	14772-14784 1	99-111	8 1	59 I
H	19   170	1 1061	14785-14796 I	112-125	! <del>9</del>	59 I
-1	20   171	1 1062 I	14799-14812	126-139	1 <b>1</b> 0 I	59 I
-1	21   172	1063	14813-14826	140-153	i <b>1</b> 1 i	59
ı	22   173	1004	14827-14340	154=167	12	59
İ	23   174	1 +065 1	14841-14354	168*181	13 H	59 I
- 1	24   175	l 1066 l	14855-14868	182-195	14	<b>59</b> 1
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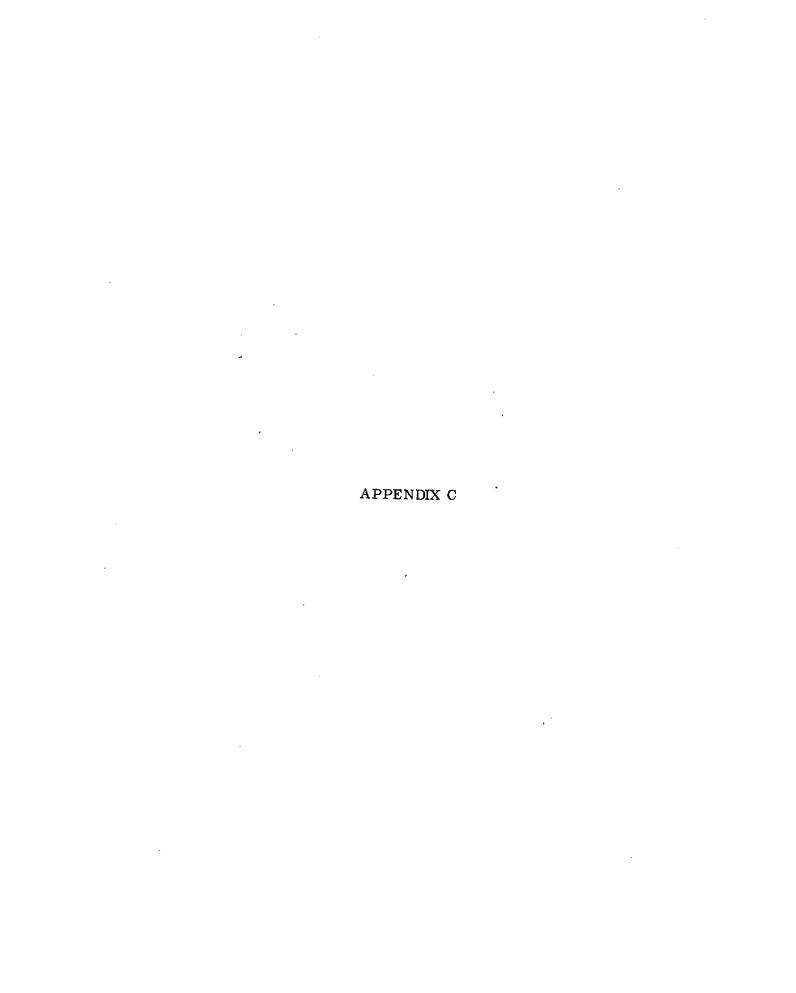
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Introduction

Although the USB has declined in power repeatedly since launch (see Reference 1), until recently there was no observable decrease in its ability to perform its functions. A sensitive technique for detecting incipient operational deterioration is described in Reference 2, using the USB/DCP link from Iceland. Reference 2 showed no deterioration at that time, even though the USB power had declined since launch from 1.6 watts (telemetryindicated) to 0.264 watts, a decline of 7.8 db.

# Objective of this Study

Since issuance of Reference 2, the USB power output has continued to decline, reaching 0.192 watts in Orbit 8424 on 19 March 1974.

This study is to determine whether the USB performance has shown deterioration at this lower power output level.

## Summary

Incipient deterioration of USB/DCS relay is evident. Prior to Orbit 8420 on 19 March 1974, the demonstrated range of USB relay of DCS messages was 2157 statute miles (3471 kilometers), essentially the optical horizon of the ERTS spacecraft. After Orbit 8424, the demonstrated range was 1900 statute miles (3060 kilometers), 88% of the original range and 78% of the original area coverage of the USB.

When the power output dropped below a telemetry-indicated value of 0.25 watts, coverage begins to shrink from the ERTS-horizon. This loss of USB coverage was detected by a sensitive technique, even though there is no observable effects as yet, on any of the USB functions: telemetry transmissions, ranging, and DCS operations all seem normal. The "cushion" in the signal-to-noise ratio of these links conceal the incipient deterioration.

### Recommendations

Switchover to the redundant B-section of the USB subsystem is recommended for the near future. Unused heretofore, the B-section is available, with a transmitter power output expected to be about 1.3 watts.

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### Discussion

Figure 0 shows the history of the USB power output since January 1, 1974. Five 18-day periods are shown as Zones 1 to 5 for later analysis. The USB power has dropped over 2 db from a power output level shown to be adequate in Reference 2. To analyze the effects of this power decline, using the technique of Reference 2 a computer program was prepared by J. Williamson of NASA, to plot the location of the ERTS Satellite at time of reception of messages from a remote DCP (6315) in Iceland. Superimposed on the printout are the horizons of the DCP and of the Greenbelt ground station ENT. Figures 1 thru 36 display this data. The first 18 figures display the data span in Zone 1 on Figure 0 from Orbit 7339 on 1 January thru Orbit 7598 on 19 January 1974, when the USB power output was 0.26 watts. The other 18 figures display the data span in Zone 5 from Orbit 8748 on 12 April thru Orbit 8993 on 29 April 1974, when the USB power output was 0.19 watts.

At the top of each of these printouts, data are shown for each message received for that day. The columns show: time of message reception; interval between messages; geographic location of ERTS; orbit number; slant range (statute miles); azimuth and elevation from Greenbelt; slant range (st. mi.) of ERTS horizon; "reference" orbit in the 18-day cycle; time and longitude of descending node; and a letter-identifier for all messages in each orbit.

The plot is bordered by identifications of latitude and longitude. The dots represent Goldstone ground station location and coverage. For purposes of this study they may be ignored. The crosses represent Greenbelt location and coverages. The area of interest is the upper right hand side, where the Greenbelt coverage "circle" intersects the coverage circle of DCP-6315 (Iceland) shown with asterisks. The letters between these intersecting coverage circles geographically locate message receptions. If all similar letters are connected, the sub-satellite paths will be traced. These paths are NE to SW in the day time, and SE to NW at night. Of particular in interest for this study is determination of whether the extreme letter on the side of the Greenbelt horizon (crosses) is close enough to the horizon to preclude room enough for another letter, after projecting the spacing, adjusted for latitude. The geographic location of message receptions are a dual function of ERTS location (i.e. reference orbit), and time of DCP transmission, which for DCP-6315 consists of 38 millisecond bursts of dat space 84 seconds apart. Statistical treatment is therefore necessary to derive extreme range.

Tables 1 thru 5 were prepared corresponding to Zones 1 thru 5 in Figure 0.

A comparison of the ranges demonstrated in the first and last tables (1 and 5) is shown in Figure 37. The solid line shows the ranges and elevation angles at which DCP messages were received when the USB power was 0.19 watts. The crosses at the lower end of this curve shows the additional ranges that were achieved when the power output was 0.26 watts.

Figure 38 shows the range at which the extreme (most remote from ENT) message was received for each of the 5 zones in Figure 0. Comparing Zone 1 to Zone 2, it can be seen that the drop from 0.260 to 0.255 watts caused no significant range-shift of the ext eme messages. In Zone 3 as the power continued to drop, the range-shift becomes significantly reduced. It can be seen that after the power dropped to 0.192 watts (Zones 4 and 5) there was a large range-shift to shorter distances.

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FIGURE 2 DOTATION OF BEST MESSAGE MASSETTIONS JACKET 2, 1974

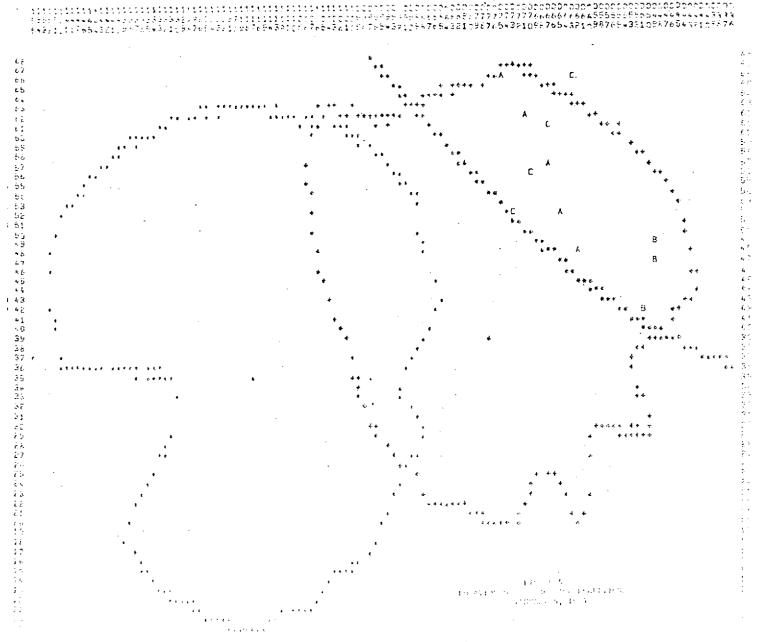
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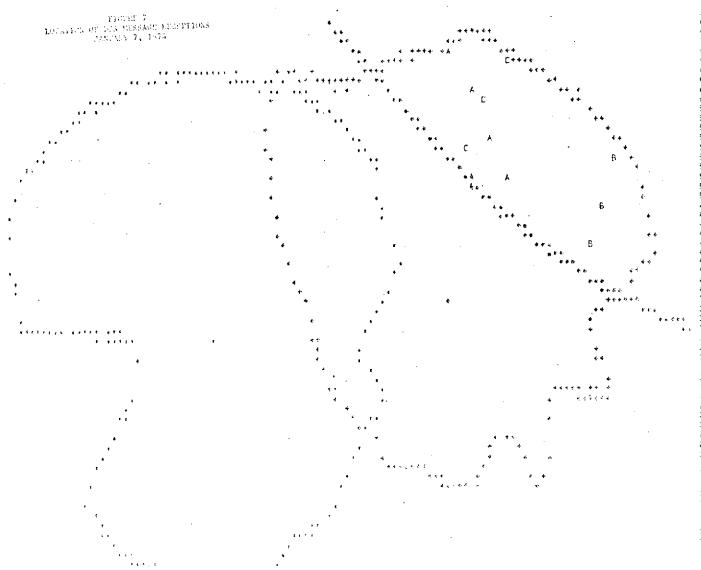
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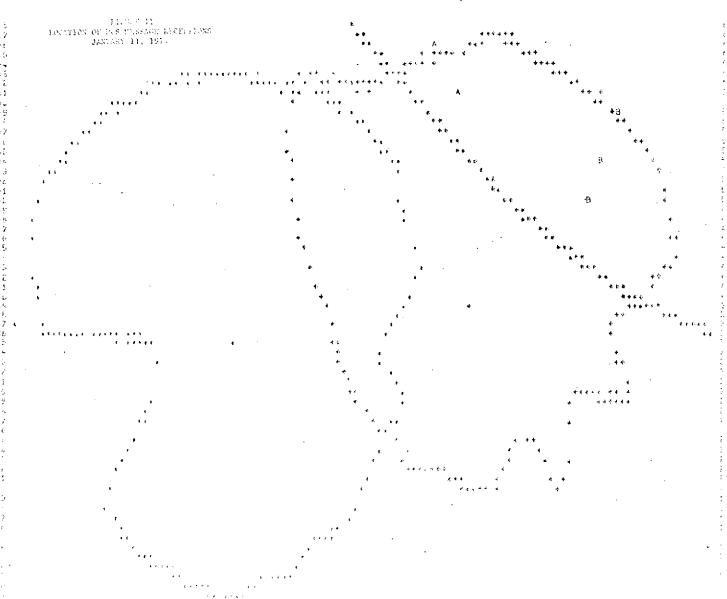
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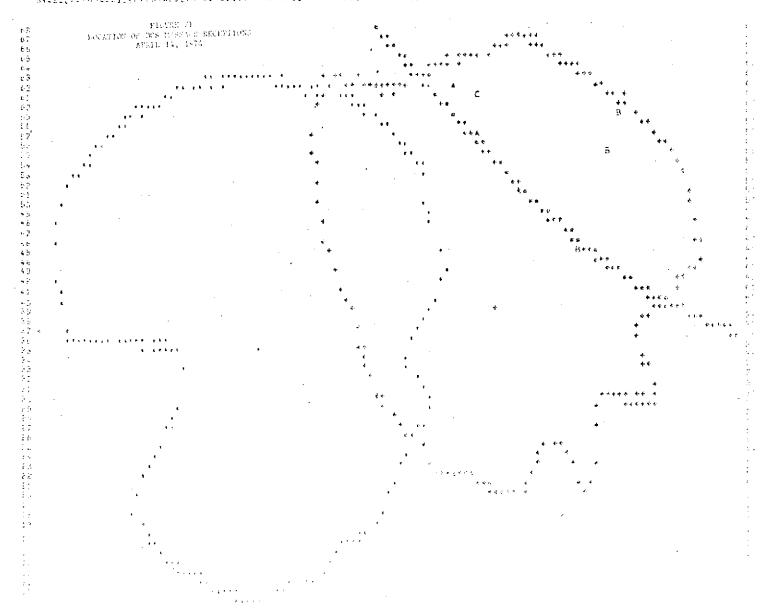
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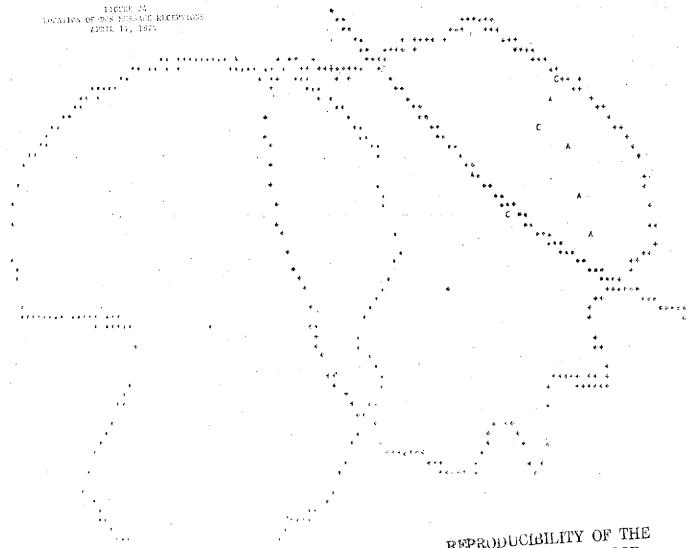
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FIGURE 32 LOUVELON OF FUR MUSICAL AMERICAN APRIL 19, 1810

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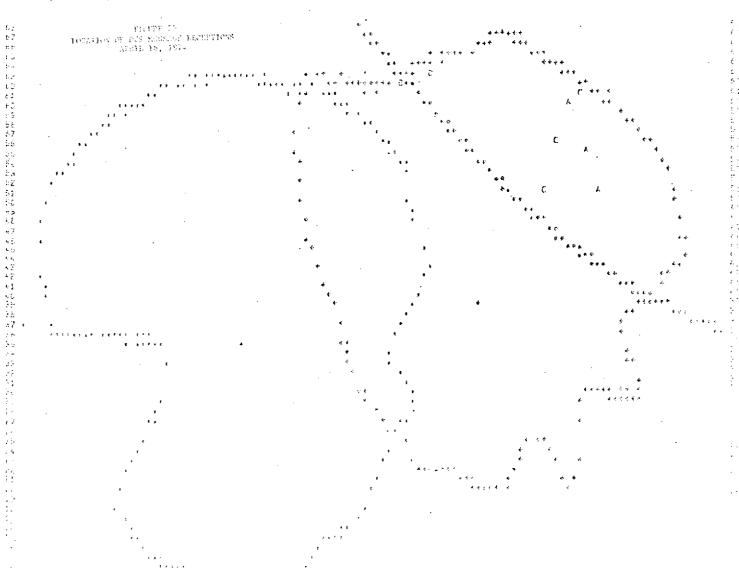
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te teva II		¢. • 7 e	eges <sup>1</sup> ,2	- e u 3	,	16024	\$195×*	6.3	40 El 40 Mg	3 4 3	105 1846 33	+127+09	n

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		, r	ू भागी के इंक्टरकार	: ; ;	F. T.	150 4 2	eléteck (*1)	1 1 4	4217014 44-51	14.1 14.5 TT	COLUMNAN PR	1916 F65* (6×3
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Hannar B	•	12814	*****	· -::::		18020	2191.4	11+1	\$6.0	232	111-1519 25	<b>+85+5</b> 8	5

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FIGURE 25 LOCATION OF RES MESSAGE BECERFIORS APAIL 21, 1974

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TABLE 1

UBS PERFORMANCE
at 0.260 watts
using DCP 6315 in Iceland

				ENT	<u> </u>		
				Last M	sg		
			Misses	Rec	<u> </u>	Num.	
			at	Range	Elev.	of	
Day	Hour	Orbit	Horizon	St. Mi.	Deg.	Msgs	Comments
001	. 00	7339	. 0	2125	1.0	5	
<b>003</b>	02	7340	Ö	1928	4.1	1	
	14	7347	Ö	1800	6.4	2	
	16	7348	Ö	1991	3.1	1	
002	00	7353	Ö	2084	1.6	4	
002	14	7361	Ö	1800	6.4	3	
003	00	7367	Ö ,	2157	0.6	4	
003	15	7375	Ö	1899	4.6	3	
004	01	7381	Ŏ	1919	4.3	2	Masking
004	13	7388	Ö	1929	4.1	3	
	15	7389	Ŏ	1800	6.4	ī	
005	01	7395	0 -	2070	1.9	5	Masking
	13	7402	i	1751	7.3	3	
	15	7403	Ō	2113	1.2	4	
006	01	7409	Ō	2130	1.0	5	Masking
	13	7416	0	1977	3.3	· 3	•
	15	7417	0	2061	2.0	4	
	17	7418	0	2102	1.4	1	
007	01	7423	Ö	2016	2.7	4	Masking
	13	7430	Ō	1872	5.1	3	
	15	7431	0	1991	3.1	3	
800	01	7437	Ō	1991	3.1	3 5	Masking
	13	7444	0	1860	5.3	3	
	15	7445	0	1939	4.0	3	
009	01	7451	0	1898	4.6	3 3	Masking
	13	7458	Ō	1922	4.3	3	
	15	7459	Ō	2112	1.2	3	
010	01	7465	0	2079	1.7	3 2	Masking
	14	7472	0	1780	6.7	3	•
	15	7473	Ō	1960	3.6	1	
011	01	7479	0	2066	1.9	3	Masking
<del>-</del>	14	7486	Ō	1958	3.7	3	~
012	01	ر 749	Ö	1999	3.0	4	Maskir g
	14	7500	Ŏ	1842	5.6	2	<u>.</u>
	15	7501	Ö	2092	1.5	3	
	* 3	1.001	U	2032	4	•	

TABLE 1

		,	-	ent			
				Last M		<b></b>	
•			Misses	Rec		Num.	
Day	Hour	Orbit	at Horizon	Range St. Mi.	Elev. Deg.	of Msgs	Comments
Day	nour	OLDIA	1101 12011	St. Ht.	DEK.	11943	Commence
013	01	7507	0	2016	2.7	3	Masking
	14	7514	0	1889	4.8	3	•
	16	7515	0	1902	4.6	2	
(Day	14 omitt	ed: no d	ata)				
015	00	7534	0	1969	3.5	. 5	
_	02	7535	0	1844	5.6	2	Masking
	14	7542	0	1801	6.4	1	
	16	7543	. 0	1872	5.1	1	
016	00	7548	0	2019	2.7	4	
	14	7556	0 ´	1952	3.7	2	
	16	7557	0	2047	2.2	2	Masking
017	00	7562	0	2123	1.1	6	_
	02	7563	0	1821	6.0	1	Masking
	14	7570	0	1862	5.3	1 2 2 5	
	16	7571	0	2029	2.5	2	Masking
018	00	7576	0	2000	3.0	5	
	02	7577	0	1984	3.2	1	Masking
	14	7584	0	1893	4.7	2 2	•
	16	<b>758</b> 5	0	2085	1.6		Masking
019	00	7590	0	1962	3.6	5 1	
	02	7591	0	1984	3.2	_	Masking
	14	7598	0	1904	4.6	_3_	

Total Msgs Received in 18 day: 160

TABLE 2

196	Ref. Orb.	<u>Day</u>	<u> Hour</u>	<u>Orbit</u>	Misses	Range	Elev. <u>Angle</u>	No. of Msg.
205         16         7850         0         2017         2.7         1           210         038         00         7855         0         1750         7.3         3           219         16         7864         0         1913         4.4         1           224         039         00         7869         0         1935         4.0         3           232         15         7877         0         1869         5.2         2           233         16         7878         0         1864         5.2         1           245         13         7890         0         1853         5.4         1           246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1966         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2	196	037	00	7841		1851	5.5	2
210	204			7849	0	1992	3.1	4
218         14         7863         0         1750         7,3         3           219         16         7864         0         1913         4.4         1           224         039         00         7869         0         1935         4.0         3           232         15         7877         0         1869         5.2         2           233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1964         3.5         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2	205		16	7850	0	2017	2.7	1
218         14         7863         0         1750         7,3         3           219         16         7864         0         1913         4.4         1           224         039         00         7869         0         1935         4.0         3           232         15         7877         0         1869         5.2         2           233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1964         3.5         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2	210	038	00	7855	0	1751	7.3	
224         039         00         7869         0         1935         4.0         3           232         15         7877         0         1869         5.2         2           233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7905         0         1961         3.6         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.7         3           23         15         7919         0         1897         4.7         3           23         15         7919         0         1897         4.7         3	218		14	7863	0	1750	7.3	
232         15         7877         0         1864         5.2         2           233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1896         3.0         4           8         13         7904         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         4.7         3         3           23         15         7919         0         1957         3.7         2           29         043         01         7925         0         2068         1.9         4	219		16	7864	0	1913	4.4	1
232         15         7877         0         1869         5.2         2           233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1895         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         7905         0         1961         3.6         2           15         7911         1         1719         7.9         2           22         13         7918         0         1897         4.7         3           23         15         7919         0         1957         3.7         2           29         043         01         7933	224	039	00	7869	0	1935	4.0	3
233         16         7878         0         1864         5.2         1           238         040         01         7883         0         2056         2.1         4           245         13         7890         0         1853         5.4         1           246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         4.7         3         2           29         043         01         7925         0         2068         1.9         4           37         15         7919         0         1957         3.7         2           29         043         01         7933         0         1875         5.0	232		15	7877	0	1869	5.2	2
245         13         7890         0         1853         5.4         1           246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         7905         0         1961         3.6         2           15         7911         1         1719         7.9         2           22         13         7918         0         1857         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7919         0         1957         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01	233		16	7878	0	1864	5.2	1
246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         4.7         3           23         15         7919         0         1957         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2         2           51         15         7647         0         1928         4.2         2         <	238	040	01	7883	0	2056	2.1	4
246         15         7891         0         1825         5.9         2           1         041         01         7897         0         1996         3.0         4           8         13         7904         0         1964         3.5         2           9         15         7905         0         1961         3.6         2           15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         4.7         3         23         15         7919         0         1957         3.7         2         29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3         4         3         044         01         7939         0         1961         3.6         4         2         1         5         6         4         13         7960         1889         4.8         2         2         5         7         045         01         7953         0         1824         4.2 <t< td=""><td>245</td><td></td><td>13</td><td>7890</td><td>0</td><td>1853</td><td>5.4</td><td>1</td></t<>	245		13	7890	0	1853	5.4	1
1       041       01       7897       0       1996       3.0       4         8       13       77904       0       1964       3.5       2         9       15       7905       0       1961       3.6       2         15       042       01       7911       1       1719       7.9       2         22       13       7918       0       1897       4.7       3       3         23       15       7919       0       1957       3.7       2         29       043       01       7925       0       2068       1.9       4         37       15       7933       0       1875       5.0       3         43       044       01       7939       0       1961       3.6       4         50       13       7646       0       1890       4.8       2       2         51       15       7647       0       1928       4.2       2       2       5       1       15       7647       0       1928       4.2       2       2       5       7       045       01       7953       0       1829	246		15	7891	0	1825	5 <b>.</b> 9	2
8       13       7904       0       1964       3.5       2         9       15       7905       0       1961       3.6       2         15       042       01       7911       1       1719       7.9       2         22       13       7918       0       1897       4.7       3       3         23       15       7919       0       1957       3.7       2       2         29       043       01       7925       0       2068       1.9       4         37       15       7933       0       1875       5.0       3         43       044       01       7939       0       1961       3.6       4         50       13       7646       0       1890       4.8       2       2         51       15       7647       0       1928       4.2       2       2         57       045       01       7953       0       1834       5.8       2         64       13       7960       0       1829       5.8       3         65       15       7961       0       2116       1.2<	1	041	01	<b>78</b> 97	0	1996	3.0	
15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3     <	8		13	7904	0	1964	3.5	2
15         042         01         7911         1         1719         7.9         2           22         13         7918         0         1897         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3     <	9		15	7905	0	1961		2
22       13       7918       0       1897       4.7       3         23       15       7919       0       1957       3.7       2         29       043       01       7925       0       2068       1.9       4         37       15       7933       0       1875       5.0       3         43       044       01       7939       0       1961       3.6       4         50       13       7646       0       1890       4.8       2         51       15       7647       0       1928       4.2       2         57       045       01       7953       0       1834       5.8       2         64       13       7960       0       1829       5.8       3         65       15       7961       0       2116       1.2       3         71       046       01       7967       0       1924       4.2       2         78       14       7974       0       1963       3.6       3         79       15       7975       0       1933       4.1       2         85       <	15	042	01	7911	1	1719		2
23         15         7919         0         1957         3.7         2           29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1829         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3     <	22	٠	13	7918	0		4.7	3
29         043         01         7925         0         2068         1.9         4           37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3     <	23		15	7919	0			2
37         15         7933         0         1875         5.0         3           43         044         01         7939         0         1961         3.6         4           50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3           92         14         7988         0         1753         7.2         3	29	043	01	7925	0			
43       044       01       7939       0       1961       3.6       4         50       13       7646       0       1890       4.8       2         51       15       7647       0       1928       4.2       2         57       045       01       7953       0       1834       5.8       2         64       13       7960       0       1829       5.8       3         65       15       7961       0       2116       1.2       3         71       046       01       7967       0       1924       4.2       2         78       14       7974       0       1963       3.6       3         79       15       7975       0       1933       4.1       2         85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3	37		15	7933	0			
50         13         7646         0         1890         4.8         2           51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3           92         14         7988         0         1753         7.2         3           93         048         01         7995         0         2007         2.9         3           106         14         8002         0         1917         4.3         3	43	044	01					
51         15         7647         0         1928         4.2         2           57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3           92         14         7988         0         1753         7.2         3           93         048         01         7995         0         2007         2.9         3           106         14         8002         0         1917         4.3         3           107         15         8003         0         2088         1.6         3	50		13	7646				
57         045         01         7953         0         1834         5.8         2           64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3           92         14         7988         0         1753         7.2         3           93         048         01         7995         0         2007         2.9         3           106         14         8002         0         1917         4.3         3           107         15         8003         0         2088         1.6         3           113         049         01         8009         0         1877         5.0         3	51		15	7647	0			
64         13         7960         0         1829         5.8         3           65         15         7961         0         2116         1.2         3           71         046         01         7967         0         1924         4.2         2           78         14         7974         0         1963         3.6         3           79         15         7975         0         1933         4.1         2           85         047         01         7981         0         1847         5.5         3           92         14         7988         0         1753         7.2         3           93         048         01         7995         0         2007         2.9         3           99         048         01         7995         0         2007         2.9         3           106         14         8002         0         1917         4.3         3           107         15         8003         0         2088         1.6         3           113         049         01         8009         0         1877         5.0         3	57	045	01	<b>795</b> 3	0			2
65       15       7961       0       2116       1.2       3         71       046       01       7967       0       1924       4.2       2         78       14       7974       0       1963       3.6       3         79       15       7975       0       1933       4.1       2         85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1	64		13	7960	0			
71       046       01       7967       0       1924       4.2       2         78       14       7974       0       1963       3.6       3         79       15       7975       0       1933       4.1       2         85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1	65		15	7961	· <b>0</b>			
78       14       7974       0       1963       3.6       3         79       15       7975       0       1933       4.1       2         85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8099       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3 <tr< td=""><td>71</td><td>046</td><td>01</td><td>7967</td><td>0</td><td>1924</td><td>4.2</td><td>2</td></tr<>	71	046	01	7967	0	1924	4.2	2
79       15       7975       0       1933       4.1       2         85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3 <t< td=""><td>78</td><td></td><td>14</td><td>7974</td><td>0</td><td>1963</td><td>3.6</td><td></td></t<>	78		14	7974	0	1963	3.6	
85       047       01       7981       0       1847       5.5       3         92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5 </td <td>79</td> <td></td> <td>15</td> <td>7975</td> <td>0</td> <td>1933</td> <td>4.1</td> <td></td>	79		15	7975	0	1933	4.1	
92       14       7988       0       1753       7.2       3         93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2	85	047	01	7981	0			
93       048       01       7995       0       2007       2.9       3         99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4	92		14	7988	0			3
99       048       01       7995       0       2007       2.9       3         106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	93	048	01	7 <b>9</b> 95	0			
106       14       8002       0       1917       4.3       3         107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	99	048	01	7995	0			
107       15       8003       0       2088       1.6       3         113       049       01       8009       0       1877       5.0       3         120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	106		14	8002	0	1917		3
120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	107		15	8003				3
120       14       8016       0       1595       10.4       1         121       15       8017       0       2187       0.1       2         127       050       02       8023       0       1753       7.2       1         134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	113	049	01	8009	0			3
121     15     8017     0     2187     0.1     2       127     050     02     8023     0     1753     7.2     1       134     14     8030     0     2129     1.0     3       135     16     8031     0     1673     8.8     3       140     051     00     8036     0     1991     3.1     5       141     02     8037     0     1843     5.6     2       148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	120		14	8016	0			1
127     050     02     8023     0     1753     7.2     1       134     14     8030     0     2129     1.0     3       135     16     8031     0     1673     8.8     3       140     051     00     8036     0     1991     3.1     5       141     02     8037     0     1843     5.6     2       148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	121		15	8017	0			
134       14       8030       0       2129       1.0       3         135       16       8031       0       1673       8.8       3         140       051       00       8036       0       1991       3.1       5         141       02       8037       0       1843       5.6       2         148       14       8044       0       1964       3.5       4         149       16       8045       0       2027       2.5       2         154       052       00       8050       0       2154       0.6       6	127	050	02	8023	0			
135     16     8031     0     1673     8.8     3       140     051     00     8036     0     1991     3.1     5       141     02     8037     0     1843     5.6     2       148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	134		14					
140     051     00     8036     0     1991     3.1     5       141     02     8037     0     1843     5.6     2       148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	135		16	8031				
141     02     8037     0     1843     5.6     2       148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	140	051	00					
148     14     8044     0     1964     3.5     4       149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6	141		02					2
149     16     8045     0     2027     2.5     2       154     052     00     8050     0     2154     0.6     6								
154 052 00 8050 0 2154 0.6 6	149							
		052						
	155		02					

TABLE 2 Cont.

Ref. Orb.	Day	Hour	<u>Orbit</u>	Misses	Range	Elev. Angle	No. of Msg.
162		14	8058	o	1907	4.5	4
163		16	8059	0	1972	3.4	1
168	053	00	8064	0	2094	1.5	4
169	4	.02	8065		1958	3-7	1-
176		14	8072	0	1913	4.4	3
177		16	8073	0	1983	3.2	ī
182	054	00	8078	Ō	2119	1.1	4
183		02	8079	Ŏ	1939	4.0	4
190		14	8086	Ö	1988	3.2	4
191	•	16	8087	Ō	1837	5.7	1

TABLE 3

Ref. Orb.	<u>Da<b>y</b></u>	Hour	<u>Orbit</u>	Misses	Range	Elev. <u>Angle</u>	No. of Msg.
224	057	00	8120	0	2116	3.6	5
232	03.	15	8128	Ō	1874	6.7	3
233		16	8129	. 0	1964	3.6	
238	058	01	8134	1	1762	7.1	1 3 3 3
245	0,00	13	8141	0	2030	2.5	3
246		15	8142	Ō	1905	4.5	3
247		16	8143	0	1879	5.0	1
1	05 <b>9</b>	01	8148	0	1874	5.1	4
8	555	13	8155	0	2021	2.6	3
9		15	8156	0	2021	2.6	4
10		16	8157	0	2024	2.6	1
15	06 <b>0</b>	01	8162	0	1928	4.2	3
33		15	8170	0	1925	4.2	2
29	061	01	8176	0	1881	4.9	3
36		13	8183	0	1994	3.1	4
37		15	8184	0	1991	3.1	4
43	062	01	8190	0	2096	1.5	
50		13	8197	0	1962	3.6	3 3
51		15	8198	0	2027	2.5	3
57	06 <b>3</b>	01	8204	0	1970	3.4	4
64		13	8211	0	1716	7.9	2
65		15	8212	0	1858	5.3	2
71	064	01	8218	0	1947	3.8	4
78		14	8225	· 1	1308	17.5	1
79		15	8226	1	1592	10.5	1
85	065	01	8232	0	2046	2.2	4
92		14	8239	0	1869	5.1	3
93		15	8240	0	2118	1.1	3
99	06 <b>6</b>	01	8246	0	2007	2.9	4
106		14	8253	0	1871	5.1	3
107		15	8254	0	2119	1.1	3
113	067	01	8260	0	1941	3.9	3
120		14	8267	0	1959	3.6	4
121		15	8268	0	2026	2.6	3
127	06 <b>8</b>	02	8274	0	2011	2.8	3
134		14	8281	0	1694	8.4	3
135		16	8282	0	1946	3.8	3
140	06. <b>9</b>	00	8287	0	1934	4.1	4
141		02	8288	0	2020	2.6	3
148		14	8295	0	1734	7.6	3
149		16	8296	0	1879	5.0	2
154	070	00	8301	Ο.	1740	7.5	4
155		02	8302	0	2079	1.7	2
162		14	8309	0	1983	3.2	4
163		1.6	8310	0	1873	5.1	1

TABLE 3

Ref. Orb.	Day	Hour	<u>Orbit</u>	Misses	Range	Elev. <u>Angle</u>	No. of Msg.
168	071	00	8315	• 0	1752	7.3	1
169		02	8316	0	1866	5.2	1
176		14	8323	0	1803	6.3	2
177		16	8324	0 .	1734	7.6	1
182	072	00	8329	1	1672	8.8	3
183		02	8330	0	1835	5.7	1
190		14	8337	1	1604	10.2	3
191		16	8338	0	1850	5.5	1
196	073	00	8343	1	1656	9.1	4
197	;	02	8344	0	1904	4.6	1
204		14	8351	0	1856	5.4	3
205		16	8352	0	1826	5.9	. 1
210	074	00	8357	0	2045	2.3	3
218		14	8365	1	1642	9.4	2

TABLE 4

29         079         01         8427         0         1813         6.1         4           366         13         8434         1         1460         13.5         1           37         15         8435         0         1783         6.7         3           43         080         01         8441         0         1787         6.6         4           50         13         8448         0         1875         5.0         3           51         15         8449         1         1583         5.9         2           64         081         13         8462         0         1703         8.2         2           65         15         8463         0         1819         6.0         2           71         082         01         8467         1         1533         11.7         7.9         2           79         15         8477         1         1551         11.4         1         1         85         083         01         8483         1         1652         9.2         3         9         3         15         8491         1         1678         8.7	Ref. Orb.	<u>Day</u>	Hour	<u>Orbit</u>	Misses	Range	Elev. <u>Angle</u>	No. of
36         13         8434         1         1460         13.5         1           37         15         8435         0         1783         6.6         4           50         13         8448         0         1875         5.0         3           51         15         8449         1         1583         5.9         2           64         081         13         8462         0         1703         8.2         2           65         15         8463         0         1819         6.0         2           71         082         01         8467         1         1533         11.7         3           78         14         8476         0         1717         7.9         2         7           79         15         8477         1         1551         11.4         1         1           85         083         01         8483         1         1652         9.2         3         92         14         8490         0         1747         7.3         3         92         14         8490         0         1747         7.3         3         1         166	29	079	01	8427	0	1813	6.1	4
37         15         8435         0         1783         6.7         3           43         080         01         8441         0         1787         6.6         4           50         13         8448         0         1875         5.0         3           51         15         8449         1         1583         5.9         2           64         081         13         8462         0         1703         8.2         2           65         15         8463         0         1819         6.0         2           71         082         01         8467         1         1533         11.7         3           78         14         8476         0         1717         7.9         2         2           79         15         8477         1         1551         11.4         1         1           85         083         01         8483         1         1652         9.2         3         3           93         15         8491         1         1678         8.7         2         1           107         15         8505         1         <								
43         080         01         8441         0         1787         6.6         4           50         13         8448         0         1875         5.0         3           51         15         8449         1         1583         5.9         2           64         081         13         8462         0         1703         8.2         2           65         15         8463         0         1819         6.0         2           71         082         01         8467         1         1533         11.7         3           78         14         8476         0         1717         7.9         2           79         15         8477         1         1551         11.4         1           85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3           92         14         8490         0         1747         7.3         3           106         084         14         8504         0         1845         5.6         2					0			3
50         13         8448         0         1875         5.0         3           51         15         8449         1         1583         5.9         2           64         081         13         8462         0         1703         8.2         2           65         15         8463         0         1819         6.0         2           71         082         01         8467         1         1533         11.7         3           78         14         8476         0         1717         7.9         2           79         15         8477         1         1551         11.4         1           85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3         3           93         15         8491         1         1678         8.7         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1756         7.2         3		080			0			
65								3
65					1			2
65		081			0			2
71         082         01         8467         1         1533         11.7         3           78         14         8476         0         1717         7.9         2           79         15         8477         1         1551         11.4         1           85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3           93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3         121         15         8511         0         1952         3.8         3         121         125         7.8         3         135         16         8533         1         1725         7		***						2
79         15         8477         1         1551         11.4         1           85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3           93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3         1           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1 <td></td> <td>082</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3</td>		082						3
79         15         8477         1         1551         11.4         1           85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3           93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3         1           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>2</td>								2
85         083         01         8483         1         1652         9.2         3           92         14         8490         0         1747         7.3         3           93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5<								
92         14         8490         0         1747         7.3         3           93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2      <		083						3
93         15         8491         1         1678         8.7         2           106         084         14         8504         0         1845         5.6         2           107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3								3
107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           155         02         8553         0         1754         7.2         1           162								
107         15         8505         1         1514         12.2         1           113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           155         02         8553         0         1754         7.2         1           162		084						2
113         085         01         8511         0         1953         3.7         3           120         14         8518         0         1756         7.2         3           121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           155         02         8553         0         1754         7.2         1           162         14         8560         0         1754         7.2         1           163<								
120       14       8518       0       1756       7.2       3         121       15       8519       1       1666       8.9       1         127       086       02       8525       0       1952       3.8       3         134       14       8532       0       1725       7.8       3         135       16       8533       1       1728       7.7       1         140       087       00       8538       0       1928       4.1       5         141       02       8539       0       1780       6.7       2         148       14       8546       0       1782       6.7       3         149       16       8547       0       1832       5.8       1         154       088       00       8552       0       1819       6.0       5         155       02       8553       0       1754       7.2       1         162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       0		085						
121         15         8519         1         1666         8.9         1           127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           154         088         00         8552         0         1819         6.0         5           155         02         8553         0         1754         7.2         1         1           162         14         8560         0         1768         7.0         3         1         168         089         00         8566         0         1872         5.1         4<		003						3
127         086         02         8525         0         1952         3.8         3           134         14         8532         0         1725         7.8         3           135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           154         088         00         8552         0         1819         6.0         5           155         02         8553         0         1754         7.2         1         1           162         14         8560         0         1774         7.2         1         1         1612         10.0         1         1         168         089         00         8566         0         1872         5.1         4         4         169         02         8567								1
134       14       8532       0       1725       7.8       3         135       16       8533       1       1728       7.7       1         140       087       00       8538       0       1928       4.1       5         141       02       8539       0       1780       6.7       2         148       14       8546       0       1782       6.7       3         149       16       8547       0       1832       5.8       1         154       088       00       8552       0       1819       6.0       5         155       02       8553       0       1754       7.2       1         162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       1		086						3
135         16         8533         1         1728         7.7         1           140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           154         088         00         8552         0         1819         6.0         5           155         02         8553         0         1754         7.2         1           162         14         8560         0         1768         7.0         3           163         16         8561         1         1612         10.0         1           168         089         00         8566         0         1872         5.1         4           169         02         8567         0         1786         6.6         1           177         16         8575         1         1665         8.9         1           182								3
140         087         00         8538         0         1928         4.1         5           141         02         8539         0         1780         6.7         2           148         14         8546         0         1782         6.7         3           149         16         8547         0         1832         5.8         1           154         088         00         8552         0         1879         6.0         5           155         02         8553         0         1754         7.2         1           162         14         8560         0         1754         7.2         1           163         16         8561         1         1612         10.0         1           168         089         00         8566         0         1872         5.1         4           169         02         8567         0         1786         6.6         1           176         14         8574         0         1783         6.7         3           177         16         8575         1         1665         8.9         1           182								1
141       02       8539       0       1780       6.7       2         148       14       8546       0       1782       6.7       3         149       16       8547       0       1832       5.8       1         154       088       00       8552       0       1819       6.0       5         155       02       8553       0       1754       7.2       1       1         162       14       8560       0       1754       7.2       1       1         162       14       8560       0       1768       7.0       3       3       163       16       8561       1       1612       10.0       1       1       162       10.0       1       1       163       1       1642       10.0       1       1       162       10.0       1       1       162       10.0       1       1       162       10.0       1       1       162       10.0       1       1       166       6.6       1       1       166       6.6       1       1       178       6.7       3       1       1       184       8.5       1       1		087						
148       14       8546       0       1782       6.7       3         149       16       8547       0       1832       5.8       1         154       088       00       8552       0       1819       6.0       5         155       02       8553       0       1754       7.2       1         162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       0								2
149       16       8547       0       1832       5.8       1         154       088       00       8552       0       1819       6.0       5         155       02       8553       0       1754       7.2       1         162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       0								3
154         088         00         8552         0         1819         6.0         5           155         02         8553         0         1754         7.2         1           162         14         8560         0         1768         7.0         3           163         16         8561         1         1612         10.0         1           168         089         00         8566         0         1872         5.1         4           169         02         8567         0         1786         6.6         1           176         14         8574         0         1783         6.7         3           177         16         8575         1         1665         8.9         1           182         090         00         8580         1         1648         9.3         4           183         02         8581         0         2114         1.2         2           190         14         8588         0         1638         9.5         3           191         16         8589         0         1854         5.4         1           196								1
155       02       8553       0       1754       7.2       1         162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         205		088						
162       14       8560       0       1768       7.0       3         163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205		700						
163       16       8561       1       1612       10.0       1         168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         218								
168       089       00       8566       0       1872       5.1       4         169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         210       092       00       8608       0       1905       4.5       5         2								
169       02       8567       0       1786       6.6       1         176       14       8574       0       1783       6.7       3         177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         210       092       00       8608       0       1905       4.5       5         218       14       8616       1       1630       9.7       3         219       1		089						
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177       16       8575       1       1665       8.9       1         182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         210       092       00       8608       0       1905       4.5       5         218       14       8616       1       1630       9.7       3         219       16       8617       0       1878       5.0       1					0			
182       090       00       8580       1       1648       9.3       4         183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         210       092       00       8608       0       1905       4.5       5         218       14       8616       1       1630       9.7       3         219       16       8617       0       1878       5.0       1					I			1
183       02       8581       0       2114       1.2       2         190       14       8588       0       1638       9.5       3         191       16       8589       0       1854       5.4       1         196       091       00       8594       1       1540       11.6       3         197       02       8595       0       2057       2.1       1         204       14       8602       1       1639       9.5       2         205       16       8603       0       1863       5.3       1         210       092       00       8608       0       1905       4.5       5         218       14       8616       1       1630       9.7       3         219       16       8617       0       1878       5.0       1		090						
190     14     8588     0     1638     9.5     3       191     16     8589     0     1854     5.4     1       196     091     00     8594     1     1540     11.6     3       197     02     8595     0     2057     2.1     1       204     14     8602     1     1639     9.5     2       205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1								2
191     16     8589     0     1854     5.4     1       196     091     00     8594     1     1540     11.6     3       197     02     8595     0     2057     2.1     1       204     14     8602     1     1639     9.5     2       205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1								
196     091     00     8594     1     1540     11.6     3       197     02     8595     0     2057     2.1     1       204     14     8602     1     1639     9.5     2       205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1					0			
197     02     8595     0     2057     2.1     1       204     14     8602     1     1639     9.5     2       205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1		091			1			3
204     14     8602     1     1639     9.5     2       205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1								
205     16     8603     0     1863     5.3     1       210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1					1			2
210     092     00     8608     0     1905     4.5     5       218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1								1
218     14     8616     1     1630     9.7     3       219     16     8617     0     1878     5.0     1		092						
219 16 8617 0 1878 5.0 1		- <b>-</b> -						
		093						4

TABLE 4

Ref. Orb.	Day	<u>Four</u>	<u>Orbit</u>	Misses	Range	Elev. Angle	No. of Msg.
232		15	8630	1	1560	11.2	2
2:3:3		16	8631	. <u>.</u>		5.5	1
238	094	01	8636	i	1739	7.5	4
245		13	8643	Õ	1815	6.1	2
246		15	8644	1	1635	9.5	2
247		16	8645	0	2018	2.7	ī
1	095	01	8650	1	1723	7.8	3
8		13	8657	0	1919	4.3	3
9		15	8658	1	1590	10.5	2
15	096	01	8664	1	1732	7.6	4
22		13	8671	1.	1664	9.0	2
23		15	8672	1	1652	9.2	2

TABLE 5

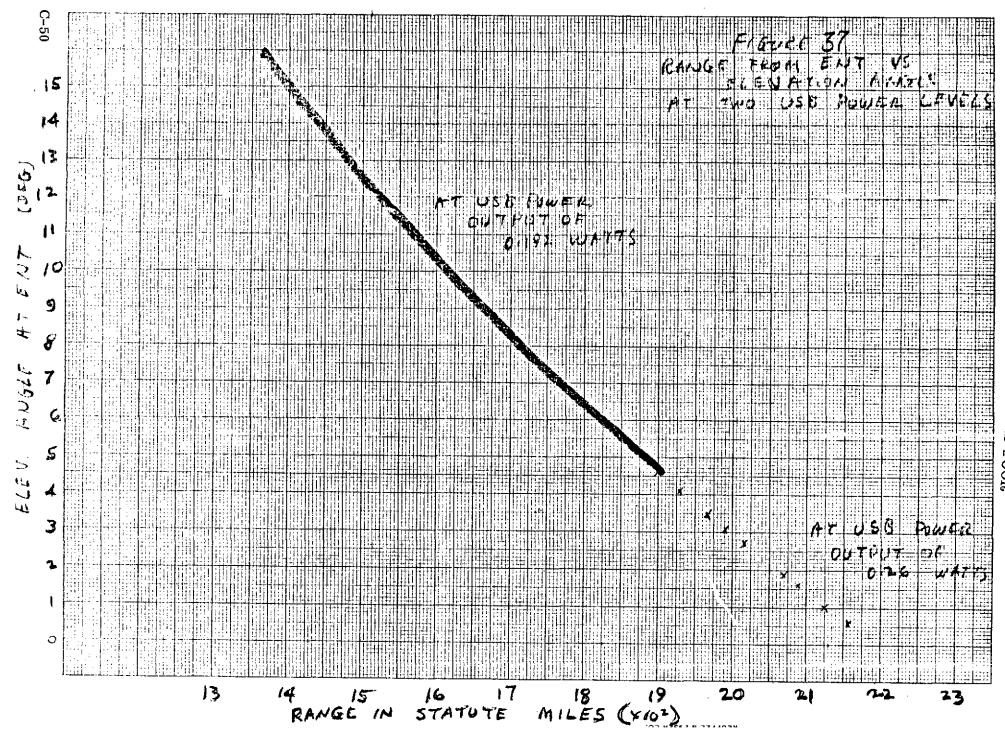
USB PERFORMANCE
at 0.192 watts
using DCP 6315 in Iceland

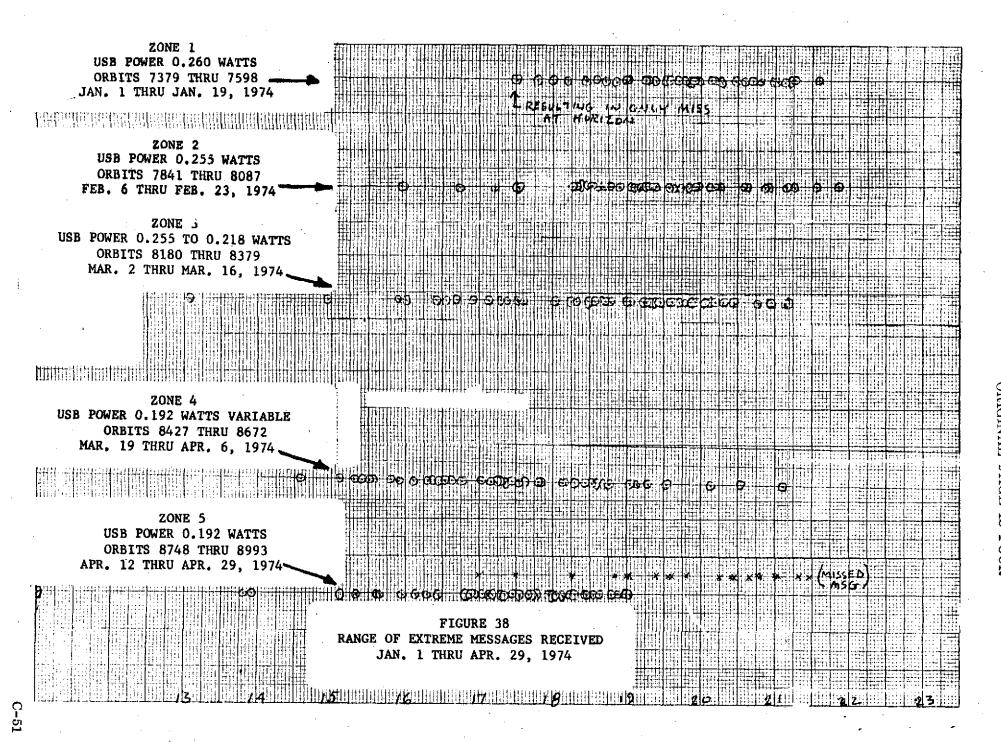
			ENT					
				Last	Msg			
			Misses	Re		Num.		
			at	Range	Elev.	of		
Day	Hour	Orbit	<u>Horizon</u>	St. Mi.	Deg.	Msgs.	Comments	
102	01	<b>8</b> 748	0	1690	8.5	3	Masking	
	14	<b>8</b> 755	0	1734	7.6	2	-	
	15	<b>87</b> 56	1	1745	7.4	1		
103	01	<b>87</b> 62	0	1806	6.3	2	Masking	
	14	<b>8</b> 769	0	1766	7.0	2	J	
	15	8770	1	1534	11.7	1		
104	.02	<b>87</b> 76	0	1796	6.4	2	Masking	
	14	<b>87</b> 83	0	1886	4.9	3	J	
	16	<b>87</b> 84	0	1717	7.9	1	Masking	
105	00	<b>8</b> 789	0	1847	5.5	4	Ŭ	
	02	8790	0	1844	5.6	2	Masking	
	14	<b>8</b> 797	0	1711	8.0	3	Ŭ	
•	16	<b>8</b> 798	0	1861	5.3	2	Masking	
106	00	<b>8</b> 803	0	1878	5.0	4	•	
	02	<b>8</b> 804	0	1754	7.2	. 2	Masking	
	14	<b>8</b> 811	0	İ729	7.7	2	J	
	16	<b>8</b> 812	1	1680	8.6	1		
107	00	<b>8</b> 817	1	1751	7.3	4		
	02	<b>8</b> 818	0	1866	5.2	1	Masking	
	14	<b>88</b> 25	0	1903	4.6	3	•	
108	00	<b>88</b> 31	1	1773	6.9	3		
	02	<b>8</b> 832	0	1888	4.8	1	Masking	
	14	<b>88</b> 39	0	1845	5.6	3	•	
	16	8840	0	1860	5.3	1	Masking	
109	00	<b>8</b> 845	1	1738	7.5	4	•	
	02	<b>8</b> 846	0	1896	4.7	1	Masking	
	14	<b>8</b> 853	0	1800	. 6.4	3	•	
110	00	<b>88</b> 59	1	1856	5.4	3		
	14	<b>8</b> 867	1	1629	9.7	3 2		
111	00	<b>8</b> 873	1	1704	8.2	3		
	15	8881	ī	1653	11.1	1		
112	01	8887	ī	1826	5.9			
	13	<b>8</b> 894	ī	1780	6.7	3 2		
	15	<b>8</b> 895	2	1386	15.3	2		

TABLE 5 Cont.

				ENT			
				Last	Msg		
			Misses	<u> </u>		Num.	
			at -	Range	Elev.	of	
<u>Day</u>	Hour	<u>Orbit</u>	<u>Horizon</u>	St. Mi.	Deg.	Msgs.	Comments
113	01	8901	1	1843	5.6	3	
	15	8909	1	1690	8.4	2	-
114	01	8915	2	1596	10.4	3	
	13	8922	1	1821	6.0	2	
	15	8923	1	1631	9.6	1	
115	01	8929	1	1567	11.0	3	
	13	8936	1	1615	10.0	2 2	
	15	8937	2	1381	15.5		
116	01	8943	1	1773	6.9	3	Masking
•	13	8950	0	1393	6.6	3 2	
	15	8951	1	1645	9.3	2	
117	01	8957	1	1712	8.0	3	Masking
	13	8964	0	1813	6.1	3	
	15	8965	1	1689	8.5	1	
118	01	8971	1	1730	7.7	1	Masking
•	14	8978	1	1728	7.7	2	
	15	8979	1	1630	9.7	1 .	
119	01	8985	3	1100	24.5	1	Masking
	14	8992	1	1561	11.1	2	
	15	8993	1	1514	12.2	1	

Total Msgs Received in 18 day: 118





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In Zone 5, in addition to the extreme ranges shown as circles, crosses are also shown to designate the range, within the ERTS horizon, at which expected messages were missed. These were derived from Figures 39 and 40. In Figure 39 are plotted the slant range from ENT for the last two messages received from each orbit of Table 1. These data were replotted in Figure 40 to derive the relationship of the range of the last message received to the range of the next expected message.

There is a large spread in the data plotted in Figure 40 because the range is dependent on the relative direction of the orbit trace. Using a conservative approach, the worse case is used, resulting in fewer attributions of missed messages. Figure 41 shows the ERTS positions A to C which permit DCS relay operations. Other positions do not fulfill the prerequisite of being simultaneously within the horizons of both the DCP and the ground station. The data in Tables 1 and 2 show that with USB power output in excess of 0.25 watts, messages from position C were received consistantly at Greenbelt. Position C represents the extreme range (horizon) for the USB portion of the relay chain. Consistant reception at this range is evidence that all previous power drops had no adverse effect on USB operational performances.

The data in Tables 3, 4, and 5 however show that with the USB power output below 0.25 watts, messages can no longer be received from C, but only from some intermediate point B.

No longer can the USB relay DCP messages out to the horizon of ENT. The operational range has been reduced. It began shrinking from the horizon at some telemetry-indicated USB transmitter power output level which the data in Tables 1 to 5 and in Figure 38 suggest is about 0.25 watts.

Because the evidence clearly shows a contraction of USB/DCS coverage, it was of interest to determine the degree to which other functions of the USB were affected. The USB transmitter is turned ON by a stored command before the spacecraft rises above the ground station horizon. Using the same reference orbits to assure identical conditions of azimuth, elevation and range, AOS locations were plotted for orbits from 7500 thru 9760. There was no visible difference in the location of AOS.

Figure 42 shows USB AOS locations unaffected by the power drop. Note that the dots (USB at 0.25 watts) and circles (USB at 0.19 watts) are at almost identical locations (68°N70°W and 61°N51.5°W) before and after power step down. The link continued to operate effectively even though the signal strength is significantly lower. The signal-to-noise level has not yet subsided to the level at which the output will be noticeably deteriorated.

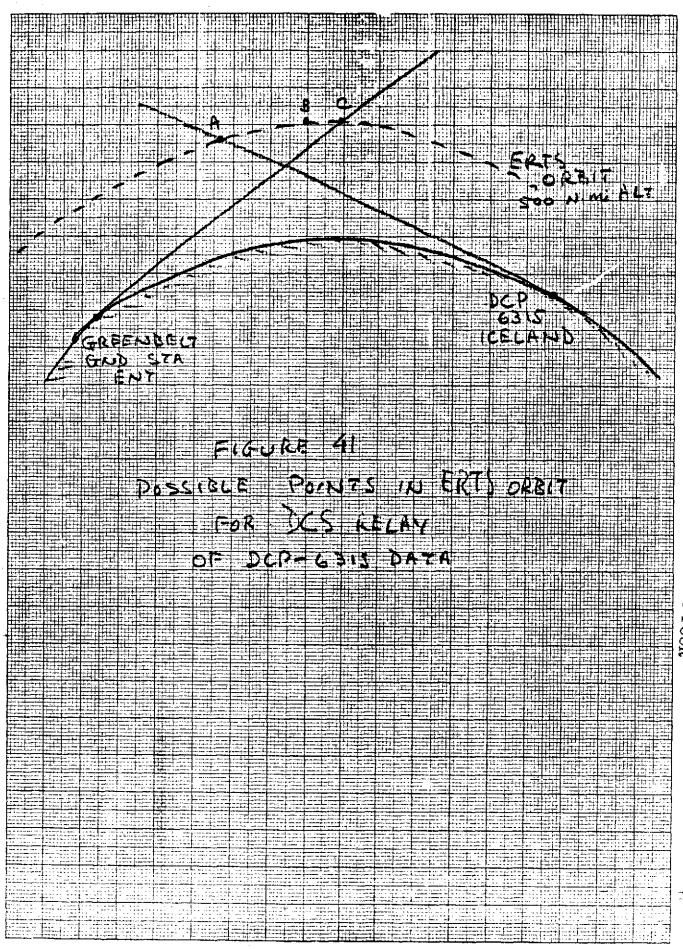
Ground Stations do not report signal level at acquisition, but only at maximum signal strength. These maximum levels show about a 2 db drop after the power step down. Clearly the signal-to-noise level at launch was so large that even at these reduced values no adverse effect can yet be seen.

In Figure 42, the effect of the power drop on DCS reception is also displayed ror the identical orbits. Note that the crosses (DCS at 0.25 watts) and squares (DCS at 0.19 watts) are clearly displaced. The squares are closer to the ground station, ENT. That is, the range has shortened.

However, even with this shortening of the range, it was not apparent to DCS observers that the coverage was diminished. Systematic fluctuations during the 18-day cycle, different for each DCP, together with occasional ground station and DCP problems, can obscure for weeks a minor decline in coverage.

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BEPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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Good telemetry and ranging continue to be provided.

As long as the power output was above 0.25 watts, the USB/DCS range was demonstrated to 2157 statute miles. The area coverage would consequently be  $\pi$  (2157) square miles. With power output down to 0.192 watts, the demonstrated range was 1900 miles and the area coverage was  $\pi$  (1900) square miles.

The range loss was then

$$\frac{2157 - 1900}{2157} = 12\%$$

and the area loss was

$$\frac{2157^2 - 1800^2}{2157^2} = 22\%$$

It should be remembered that, as described in Reference 1, when the pre-launch calibration curve for the USB was derived, the single low value point was at about 0.4 watts. The true value of USB power output may therefore be somewhat different than that derived from the telemetry of ERTS.

It is interesting to note that the same data above when reprogrammed to display data on the maximum range of the DCP transmitter (6315) showed no loss of range thruout this time period exceeding 2000 miles every day in the period of Zone 5, and achieving values of over 2260 statute miles, an elevation angle of  $1^{\circ}$  below the horizon!

K.S. Rizk

Systems Engineer

APPENDIX D

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	ELECTRIC CE DIVISION	-	*CLASS. LTR.	OPERATION	PROGRAM	SEQUENCE NO.	REV. LTR.
PHI	LADELPHIA TION REGUEST / RELEA	PIR NO.	U		- 1N23	— 109 FOR UNCLASSIFIE	
ROGRAM INFORMA	INON REGUEST / RELEA	NOE	TO USE UNI	FUR CLASSIFIE	ED AND O	FUR UNCLASSIFIE	
K.S. Rizk				. Winches	ter		
DATE SENT	DATE INFO. REQUIRED F	PROJECT AND REQ	. NO.		REFERENCE	DIR. NO.	<del></del>
5/2/74				ĺ			
SUBJECT	<u> </u>					<del></del>	<del></del>
Prince Albert Ho	orizon for MSS Recep	otion					
NFORMATION REQUEST	red/released						
Introduction:							!
	these early on-times The Prince Albert						
For a compl 10 April 1974, P received.	lete 18 day cycle, f Prince Albert report	rom orbit a	8477 on 23 liest time	March 19 when goo	74 thru d MSS da	orbit 8728 Ita was bein	on 1g
Amplifier), Link are used which h	sts this data. Also c 4 (USB) and MSS we have ERTS data "read ist column is listed	ere on, war: ly" time ea:	med-up and rlier than	operating Prince A	g proper 1bert's	ly. Only t actual acqu	hat data
Figure 1 sh The horizon flat movement to that	nows the horizon of tens at 80.9 <sup>0</sup> N beca latitude.	the Prince use the or	Albert gro bital incli	ound stat nation o	ion for f ERTS-1	ERTS MSS da . limits the	ta. northward
the earth's surf	al MSS horizon as cace. This correspo	nds to a si	lant range	1 is 184 of 3705	47 n. mi Km, at a	. (3421 Km) n elevation	along angle
It is inter along the earth'	esting to note the s surface of 1980 n	reception a	at 40 <sup>0</sup> W 80 <sup>0</sup> This was pr	N which o	correspo ue to a	nds to a di ducting ano	stance omaly.

K.S. Rizk

Systems Engineer

/pkp

PAGE NO. A RETENTION REQUIREMENTS Distribution: os COPIES FOR MASTERS FOR Jack Efner 3 MOS. Lee Smith 3 MOS. 6 MOS. L. Gonzales 6 M04. 12 MOS. MÇS. MOS.

Table 1
Prince Albert MSS Acquisition Times

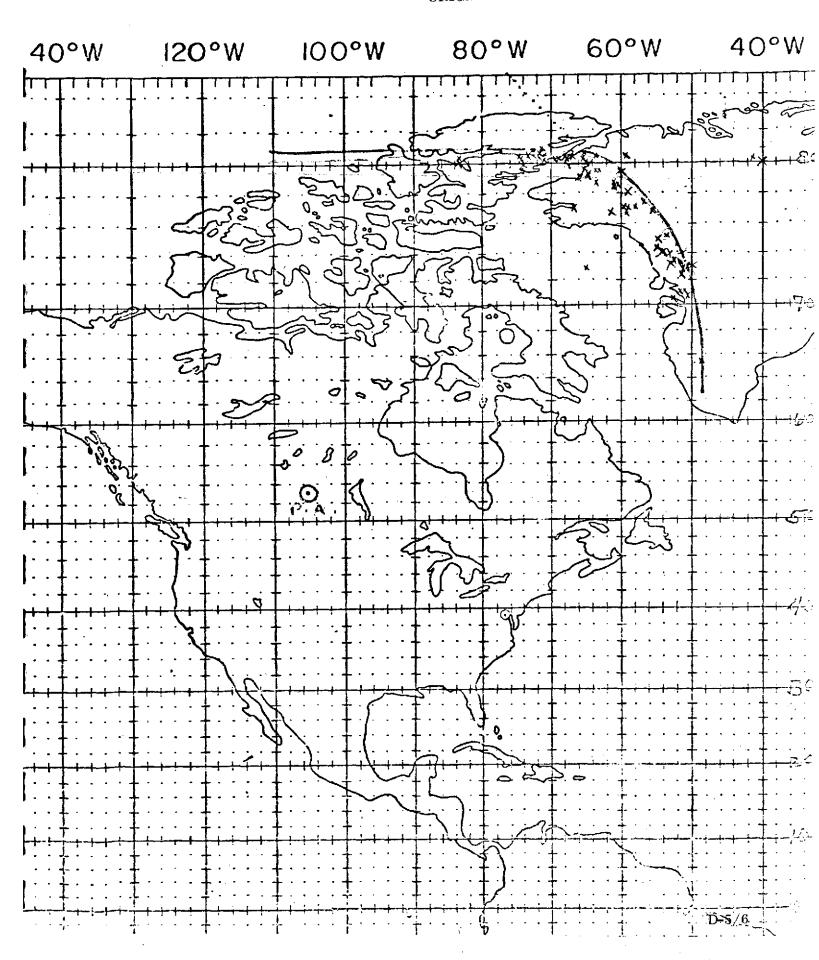
_		P.A. Start		ffective Start O	f	ERTS	Position
Date	Orbit_	Time	Link 3	Link 4	MSS	Long.	Lat.
3/23	8477	15:38:04	15.24.40	15 07 00			
3/23	8478	17:20:12	15:34:48	15:36:00	15:36:30	54	74
3/23	8479		17:16:47	17:17:00	17:18:31	67	78
3/23		19:01:49	18:59:10	19:00:55	19:01:45	72	80
	8493	19:07:30	19:05:48	19:07:00	19:07:30	64	80
3/25	8505	15:49:56	15:49:58	15:49:58	15:50:48	ľ	
3/25	8506	17:30:56	17:29:55	17:29:57	17:30:45	64	80
3/25	8507	19:13:12	19:12:21	19:11:57	19:13:11	66	80
3/26	8519	15:55:16	15:55:17	15:55:00	15:56:07		
3/26	8520	17:36:35	17:35:13	17:36:00	17:36:02	69	79
3/26	8521	19:18:50	19:18:04	19:18:45	19:18:53	74	80
3/27	8532	14:22:18	14:22:19	14:21:06	14:23:		
3/27	8533	16:01:47	16:01:50	16:01:00	16:02:40		
3/27	8534	17:42:11	17:40:31	17:41:00	17:41:19	60	79
3/27	8535	19:24:29	19:23:47	19:24:00	19:24:37	60	81
3/28	8546	14:27:13	14:27:12	14:26:42	14:28:04	"	91
3/28	8547	16:07:06	16:07:08	16:07:00	16:08:00	65	73
3/28	8548	17:47:51	17:47:00	17:46:39	17:47:31	66	
3/28	8549	19:30:05	19:29:55	19:30:03	19:30:47	00	79
3/29	8560	14:31:10	14:30:00	14:30:00		4.0	
3/29	8561	16:11:32	16:10:21		14:30:52	49	68
3/29	8562	17:53:31	19:51:57	16:10:00	16:11:13	55	77
3/29	8563	19:35:47		19:51:00	19:52:49	63	79
3/30	8574	· ·	19:35:13	19:34:00	19:36:05	72	81
3/30	8575	14:36:57	14:36:58	14:37:00	14:37:34		
3/30		16:18:32	16:18:34	16:18:00	16:19:26		
	8576 8573	17:59:09	17:58:30	17:59:00	17:59:22	62	80
3/30	8577	19:41:27	19:40:56	19:41:22	19:41:48	73	81

Table 1 (continued)

	· · · · · · · · · · · · · · · · · · ·	P.A. Start	E1	fective Start Of		ERTS Po	osition
Date	Orbit	Time	Link 3	Link 4	MSS	Long.	Lat
3/31	8588	14:41:59	14:41:30	14:40:00	14:42:18	50	70
3/31	85.89	16:22:46	16:21:47	16:20:00	16:22:39	53	77
3/31	8590	18:04:48	18:03:48	18:02:00	18:04:40	65	80
3/31	8591	19:47:05	19:47:04	19:44:58	19:47:56		_
4/1	8602	14:47:32	14:46:44	14:46:00	14:47:36	5:0	71
4/1	8603	16;28;26	16:27:30	16:27:00	16:28:22	58	77
4/1	8604	18:10:29	18:09:06	18:08:00	18:09:58	65	79
4/1	8605	19:52:47	19:52:22	19:50:00	19:53:14	71	81
4/2	8616	14:53:01	14:52:27	14:52:00	14:53:19	65 71 51	71
4/2	8617	16:34:02	16:33:13	16:33:00	16:34:05	58	78
4/2	8618	18:16:08	18:15:14	18:15:00	18:13:06	64	- 80
4/2	8619	19:58:34	19:58:05	19:57:00	19:55:56	68	80
4/3	8630	14:58:42	14:58:10	14:57:00	14:59:02	51	71
4/3	8631	16:39:45	16:38:56	16:38:00	16:39:48	58	79
4/3	8632	18:21:48	18:20:32	18:20:00	18:21:24	66	80
4/3	8633	20:04:05	20:03:48	20:02:00	20:04:40	77	80
4/4	8644	15:04:06	15:02:13	15:02:00	15:03:03	51	73
4/4	8645	16:45:19	16:43:24	19:43:00	16:44:14		78
4/4	8646	18:27:27	18:26:15	18:26:00	18:27:05	59 68	81
4/5	8658	15:09:37	15:08:21	15:08:00	15:09:11	50	73
4/5	8659	16:50:56	16:48:42	16:48:	16:49:32	70	76
4/5	8660	18:33:06	18:31:57	18:31:00	18:32:47	65	80
4/6	8672	15:15:10	15:13:28	15:13:00	15:14:30	53	73
4/6	8673	16:55:35	16:54:24	16:54:00	16:55:16	53 40	80
4/6	8674	18:38:45	18:37:40	18:37:00	18:38:22	65	80
4/6	8675	20;21;01	20:20:56	20:20:00	20:21:48	72	81
4/7	8686	15:20:42	15:20:06	15:20:00	15:20:56	51	74
4/7	8687	17:02:14	17:00:32	17:00:00	17:01:22	51 63	78
4/7	8688	18:44:24	18:43:48	18:44:00	18:44:38	70	80

Table 1 (continued)

		P.A. Start	E	ffective Start O	£	ERTS Po	osition
Date	Orbit	Time	Link 3	Link 4	MSS	Long.	Lat.
4/8	8700	15:26:19	15:25:54	15:26:00	15:26:46	53	74
4/8	8701	17:09:10	17:09:10	17:07:00	17:10:02	Ī	
4/8	8702	18:50:04	18:49:31	18:48:00	18:50:23	67	81
4/8	8793	20:32:50	20:32:47	20:32:16	20:33:39	63	80
4/9	8714	15:32:02	15:29:57	15:30:00	15:30:49	54	74
4/9	8715	17:13:31	17:12:23	17:12:00	17:13:15	60	79
4/9	8716	18:55:55	18:54:49	18:54:00	18:55:41	74	80
4/9	8717	20:38:05	20:38:05	20:37:00	20:38:56		



APPENDIX E



PHILADELPHIA

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ROGRAM	INFORMATION	REQUEST	/RELEASE

	*CLASS, LTR.	OPERATION	PROGRAM	SEQUENCE NO.	REV. LTR.
IR NO.	์ บ	- 1N23	ERTS	121	

CLASSIFIED AND "U" FOR UNCLASSIFIED

FROM		то	
K.S. R	izk	T.W.	Winchester
8/16/74	DATE INFO. REQUIRED	PROJECT AND REQ. NO.	REFERENCE DIR. NO. PIR-U-ERTS-1N23-108 dated April 30, 1974
SUBJECT		ebend Video Tano Recorde	

## INFORMATION REQUESTED/RELEASED

## Introduction

The reference PIR describes the history of Wide Band Video Tape Recorder No. 1 (WBVTR-1) from launch to Orbit 9000. This report updates the history thru Orbit 10500.

## Discussion

The history of WBVTR-1 for the last 1500 orbits is summarized in Table 1. The corrective actions employed were:

- a change in the Record input current attenuator during Orbit 9342 (change from 7 db insertion loss to 6 db) and again in Orbit 10207 (change from 6 db insertion loss to 5 db).
- b) LAP operation in Orbit 9998.
- Headwheel shoe multiple cycling (in and out) in Orbit 10373. c)
- repetitive Test, Records and Playbacks after Orbit 10373.

In general these corrective actions have not as yet produced major improvements. Figures 1, 2, & 3 are strip charts of selected WBVTR-1 functions for tape recorder performance since Orbit 10373. The sequence of orbits is from right-to-left. Time increases left-toright in each orbit, with the single exception of right to left in Orbit 10375 of Figure 1.

A comparison of the values shown in Figures 1, 2, and 3 with that of the recent past (Orbit 9530) and with the normal since launch is shown in Table 2.

During Orbit 10421, WBR was accidentally left in Standby both before and after the Rewind preceding the two Record operations (see Figure 3). During this 15 minutes of Standby, the Headwheel current declined from 450 ma to 430 ma, showing there was no headwheel contact with the tape (such as would occur in a broken pivot) in this condition.

Table 2 shows that during the orbits since 10393, there is a trend toward improvement in Headwheel Current. Record and Playbacks will be continued for about 10 more cycles after which a study of the resultant data will be made to seek effective corrective action.

K.S. Rizk, Sys	tems Higineer				
Distribution:	L. Smith J. Hayes (2) R. Stauffer D. Schwartz	B. Phucas H. Boys K. Rizk (3)	1 of 6	#RETENTION RI COPIES FOR  I MO. 3 MOS.  MOS.	EQUIREMENTS  MASTERS FOR  3 M09.  6 M05.  12 M05.  M05.  D0 NOT DESTROY

	1974					
STATE	DATE	ORBIT	ACTIVITY	ACTION TAKEN	PERT. RESULTS	FOOTAGE
LIM	APR 30	9001 to			HWI upper 600 ma.	
OPNS	MAY 24	9341	Rec & P/B	Repetitions	P/B V upper 500 mv	1050-1250
					MFSE 50 to 250	attraction appared
				Changed Insert. loss	P/B V gradually	
TEST	MAY 24	9342	Rec. Current adj.	from / db to 0 to 6 db	climbed to upper 600 ma	1050-1250
LIM	MAY 24	9343			HWI up to .66	1,030 1129
OPNS	JULY 2	9880	Rec & P/B	Resumed opns	MFSE 75-400	1050-1250
LIM			HWI rose rapidly			
OPNS	JULY 2	9881	to 730	Suspended opn		1050-1250
			MFSE up to 5000	F		1030 1230
STUDY	JULY 2	9882	None			
	JULY 10	9997				
TEST	JULY 10	9998		LAP		
TEST	JULY 10	9999 -	Rec & P/B		HWI 660-710	950-1000
	JULY 11	10003			MFSE 3000	
TEST	JULY 11	10004	Rec & P/B		HWI 680-720	1100-1200
	JULY 17	10087			MFSE ~5000	
STUDY	JULY 17	10088	None	Study at GE, NASA		
	JULY 25	10206		and RCA		
				Changed Insert. loss		
TEȘT	JULY 25	10207	Rec Current Adj	from 6 db to 7 to 0		
				to 5 db		
	j				HWI 660-710 ma	
TEST	JULY 25	10212	·		MFSE~ 10000	1100-1220
					P/B V 270 to 490 mv	<u> </u>
STUDY	JULY 25	10212	NONE	Study at GE, NASA		1
	AUG 5	10361		and RCA		<u> </u>
TEST	AUG 5	10362	R/W to 8 (footage)			8
TEST	AUG 6	10373		33 Shoe Cycling in/out		8-91
TEST	AUG 6	10375	twice per day	total of 11 cycles	HWT slowly dropping	
	AUG 10	10422	Double Rec & P/B	1	to 580 ma	9-108
COURT	110 10	10/00			MFSE above 12000	
STUDY	AUG 10	10422	NONE	Study at GE, NASA	·	
	AUG 15	10500	<u> </u>	and RCA		

TABLE 2

COMPARISON OF WBR FUNCTION VALUES.

			Norm Launch		Recent	Range	
			to Orb	Orb	Orb	Orb	1
FUNC	DESCRIPTION	MODE	9000	9530	10275-10392	10393-10422	Units
13031	Recorder	Rec	3.48	3.50	3.50	3.50	amperes
	Input	P/B	3 <b>.</b> 75	3.76	3.76	3.76	
Į į	Current	Rew	2.02	2.04	2.04	2.04	ĺ
		Stby	1.90	1.71	1.52-1.65	1.52-1.65	
13030	Headwheel	Rec	575	557	610-690	530-640	m.a.
İ	Motor	P/B	570	525	560-670	550-640	
	Current	Rew	450	450	450-460	450-460	Ì
		Stby	445	445	450	430-450	·
13026	Capstan	Rec	245	260	210-280	210-280	m.a.
	Motor	P/B	255	260-310	210-280	210-310	
	Current	Rew	192	220	220-260	230-280	<u> </u>
13023	Playback	P/B	420	520-580	350-700	430-720	m.v.
	Voltage						
	MFSE Counts	P/B	10	80	~15000	~15000	-

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E-4

